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AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE NAVAL AVIATION DEPOT NORTH ISLAND SAN DIEGO, CALIFORNIA 92135-5112

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GASEOUS EMISSIONS FROM AIRCRAFT ENGINES

A HANDBOOK FOR THE CALCULATION OF EMISSION INDEXES
AND GASEOUS EMISSIONS FROM AIRCRAFT ENGINES

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Naval Environmental Protection Support Service

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Aircraft Environmental Support Office
Naval Aviation Depot, Naval Air Station
Vorth Island, San Diego, CA 92135
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A HANDBOOK FOR THE CALCULATION OF EMISSION INDEXES
AND GASEOUS EMISSIONS FROM AIRCRAFT ENGINES

AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE
NAVAL AVIATION DEPOT
NORTH ISLAND
SAN DIEGO, CALIFORNIA 92135-5112

PREFACE

The Commander, Naval Air Systems Command provides the Aircraft Environmental Support Office to the Naval Environmental Protection Support Service, through the Commanding Officer, Naval Aviation Depot North Island. The Aircraft Environmental Support Office is responsible for managing and issuing air emissions and noise level data from naval air operations and related maintenance functions.

The Naval Facilities Engineering Command, through the Naval Environmental Protection Support Service, assigned the Aircraft Environmental Support Office the task of preparing a Handbook of Gaseous Emissions from Aircraft Engines.

The first summary of gaseous emissions from aircraft engines, by the Aircraft Environmental Support Office, appeared in 1972. It was a two-page list of emissions from eight types of engines. This list soon expanded into the Aircraft Engine Emissions Catalog, which was a collection of emissions data obtained both by the Aircraft Environmental Support Office and by others. The Aircraft Engine Emissions Catalog, through the addition of emissions data by several revisions and supplements, soon became a document of some 400 pages. Now the user, who often had no experience in measuring or qualifications in evaluating emissions data, assumed the task of searching out fundamentals from a mass of data. Further expansion of the Aircraft Engine Emissions Catalog was destined to produce an unwieldy publication. It would not meet the need of most users for a convenient and reliable source of information about gaseous emissions from various types of aircraft engines.

The Aircraft Environmental Support Office decided that a Handbook, featuring our selection of typical emissions from an engine type, would be the best way to present emissions data. The Handbook would list only a single representative engine for each type/numeral/model indicator, unless changed emission characteristics, caused by the modification of the engine design, justified multiple listings.

While the Aircraft Environmental Support Office was collecting emissions data, SAE (formerly the Society of Automotive Engineers), through its E-31 Committee (Aircraft Exhaust Emission Measurement), was standardizing methods of emissions measurements and calculations. The work of the E-31 Committee produced a publication, Aerospace Information Report (AIR 1533), which defines optimum procedures for the calculation of basic emissions parameters for aircraft engines.

<u>Gaseous Emissions From Aircraft Engines</u> brings together the standardized calculations of SAE and the selections of emissions data of the Aircraft Environmental Support Office.

This Handbook is intended for operators of test facilities, officers at Naval Aviation Depots and Aircraft Intermediate Maintenance Depots, and other personnel who need to estimate the amount of gaseous emissions coming from the operation of aircraft engines. It shows how to calculate emission indexes from the measured concentrations of gases in the engine exhaust, and how to use emission indexes with engine operational data to estimate the total emissions from an engine. It defines how the Aircraft Environmental Support Office calculates and uses emission indexes to estimate emissions from aircraft engines. It supports these explanations with examples of the calculations. It also shows how to use computers and small calculators to make the calculations. The Handbook includes examples of emissions data for those engines most likely to be operated at naval air installations.

Of course, this Handbook must change to keep up-to-date. We expect to obtain improved emissions data as well as emissions data for other engines. We expect revisions to the SAE standard methods for calculating emission indexes, and when these occur we will modify AESO 1-87 as needed. We expect to write enhanced and additional computer and calculator programs. We may change format of tables and data sheets for improved ease of use. With these changes in mind, the format is loose-leaf. In this way we can expand sections and appendixes through the issue of additional pages rather than by issue of a new report. Each data sheet and each summary table has the date of printing at the bottom of the page.

This copy of AESO Report No. 1-87 contains all additions and revisions to April 4, 1990.

We look forward to receiving comments from users and readers of this Handbook.

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GASEOUS EMISSIONS FROM AIRCRAFT ENGINES

A Handbook for the Calculation of Emission Indexes and Gaseous Emissions from Aircraft Engines

AESO Report No. 1-87, September 1987

EXECUTIVE SUMMARY

For test cells, regional and state air pollution control agencies require that naval air installations obtain first, a permit to construct, and then a permit to operate. To apply for permits, personnel responsible for operating the test cells need to know the amounts of gaseous and particulate emissions formed during engine testing. This Handbook shows how to estimate the gaseous emissions of carbon monoxide, oxides of nitrogen and hydrocarbons formed during the operation of gas turbine engines.

The estimation of total emissions needs, for each power setting of the engine, (1) a ratio of the contaminant formed to the amount of fuel used (the so-called emission index), (2) the duration of the operation and (3) the fuel flow rate. Of these, the emission index is the most difficult to find.

This Handbook furnishes summary tables of representative emission indexes, at various power settings, for the gas turbine engines most likely to be operated at naval air installations. These tables also include fuel flow rates. Thus, anyone knowing the duration of the power settings can estimate the total gaseous emissions from various aircraft engines. The discussion of the emission index includes instructions on how to calculate it using both computers and small programmable calculators.

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L INTRODUCTION

Gaseous emissions from aircraft engines are an obvious source of air contamination. Although military aircraft engines are exempt from emission regulations, the facilities for testing them, such as test cells, are Test cells are emission sources because of the aircraft engines operating within them. Personnel, responsible for operating these facilities, often must apply to regional regulating agencies for authority-to-construct or For gaseous emissions, the regulating agencies permission-to-operate. want to know the concentrations and the amounts of the combustion products such as carbon monoxide, carbon dioxide, oxides of nitrogen, hydrocarbons and oxides of sulfur coming from the operation of the engine. this information to determine whether or not a facility is in compliance with their regulations. If a facility is out of compliance, emissions data aids in finding an acceptable solution, such as modification of the facility, an emissions trade, or a rule change. One use of this Handbook is to estimate emissions from the testing of an aircraft engine in a test cell and, hopefully, to eliminate the expense and delay of additional and We believe that this Handbook meaningless source testing. sufficient data to make a reasonable estimate of the gaseous emissions coming from most of the gas turbine engines in the navy inventory.

The estimation of the amount of a gaseous constituent in the exhaust from an aircraft engine, for a specified length of time at any power setting, uses (1) a ratio of the gaseous constituent formed to the amount of fuel used (the so-called emission index), (2) the duration of the operation and (3) the fuel flow rate. With these data, the estimation of total emissions is simply a matter of finding the amount of a constituent formed at each power setting, then adding the amounts from the various power settings to get the total emissions of that constituent. However, of the needed data, only the fuel flow rates are readily available. Emission indexes are hard to find and durations of operation are poorly defined.

Emission indexes are the results of special testing and, even if known, normally are not a part of engine operational records. Also, an emission index is not a constant value. Emission indexes for the same power setting vary not only among engines of the same type and model but also among the same power setting used at different times during an operating sequence for the same engine.

Do not expect to find accurate records of engine run times at various power settings at the facility testing the engine. Although these records often specify a run time to qualify the engine at various power settings, they do not account for other run times such as those needed to get the engine to stable conditions, those used in changing between power settings and those used in special test sequences.

This Handbook first selects, from the database at the Aircraft Environmental Support Office, those emission indexes, which in our opinion, represent the emissions from an engine type, and are suitable for estimating the amounts of emissions from similar engines. Then, the summary tables of section 7 list emission indexes and other emissions data for a group of power settings. These tables include fuel flow rates. Now, by referring to a single page, anyone knowing the engine run times at various power settings can estimate the total gaseous emissions from various aircraft engines. We expect that many users of this handbook need only the summary tables of section 7.

Because of the importance of the emission index and because some users may have to calculate it, this Handbook describes in detail its calculation and use.

The optimum calculation of the emission index uses a computer for the matrix solution of ten combustion equations. The Aircraft Environmental Support Office believes that the IBM AT/XT (or compatible) computers, now widely used, will have increasing availability. Our computer programs are for it. This Handbook gives all the details needed to get data into the matrix and solve it using such computers. The computer programs (Appendix B), feature steps to make a permanent record of both the data used in the calculations and the results of the calculations.

For those without a computer, this Handbook shows how to use a small programmable calculator to get solutions equivalent to the ones obtained using a computer. The calculator programs need a Hewlett Packard HP-41C/41CV/41/CX calculator. The calculator programs (Appendix A) record entries and calculations, but the most important programs also have a non-printing version.

Appendix C contains a collection of the data sheets each of which gives complete information about a single power setting, including all of the data needed to calculate the emission in x by the matrix solution. These data sheets provide the data for the summary tables of section 7. We expect that, because of its specialized character, most users of this Handbook do not need Appendix C. Accordingly, this Handbook may be transmitted without it.

2 BACKGROUND INFORMATION

The estimation of the gaseous emissions coming from an aircraft engine needs an emission index for each constituent of the exhaust. This section defines the emission index, gives background information about its calculation, and relates the contents of this Handbook to Aerospace Information Report AIR 1533* (Reference 1).

2.1 Emission Index

The term 'emission index' is the same as the term 'emission factor' as defined by the U. S. Environmental Protection Agency in AP-42 (Reference 2):

"One of the most useful (and logical) tools for estimating typical emissions is the 'emission factor', which is an estimate of the rate at which a pollutant is released to the atmosphere as a result of some activity, such as combustion or industrial production, divided by the level of that activity (also expressed in terms of a temporal rate). In other words, the emission factor relates the quantity of pollutants emitted to some indicator (activity level) such as production capacity, quantity of fuel burned, or vehicle miles traveled."

When applied to aircraft engines, an emission index (emission factor) is a ratio which relates the amount of a pollutant, in the exhaust from an aircraft engine, to the amount of fuel used. Because aircraft engines use relatively large amounts of fuel, a convenient expression for the emission index is units of mass per hour divided by 1000 units of mass per hour, i.e., pounds of pollutant per 1000 pounds of fuel, or any other mass units, such as kilograms of pollutant per 1000 kilograms of fuel. The emission index is independent of the total amount of fuel used.

2.2 Methods of Calculation for the Emission Index

At first, the calculation of an emission index used a linear equation (References 3, 4 and 5). The variables in this equation are the measured concentration of the constituent in the exhaust, the molecular weight of the constituent and the hydrogen-to-carbon ratio of the fuel. Later, References 5, 6 and 7 developed, for aircraft piston and gas turbine engines, a procedure which used a group of simultaneous equations in a matrix solution. Reference 8 developed a more comprehensive matrix solution from the basic matrix.

^{*} This Handbook refers to Reference 1 as SAE AIR 1533. Some references to SAE AIR 1533 include a following number in parenthesis. This number identifies an equation in SAE AIR 1533.

The matrix method sets up, through a single solution, parameters for determining all of the emission indexes, as well as other variables. The matrix method needs a computer of sufficient size and speed to make the calculations for the solution of a 10 x 10 or an 11 x 11 matrix. The size 11 matrix uses argon and nitrogen as separate constituents. The size 10 matrix combines them. Linear equations, derived from the matrix solution, allow a small programmable calculator to determine emission indexes which are equivalent to those obtained using the matrix solution.

2.3 Aerospace Information Report AIR 1533 (SAE AIR 1533)

The SAE* Technical Board acknowledges Reference 8 as the source for much of the subject matter in their publication, SAE AIR 1533. The SAE Technical Board recommends this publication as an American National Standard for the calculation of emission indexes for gas turbine engines. The Aircraft Environmental Support Office (AESO) supports this procedure as the optimum method for the calculation of emission indexes and expects to use it as the primary method for determining all emission indexes.

This Handbook is correlated with SAE AIR 1533. It uses the same equations, terms, definitions, nomenclature and symbols, except as noted for hydrocarbons and efficiency (see par. 2.4). The user of this Handbook needs to refer to SAE AIR 1533 for information such as the chemical equation for the combustion of a hydrocarbon fuel in air, the set of ten simultaneous equations needed for the matrix and the development and use of the comprehensive matrix solution. This Handbook does not repeat this information but instead, supplements SAE AIR 1533 by concentrating on applications, further explanations, examples of specific calculations, and comparisons of the calculations by linear equations with those by the matrix solution. To enhance coordination, this Handbook often uses the data from the sample calculation of SAE AIR 1533 (pages 34-36) in its examples.

For the convenience of the user, the Aircraft Environmental Support Office has purchased reprints of SAE AIR 1533 and expects to include one with each copy of this Handbook as long as our supply lasts. We advise the user that SAE AIR 1533 is not a part of this Handbook and that the copyright of SAE AIR 1533 belongs to SAE.

NOTE: THIS COPY OF AESO REPORT NO. 1-87 DOES NOT INCLUDE A REPRINT OF SAE AIR 1533.

^{*} The Society of Automotive Engineers now uses the acronym SAE as the name of the organization.

2.4 Nomenclature and Suggested Values

In this Handbook, the notations of nomenclature and suggested values appear close to the place of use rather than in a summary. These are the same in both this Handbook and SAE AIR 1533 except as noted in paragraphs 2.4.1 and 2.4.2. Both publications use the same definition of terms. Those needing complete lists should refer to pages 3 to 5 of SAE AIR 1533.

2.4.1 'Hydrocarbons'

This Handbook uses $C_x H_y$ to indicate the exhaust hydrocarbons rather than the abbreviation HC. A hydrocarbon fuel uses the general formula $C_m H_n$. The use of $C_x H_y$ or $C_m H_n$ is consistent with using chemical formulas as nomenclature for carbon monoxide, carbon dioxide and oxides of nitrogen. Since the composition of the exhaust hydrocarbons usually is not known, this report uses x = m and y = n.

2.4.2 'Efficiency'

To accommodate different computer printers, this Handbook sometimes uses 'NO $_{\rm X}$ C/E', instead of the Greek letter eta ($^{\rm N}$), as a notation of the efficiency for the conversion of the oxides of nitrogen to nitric oxide. It also writes out the term 'combustion efficiency' instead of using the notation $_{\rm b}$. The letter eta appears at different locations in the character set of the printers and sometimes is missing.*

^{*} The print-outs from the computer programs in this Handbook also use the degree symbol. It too appears at different locations in the character sets of printers. Users may have to modify our computer program to coordinate with their printer. Because we used BASIC as the program language, modification is easy. For example, in the program line LPRINT CHR\$(###), "F"; the value field (###) locates the degree sign in the character set. For the IBM Proprinter the value field is 248, for the HP LaserJet Printer, the value field is 179. Change this line as needed.

3 MEASUREMENTS NEEDED TO DETERMINE EMISSION INDEXES

The concentrations of carbon monoxide, carbon dioxide, oxides of nitrogen, and hydrocarbons in the engine exhaust are the most important variables in the calculation of emission indexes and, as a group, account for most of the value of the indexes. These concentrations must be measured, at each power setting, during the operation of the engine. Ideally, other measured data include the humidity of the ambient air (wet and dry bulb temperatures, relative humidity and barometric pressure), the concentrations of nitric oxide (NO), the efficiency of the converter for changing nitrogen dioxide (NO₂) to nitric oxide, the concentration of oxygen, and the carbon-hydrogen analysis of the fuel. Paragraphs 3.4, 3.5, 3.6 and 3.7 tell how to estimate these data when they are missing. This section also discusses adjustments to the measured concentrations to compensate for instrument interferences by oxygen, carbon dioxide and water.

3.1 Units of Measurement

Emissions data usually record the measured concentrations of carbon dioxide and oxygen as percents, and the concentrations of carbon monoxide, oxides of nitrogen, nitric oxide, and hydrocarbons as parts per million (ppm). The combustion equations discussed in SAE AIR 1533 and in this Handbook use mole fraction concentrations (indicated by number enclosed in brackets, []). To convert percent to a mole fraction concentration, divide by 100. To convert parts per million to a mole fraction concentration, divide by 1,000,000. The computer and calculator programs in this Handbook accept the inputs of the concentrations of carbon dioxide and oxygen as percents and the inputs of all other concentrations as parts per million. The programs make the needed conversions to mole fraction concentrations.

3.2 Sampling Position

If the engine is on a test stand or in an airframe, the sampling position is at the engine exhaust plane. If the engine is in a test cell, the sampling may be elsewhere in the exhaust system. Most of the sampling posicions used by the Aircraft Environmental Support Office were in a test cell after the addition of supplemental air, so that the measured emissions represented the exhaust from the test cell rather than the exhaust from the engine. For a completed combustion reaction, the concentrations of the constituents may vary with the sampling position; the emission index, which is a ratio, does not. For example, the concentration of the constituents in a sample taken directly behind an engine will be much higher than the concentrations of one withdrawn further from the engine, after the addition of air to the exhaust stream. By contrast, the emission indexes at each of these positions will be about the same. The air did nothing other than dilute the concentration.

3.3 Basis of Measurement

The basis of measurement of the concentrations of gases in the exhaust of an engine is wet, semi-dry or dry. The exhaust stream from the

engine contains water formed during combustion as well as that from the ambient air. If a gas stream is not dried before analysis, the basis of measurement is wet. If the gas stream is dried partially, for example, by passing through a cooling coil to remove most of the water, the basis of measurement is semi-dry. If the gas stream is dried completely the basis of measurement is dry.

A common measurement basis is semi-dry for carbon monoxide, carbon dioxide, and oxygen, and wet for oxides of nitrogen and hydrocarbons. Some measurements of the oxides of nitrogen may be on a semi-dry basis. The recommended basis for hydrocarbon measurements is wet (References 3, 4 and 7). However, some instruments measure hydrocarbons on a semi-dry basis. The computer and calculator programs in this Handbook do not adjust for semi-dry hydrocarbon measurements. To use such measurements, adjust to a wet basis before using in the programs.

3.4 Humidity of the Inlet Air and the Exhaust Sample

Conversions from a semi-dry to a wet (or dry) basis and the calculation of X/m use the variable h, which is the humidity of the inlet air (moles of water vapor per mole of dry inlet air). All emission calculations need a value for h, either determined or calculated. Figure 3-1 shows how to obtain the humidity of the inlet air using either a psychrometric chart or a vapor pressure-temperature table.

When humidity data are missing, use a reasonable estimate for h based on representative relative humidities, temperatures and barometric pressures. For example, The Aircraft Environmental Support Office uses h = 0.01 for measurements in California, and h = 0.02 for measurements in Florida.

3.4.1 Humidity of the Inlet Air from Psychrometric Charts

Psychrometric charts appear in many engineering handbooks. Usually these charts are relatively small, appear cluttered because of much information in a small space, and consequently are hard to read. Those using psychrometric charts should find a large one such as Reference 9. A typical chart plots dry bulb (ambient) temperature as the abscissa and specific humidity (pounds or grains of water per pound of air) as the ordinate. In addition, curves show various relative humidities and dew points. Lines show wet bulb temperatures.

To determine the specific humidity from relative humidity measurements, find the intersection of any two of the following: the dry bulb temperature line, the wet bulb temperature line or the relative humidity curve; then read across to the specific humidity on the ordinate. Or, if the dew point is given, read directly across to the specific humidity. Convert the specific humidity (W) (a weight ratio) to the humidity of the inlet air (h) (a molar ratio) by using the ratio of the molecular weights of water (MWATER) and air (MAIR) (see SAE AIR 1533 page 34). A psychrometric chart applies to only one barometric pressure, usually 29.92 in. Hg.

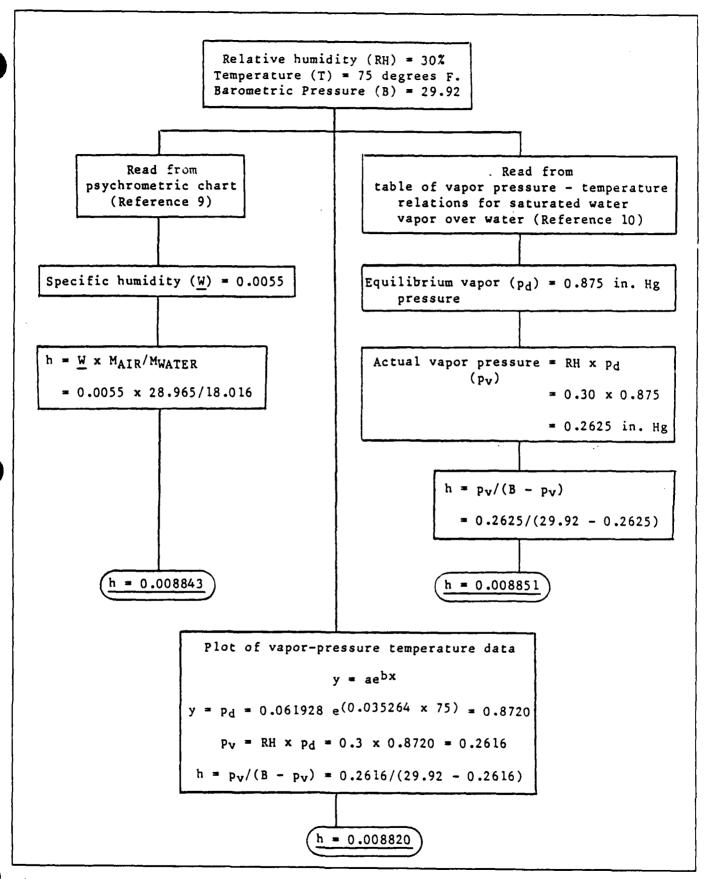


Figure 3-1. Calculation of the humidity of inlet air (h) as moles of water vapor per mole of dry inlet air.

3.4.2 Humidity of Inlet Air from Vapor Pressure-Temperature Tables

Likewise, many engineering handbooks contain tables of vapor pressure-temperature relations for saturated water vapor over water. Use these tables to read directly the equilibrium vapor pressure for any temperature. Multiplication of the equilibrium vapor pressure by the relative humidity ratio gives the actual vapor pressure (or vapor pressure at the dew point). The humidity of the inlet air (h) is the ratio of the actual vapor pressure to the air pressure, $h = p_v/(B - p_v)$.

For use in computer and calculator programs, the vapor pressure-temperature data needs to be expressed as an algebraic equation. Analysis of vapor pressure-temperature data from reference 10 using program CFIT from a Hewlett-Packard Advantage Advanced Solutions Pac showed that they fit the exponential equation

$$y = ae^{bx}$$

where y = vapor pressure (in. Hg), x = temperature (degrees F.), a = 0.053226 and b = 0.038251 (for temperatures below 50 degrees); a = 0.061928 and b = 0.035264 (for temperatures from 50 to 75 degrees); and a = 0.080455 and b = 0.031767 (for temperatures above 75 degrees).

The user of AESO computer and calculator programs enters either the humidity of the inlet air (h) or those data needed for its calculation. These data are (a) a combination of the relative humidity, dry bulb (ambient) temperature and barometric pressure, or (b) the dew point temperature (at which, by definition, relative humidity = 100%) and the barometric pressure. Figure 3-1. compares the values of h calculated by each of these methods with the value obtained from a psychrometric chart.

3.4.3 Humidity of the Exhaust Sample

The term h_{sd} is the humidity of the exhaust sample after leaving the gas dryer. The water content is reduced to about 1%. This Handbook uses a constant value of 0.00607 for h_{sd} . See SAE AIR 1533, page 34.

3.5 Nitric Oxide and Converter Efficiency

The oxides of nitrogen, in the exhaust from a gas turbine engine, are mostly in the form of nitric oxide with small amounts of other oxides of nitrogen, of which the principal one is nitrogen dioxide. Nitric oxide is the only oxide of nitrogen detected by the method of analysis (chemiluminescence). To determine the total concentration of the oxides of nitrogen, the nitrogen dioxide first must be converted to nitric oxide by heat or by ultraviolet irradiation. This conversion is not complete. The measured concentration of nitrogen dioxide (the concentration of the oxides of nitrogen minus the concentration of nitric oxide) must be divided by the efficiency of the converter to get the true concentration of nitrogen dioxide. This concentration of nitrogen dioxide, when added to the concentration of nitric oxide, gives the concentration of the oxides of nitrogen.

For those tests recording only the concentration of the combined oxides of nitrogen, this Handbook assumes that the oxides of nitrogen are 97% nitric oxide and 3% nitrogen dioxide. This is a realistic composition for high engine power settings, which are the ones producing most of the oxides of nitrogen and thus most affecting the emission index. If the efficiency of the converter is unknown, 95% is a reasonable estimate.

3.6 Oxygen

The concentration of oxygen can be measured, but its calculation either by using equation (78) of SAE AIR 1533, page 25, or by a matrix solution, is more convenient. In our measurements we found that the sensor of the oxygen analyzer needed frequent servicing or replacement.

3.7 Fuel Analysis

Fuel analysis determines the variables m and n (the molecular constants for the fuel $C_m H_n$). If m and n have not been determined by fuel analysis, this Handbook uses a hydrogen (n) to carbon (m) ratio of 2 for JP-4 fuel (n = 19.0 and m = 9.5) and 1.8 for JP-5, (n = 23.4, and m = 13.0)

3.8 Adjustments to Measured Concentrations

3.8.1 Adjustment for Carbon Dioxide in Ambient Air

Ambient air contains carbon dioxide and this concentration must be subtracted from the measured concentration of carbon dioxide in the exhaust, before calculating emission indexes. Some combustion equations and all matrix solutions include this correction. The calculations of all emission indexes use the concentration of carbon dioxide. So, failure to correct for ambient carbon dioxide affects all of the emission indexes.

3.8.2 Adjustments to Measured Concentrations for Instrument Interferences

All methods for the calculation of emission indexes adjustments to the measured concentrations of the constituents for (1) the interference of oxygen on the measured concentration of carbon dioxide, the interference of carbon dioxide, and water on the measured concentration of carbon monoxide, and (3) the interference of carbon monoxide and water on the measured concentration of the oxides of nitrogen. using linear equations, the measured concentrations must be adjusted before calculating the emission indexes. The matrix method allows the use of the measured concentrations with the instrument coefficients J, L, L', M and M' making the adjustments during the solution. The coefficient J adjusts the measured concentration of carbon dioxide for the interference of oxygen. The coefficients L and M adjust the measured concentration of carbon monoxide for the interferences of carbon dioxide and water. coefficients L' and M' adjust the measured concentration of the oxides of nitrogen for interferences of carbon dioxide and water.

SAE AIR 1533 describes how to use the instrument coefficients J, L, L', M, and M' to make adjustments but does not tell how to determine these coefficients other than by remarks such as "to be determined by experiment" or "from the vendor." SAE AIR 1533 (page 10) gives typical values for the interference coefficients L, L', M, and M'. These are the same as the ones determined for a specific instrument at the National Gas Turbine Establishment (Reference 8). SAE AIR 1533 (page 34) uses +0.09 as the value of J. Reference 8 states that -0.07 is the median value for J from a survey of users in the United Kingdom and in the United States. SAE AIR 1533 does not reference the source of the +0.09 value.

The following paragraphs describe how the Aircraft Environmental Support Office determines the instrument interference coefficients. We expect to modify these methods, as needed, to conform to anticipated standardization of methods.

3.8.3 Interferences to the Carbon Dioxide Measurement

The concentration of carbon dioxide needs adjustment for the interference of oxygen. The Aircraft Environmental Support Office has not determined the value of J for its carbon dioxide analyzer and will use J=-0.07 as an approximate value in calculations of emission indexes from our measurements. Elsewhere in this Handbook, however, examples of calculations use J=+0.09 to permit direct comparisons with the sample calculation of SAE AIR 1533, pages 34 - 36.

3.8.4 Interferences to the Carbon Monoxide Measurement

The mobile emissions laboratory of the Aircraft Environmental Support Office uses nondispersive infrared analyzers to determine the concentrations of carbon monoxide and carbon dioxide. The same gas stream passes through both instruments. Concentrations of carbon dioxide and water change the output from the carbon monoxide analyzer even though there is no carbon monoxide in the gas stream. These outputs appear as positive deflections of the recorder trace, from the zero calibration of carbon monoxide, and must be subtracted from the measured values of carbon monoxide.

The amount of the deflection also depends upon the characteristics of the optical system of the infrared analyzer. Some analyzers use filters to eliminate most of the interferences from carbon monoxide and water. With proper filters, the adjustments to the measured concentrations for the presence of carbon dioxide and water are small, causing less change in the emission indexes than the change expected from variations in instrument performance.

3.8.5 Determination of L

To determine L, we passed samples containing various known amounts of carbon dioxide in nitrogen through the carbon monoxide analyzer. Each sample caused a positive response from the analyzer which was equated to a concentration of carbon monoxide in parts per million.

The carbon monoxide analyzer, used in the first measurements by the Aircraft Environmental Support Office, did not have filters to decrease the interferences from carbon dioxide and water. A calibration gas containing 1% of carbon dioxide caused the same response in the carbon monoxide analyzer as a carbon monoxide concentration of 9 ppm. For a calibration gas containing 3.04% carbon dioxide, this response was equal to 18 ppm of carbon monoxide or 6 ppm for each 1% of carbon dioxide. This instrument soon was modified with filters. Filters reduced the response to that equal to about 1 ppm of carbon monoxide for each 1% of carbon dioxide.

In equation (13) of SAE AIR 1533, the term $L[CO_2]$, when the concentration of carbon dioxide is 1%, must have a value which decreases the measured concentration of carbon monoxide by 9 ppm. Thus, $L[CO_2] = -0.000009$. Thus, $L \times 0.01 = -0.000009$, or L = -.0009. Using a similar calculation, the value of L at 3% carbon dioxide is -0.0006, i.e., (L $\times 0.03 = -0.000018$). For adjustments without filters, the Aircraft Environmental Support Office uses L = -0.0009 for carbon dioxide concentration to 1.2%, L = -0.0008 for concentrations from 1.2 to 1.8%, L = -0.0007 for concentrations from 1.8 to 2.5% and, L = -0.0006 for concentrations above 2.5%. For measurements made with filters, $L \times .01 = -0.000001$ and L = -0.0001.

3.8.6 Determination of M

To determine M, we passed ambient air through a cooling bath (water-ethylene glycol regulated at zero degrees F by refrigeration) to condition the air to a semi-dry basis. We assume that now $[\rm H_2O]$ = h = 0.00607. Using our infrared analyzer without filters, the instrument response varied. The deflection was the same as that caused by 13 ppm to 40 ppm of carbon monoxide. Filters reduce this response to a deflection which was the same as that caused by about 2 ppm of carbon monoxide. Because of variation in the response of the infrared analyzer to ambient air, each test made using the infrared analyzer without filters uses its own value for M.

Just as previously described for L, the calculation of M uses the term $M[H_2O]$ from equation (13) of SAE AIR 1533. For example $M[H_2O]$ = -0.000013. Then, if $[H_2O]$ is 0.00607, M = -0.000013/0.00607 = -0.00214 or, -0.00659 for the interference equivalent to 40 ppm. With filters, M = -0.000002/0.00607 = -0.00033.

3.8.7 Interferences to the Oxides of Nitrogen Measurement

The Aircraft Environmental Support Office has not determined values for L' and M' for any of the three different NO_X analyzers used in our measurements. We will use L' = 0.14 and M' = 0.28 as approximate values.

4 CALCULATION OF EMISSION INDEXES

The efficient calculation of emission indexes, using linear equations, needs a programmable calculator. The calculation, using the matrix method, needs a computer. This section shows how to use both calculators and computers to determine emission indexes. The calculator and computer programs feature print-outs which record the variables used and the parameters calculated. With adjustment to the measured concentrations of the constituents for humidity, instrument interferences and converter efficiency, the calculator program gives the same emission indexes as the computer program. The adjustments to the measured concentrations, although correct technically, cause only slight changes in the emission indexes.

4.1 Molecular Weights

The calculation of an emission index needs a molecular weight for the constituent of the emission index. For carbon monoxide and carbon dioxide there is but one constituent, and the molecular weight is the same as the formula weight.

For the oxides of nitrogen the composition is mostly nitric oxide with small amounts of nitrogen dioxide. By convention, the emission index for the oxides of nitrogen is calculated as if there were a single oxide, namely nitrogen dioxide.

For hydrocarbons, there are many constituents. The formulas and molecular weights used for the calculation of this index are CH, 13.019 (Reference 4); $\text{CH}_{\text{y/x}}$, usually 13.825 or 14.027 (References 1, 5 and 7); and CH₄ (methane), 16.043 (References 3 and 8). This Handbook uses the notation $\text{CH}_{\text{y/x}}$ to indicate [M_C + (y/x)(M_H)]. Assuming hydrogen to carbon ratios (y/x) of 2.0 for JP-4 fuel and 1.8 for JP-5, the molecular weight of hydrocarbons is 14.027 (equivalent to CH₂) for JP-4 and 13.825 (equivalent to CH_{1.8}) for JP-5.

In calculations from AESO data, the tables of this Handbook give emission indexes for hydrocarbons as if the constituent was either $CH_{y/x}$ or CH_4 . When recording data from other sources, this Handbook uses the hydrocarbon emission index as reported. To convert between hydrocarbon emission indexes, multiply by the appropriate ratio of molecular weights. For example, to convert $EI(CH_4)$ to $EI(CH_2)$, multiply by 14.027/16.043. To convert $EI(CH_4)$ to $EI(CH_3)$, multiply by 13.019/16.043.

4.2 Calculation of Emission Indexes Using Linear Equations

The simplest method for the calculation of an emission index uses a linear equation such as equations (1) or (2) of Figure 4-1. (References 3, 4, and 5). Note that Reference 3 gives an equation for the calculation of the "CO emission rate." This equation includes the terms of equation (1) which calculate an emission index. Reference 3 does not identify these terms as an emission index. Equations (1) and (2) differ from one

$$EI_{z} = \left(\frac{[z]}{[CO] + [CO_{2}] + [C_{x}H_{y}]}\right) \left(\frac{10^{3} M_{z}}{MC + \alpha MH}\right)$$
(1)

$$EI_z = \left(\frac{[z]}{[CO] + [CO_2] + [C_XH_Y] - T}\right) \left(\frac{10^3 M_z}{M_C + \alpha M_H}\right)$$
 (2)

$$EI_{z} = \left(\frac{[z]}{[CO] + [CO_{2}] + [C_{x}H_{y}]}\right) \left(\frac{10^{3} M_{z}}{M_{C} + \alpha M_{H}}\right) (1 + TX/m)$$
(3)

[z] is the mole fraction concentration of a constituent z of the exhaust, specifically the mole fraction concentration of carbon monoxide, carbon dioxide, oxides of nitrogen (as nitrogen dioxide) or hydrocarbons (as CH_y/x or as methane). Note that z is not the same as the variable Z which is defined by equation SAE AIR 1533 (59), page 22.

 M_z is the molecular weight of the constituent, specifically: carbon monoxide (28.0104); carbon dioxide (44.0098); nitrogen dioxide (46.0055); CHy/x (14.027, when y/x = 2); or methane (16.043).

Mc is the atomic weight of carbon (12.011).

MH is the atomic weight of hydrogen (1.008).

a is the hydrogen-carbon ratio of the fuel, which is about 2 for JP-4 and about 1.8 for JP-5.

T is the mole fraction of carbon dioxide in the dry inlet air (0.00032).

X is the number of moles of dry air per mole of fuel in the initial air fuel mixture. For the determination of X/m use equations 60 and 61 of SAE AIR 1533, page 22.

m is the molecular constant for carbon in the fuel $C_m H_n$.

Figure 4-1. Combustion equations for the calculation of emission indexes.

another only in that equation (2) subtracts the concentration of carbon dioxide in ambient air (T) from the measured concentration of carbon dioxide. These equations can be solved with a simple calculator, or even without one. References 1 and 8 derived equation (3) from products of the matrix solution of simultaneous combustion equations. Equation (3) is more complicated to solve than equations (1) or (2) because it needs the calculation of X/m. Its solution with a simple calculator is tedious, but becomes easy with a programmable calculator. The emission indexes calculated by equations (2) and (3) are the same when the user adjusts the concentration of the constituent for the effects of humidity, instrument interferences and converter efficiency

4.3 Calculation of Emission Indexes by the Matrix Solution of Combustion Equations

The optimum method (Reference 1) for the calculation of emission indexes uses a comprehensive matrix solution of ten simultaneous equations describing the chemical combustion of a hydrocarbon fuel. This method should be used whenever feasible. As already mentioned, the user of this Handbook must refer to SAE AIR 1533 for the derivation of the matrix from the combustion equations and the modification of the basic matrix to the comprehensive matrix.

The matrix method has the advantage over the use of linear equations in that it develops, in a single solution, values of P, (P_1-P_8) , P_T and X. This list is the P vector. The values in the P vector allow the calculation of all of the emission indexes of the constituents as well as the wet and dry concentrations of the constituents of the exhaust and other parameters needed in combustion studies. The matrix method needs a computer for its solution. Although solution of a size 10 matrix using a small calculator is possible, it is not practical because of the time needed for the inversion of the matrix. The computer program for the matrix solution needs, as input, the measured concentrations of the conituents, the humidity terms needed to adjust them, and the instrument interference coefficients.

4.4 Aids for the Solution of Linear Equations and the Matrix

4.4.1 Solution of Linear Equations Using a Programmable Calculator

Appendix A, which contains selected pages from Reference 12, gives instructions and programs for the use of a small programmable calculator to solve equations (2) and (3) of Paragraph 4.2. Figures Al-1 to Al-5 give examples of the calculations needed to adjust the measured concentration of the constituents, and to determine the emission indexes, the fuel to air ratio and the combustion efficiency. These examples use the data of the sample calculation of SAE AIR 1533. Programs AIRAP AIRA use equation (3). Program AIRB uses equation (2). Program AIRAP makes a permanent record of the data entered and calculated. Program AIRA uses the same data as program AIRAP but shows the calculations only in the display of the calculator. Program AIRB is satisfactory for estimates especially when nothing is known about the quality of the data or the adjustments to the measured concentrations. With adjustments for

instrument interferences and humidity, however, program AIRB, gives values which are very close to, or sometimes the same as, those obtained by equation (3). Like Program AIRA, program AIRB shows the calculations only in the display of the calculator.

4.4.2 Solution of the Matrix Using a Computer

Appendix B lists two computer programs MATEI (MATrix Emission Index and SAMPFL (SAMPle FiLe). Both programs are in BASIC language for an IBM PC AT or XT computer (or IBM PC compatible computers).

The program MATEI uses the matrix solution of Table C-1 of SAE AIR 1533, page 38, written in BASIC instead of FORTRAN. If a computer has a library of matrix functions, BASIC commands such as MAT I = INV(A): MATI1 = I*A: MAT P = I*F can replace lines 120 - 410 of Table C-1. Program MATEI adds, to the program in table C-1, the many steps needed to get the data to the matrix and print the calculations from it. The user of program MATEI has the option of entering data from a preassembled file or adding it to the program in response to inquiries on the monitor. Program MATEI uses either an IBM Proprinter or a Hewlett-Packard printer. An option of Program MATEI, uses a LaserJet printer with a T font to add lines to the print-out. For the preparation of the data sheets in this Handbook, the Aircraft Environmental Support Office used an enhanced version of program MATEI, namely MATEIE. This program uses two additional fonts, Prestige Elite and Math 8, to change the style of the print-out. The calculations from both programs are the same.

Program SAMPFL explains how to prepare a data file for use with program MATEI. Each file has a unique name. Each file represents a specific power setting for a specific engine.

Appendix B includes: (a) Figure Bl which lists the 100 elements of the comprehensive matrix using the data of the sample calculation of SAE AIR 1533, (b) Figure B2 which shows the matrix constant, the P vector; and (c) Figure B3 which gives specific examples of calculations using the P vector. The values in the P vector (Figure B2) are the same as those of the P vector reported by SAE AIR 1533. These figures are references for anyone installing the matrix solution on a computer system.

4.5 Print-outs from Computer and Calculator Programs

4.5.1 Print-outs from the Computer Program MATEIE

Figures 4-2 and 4-3 show the print-outs from Program MATEIE. The purpose of the print-out is to make a data sheet which shows the original data used in the matrix, records calculations from the P vector of the matrix and gives information about the engine test. Each data sheet describes gaseous emissions at a single power setting for a specific engine. Lines group the data sheet into blocks, which are identified by letters. For comparison with SAE AIR 1533, Figure 4-2 shows the data sheet prepared by Program MATEIE using the data of the sample calculation of SAE AIR 1533. Figure 4-3 shows the data sheet for an engine run which includes engine operation data and the measurement of oxygen.

A	SAE	SAMPLE CALCULATION	File SAE	
8	J - 0.09 L0.0001 L' - 0.14 M0.00045 M' - 0.28	h = 0.008843 h _{sd} = 0.00607	m = 9.5 n = 19.0 η = 0.95	
	CONSTITUENT	EXHAUST CONCENT	TRATION alculated semi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	2.00 sd 2.045 ppm 20 w 21.42 ppm 9 w 9.37 ppm 12.05	9.31 9.10 11.98 11.70 230.3 225.0 17.979 17.569	47.65 3076.41 3.37 1.47 1.90 11.11 12.71
D	Sulfur dioxide, calc.			0.40
Ε		oxygen, calc.(ppm wet) oxygen, meas.(ppm wet)	110	
F	K = 0.9713 F/A = 0.009998 Combustion efficiency =	97.78%		
G				
Ħ	Measurement by N/A Measurement at SAE AIR Date of measurement N/ Engine S/N N/A	- -		

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Figure 4-2. Computer print-out of the data sheet for the gaseous emissions from an engine using the data of the sample calculation of SAE AIR 1533.

A	T56-A-16	MILITARY		File T56001M			
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.86 in. h = 0.008884 h = 0.00607		m - 13.0 n - 23.4 η - 0.95			
	CONSTITUENT		dry s	IION ulated emi- wet dry	EMISSION INDEX		
c	Carbon monoxide ppp Carbon dioxide % Oxides of nitrogen ppp Nitric oxide ppp Nitrogen dioxide ppp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.21 sd n 67.1 sd n n nC 2.9 w	2.20 67.9 65.8 65.8 2.1 3.0	6.9 6.8 2.18 2.13 7.5 66.1 5.4 64.0 2.1 2.1 3.0 2.9 7.90 17.51 9.30 77.58 2.77	0.65 3229.31 10.45 10.12 0.33 0.14 0.16		
D	Sulfur dioxide, calc.				0.40		
ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			345 318			
F	K = 0.9723 F/A = 0.010231 Combustion efficiency = 99.97% Shaft horsepower = 4090 Engine speed = 13820 rpm Engine exhaust temperature = 1970°F						
G	EMISSION RATE (pounds of for a fuel flow rate of 2 Carbon monoxide Carbon dioxide 7 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	219 pounds per hour 1.45 165.85 23.18	-				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 23 J Engine S/N 102138 Test Cell 11, single poin JP-5 fuel.	RKFAC ALAMEDA UNE 1976		stack.			

AESO 09-30-1987

Figure 4-3. Computer print-out of the data sheet for the gaseous emissions from a T56-A-16 engine at military power.

Block A - A header shows

- (1) the engine type indicator, type numerals, manufacturer's symbols and model indicator,
- (2) the engine power setting, and
- (3) the name of a data storage file.

The first three or four characters of the file name identify the engine type (e.g., T56, J79, F404). The next three characters, which usually are numbers or letters, give a unique designation to a group of power settings such as those used in the testing of an engine. A final letter indicates the power setting: I for idle; N for normal rated; X for maximum continuous; M for military, intermediate rated power, or takeoff; A for afterburner; B, C, D and other letters as needed, for power settings between idle and military. The AESO data sheets use the same identification of the power setting as recorded on the engine operational records at the place of the measurement. No print-out of a file name indicates that the computer program prepared the data sheet from entry of data into the program in response to inquiries appearing on the computer monitor.

Block B - This block has three groups of data.

The first group shows the instrument interference coefficients used in the calculation. A blank space means that matrix solution did not use instrument interference coefficients to adjust the measured concentrations of the constituents.

The second group shows terms related to humidity adjustments, namely,

- (1) the ambient (dry bulb) temperature (T),
- (2) the relative humidity (RH) (or the dew point temperature),
- (3) the barometric pressure (B),
- (4) the humidity of the inlet air (h), and
- (5) the humidity of the exhaust sample (h_{sd}) . For measurements giving a dew point temperature, the word 'DEW' replaces T and RH on the data sheet.

The third group of data shows the molecular constants of the fuel and the efficiency of the nitrogen dioxide/nitric oxide converter. Fuel analysis determines the molecular constants. Typically, the hydrogen (n) to carbon (r) ratio is about 2 for JP-4 fuel (n = 19 and m = 9.5), and about 1.8 for JP-5 fuel (n = 23.4 and m = 13.0).

Block C - For the constituents of the exhaust, a table shows the measured concentrations, the calculated dry, semi-dry and wet concentrations, and the emission indexes.

A notation after a measured concentration show the basis of the measurement, 'sd' for semi-dry and 'w' for wet. If the measurements did not include one for nitric oxide, the corresponding space is blank. The concentration of nitrogen dioxide is not measured. The matrix solution needs a value for the concentration of nitric oxide. If not measured, the computer program sets the concentration of nitric oxide at 97% of the concentration of the oxides of nitrogen. The calculation of the emission index from either of the hydrocarbon molecular weights uses the same concentration of hydrocarbons.

The matrix solution determines the values of the concentrations of the constituents and the emission indexes. Figure B3 of Appendix B shows details of these calculations. The matrix solution does not need the measured concentrations of oxygen, nitrogen and water. Some emission measurements include one for oxygen. If not measured, the corresponding space is blank.

Block D - The sulfur content of the fuel determines the emission index of sulfur dioxide. Sulfur appears in the exhaust mainly as sulfur dioxide. Although the emission index for sulfur dioxide can be calculated from a measured concentration, it is more convenient to calculate it from the sulfur content of the fuel. An aircraft fuel, such as JP-5, may contain as much as 0.4% of sulfur. Normally it contains about 0.02% (Reference 11). We assume that the entire sulfur content of the fuel is converted into sulfur dioxide at all power settings. Thus, for a fuel with a sulfur content of 0.02%, 1000 pounds of fuel contains 0.2 pounds of sulfur which is converted into 0.4 pounds of sulfur dioxide. The emission index for sulfur dioxide, at all engine power settings, is 0.40.

Block E - To have a uniform basis for the comparison of sources, some regulating agencies need to know the concentration of the oxides of nitrogen at an oxygen content other than the one measured. The following equation shows the conversion to a basis of 3% oxygen. Any concentration of oxygen may be substituted for the 3% concentration.

[NO_X] at 3% oxygen = [NO_X]_m x
$$\frac{\text{oxygen in air } (\%) - 3\%}{\text{oxygen in air } (\%) - \text{oxygen in sample } (\%)}$$

where $[NO_X]_m$ is the measured concentration (ppm) of the oxides of nitrogen and the oxygen content of air is 20.948%. Then, adjusting a measured concentration of 66.1 ppm oxides of nitrogen in a sample containing 17.51% oxygen to a concentration in a sample with oxygen content of 3%:

$$[NO_x]$$
 at 3% oxygen = 66.1 x $\frac{20.948 - 3}{20.948 - 17.51}$ = 345 ppm.

Block E gives two values for the concentration of the oxides of nitrogen (wet basis) at 3% oxygen, one from the calculated concentration of oxygen and the other from the measured concentration of oxygen. The calculation from the measured concentration of oxygen first changes the concentration to a wet basis using the value of K from block F. For example, using equation (58) of SAE AIR 1533,

 $[0_2]_w = K \times [0_2]_{sd} \times (1 + h_{sd})$

 $[0_2]_w = 0.9723 \times 17.6 \times 1.00607 = 17.22.$

Block F - The entries in this block give the constant K, the fuel to air ratio and the combustion efficiency, as calculated by the matrix solution; and the thrust (or shaft horsepower), engine speed and engine exhaust temperature as reported in the engine operation records. Emission index calculations do not use engine speed or engine exhaust temperatures. In this Handbook the term engine exhaust temperature means the temperature, associated with the engine exhaust gas, as reported by the testing facility. For example this temperature may be the exhaust gas temperature for a J79 engine, but the turbine inlet temperature (T5) for a TF41 engine. The calculation of emission indexes may use a plot of thrust (or shaft horsepower) vs. emission index. See Paragraph 6.3.

Block G - After determining the emission indexes, the AESO computer program determines the emission rates using the emission indexes from Blocks C and D, and the fuel flow rates. If the data did not include fuel flow rates there is no calculation of emission rates and the corresponding space is blank. The emission rate of the pollutant is obtained by multiplying the fuel flow rate (in thousands of pounds) by the emission index. Note that the computer uses the emission index as a single precision number in calculating the emissions rates. The tables give the emission indexes rounded to two decimal places. This means that multiplying the emission index on the data sheet by the fuel rate may give a slightly different emission rate from the one recorded on the data sheet.

 $\underline{Block\ I}$ - The reference part of the print-out tells who made the measurement, where and when, the engine serial number, the type of fuel used and optional information.

The date at the bottom of the sheet is 09-30-87 for all data sheets included in the first printing of this Handbook. Data sheets added after the first printing will show a later date.

4.5.2 Print-outs from Calculator Programs

Figure 4-4 shows print-outs from the calculator program AIRAP. These show only the most important emissions data. The instructions, in Appendix A, for program AIRAP explain the content of each line of the print-out. The user who needs additional print-out should modify the program.

0.09 -1.30-04 0.14	-0.07 -1.00-04 0.14
-4.50-04 0.23	-3.30-04 0.28
9.5 19.0 0.008843	13.0 23.4 9.998884
0.98697 9.95	0.00607 0.95
500.0 2.00 20.0 9.0 225.0	15 97 29.86
EI	11.1 2.21 67.1 65.1
00 = 47.65	2.9 FUEL = 2219.0
CO2 = 3076.41	ΕΙ
HOX = 3.37 CXHY, CHY/X = 11.11	co = 9.65
CXHY, CH4 = 12.71	002 = 3229.32
	NOX = 10.45
CO WET = 483.3	CXHY, CHY/X = 0:14 CXHY, CH4 = 0:16
CO2 WET = 1.986 NOX WET = 20.8	CART) CRY - 0:10
CXHY WET = 225.0	CO WET = 6.8
3 ,	CO2 WET = 2.135
% OXYGEN, WET = 17.57	NOX WET = 66.1 CXHY WET = 2.9
NOX AT 3% 02 = 111 WATER ≈ 2.87%	CART WET - 2.9
F/A = 0.009998	% OXYGEN, WET = 17.51
COMB. EFF. = 97.78%	HOX AT 3% 02 = 345
	WATER = 2.77% F/A = 0.010231
	COMB. EFF. = 99.97%
	POUNDS PER HOUR
	CO = 1.45
	CO2 = 7165.86
	HO2 = 23.18 CHY/X = 0.31
	CH4 = 0.35
	S02 = 0.89

SAE AIR 1533 military power compare with Figure 4-2 compare with Figure 4-3

T56-A-16

military power

Figure 4-4. Print-outs from program AIRAP.

Sample calculation SAE AIR 1533

4.6 Comparison of Calculations by Computers and Programmable Calculators

Table 4-1 compares the values of emission indexes determined by computers and programmable calculators. The difference in precision between the computer, used for the matrix solution, and the calculator, used for the solution of linear combustion equations, cause the small variations in the emission parameters. For practical use, the determinations by computers and programmable calculators are equivalent.

4.7 The Effect of Adjustments to Measured Concentrations on Emission Indexes

Table 4-2 shows how combinations of adjustments, to the measured concentrations of the constituents of an engine exhaust, affect the emission indexes. These adjustments are for the pressure broadening coefficient (J), the instrument interference coefficients (M, M' L, L'), the humidity (h and h_{sd}), the efficiency of the nitrogen dioxide to nitric oxide converter (η), and the ambient carbon dioxide concentration (T). Table 4-2 uses the data from the sample calculation in SAE AIR 1533 and the comprehensive matrix solution. An asterisk in a column indicates that the variable is at the value used in the sample calculation (for T this value is 0.00032). A zero in a column indicates a value of zero for J, L, L', M, M', h, h_{sd}, η , or T. For the converter efficiency, a zero means no correction, i.e., 100% efficiency.

Row 1 of Table 4-2 makes all of the adjustments to the measured concentrations and thus gives the emission indexes of the sample calculation. Other rows change one or more of the variables. For example, row 11 uses all of the instrument coefficients at zero. Row 23 makes none of the adjustments. Rows 14 and 15 compare the change in the emission index for the oxides of nitrogen when the converter efficiency is 95% or 100%. Obviously, only the emission index for the oxides of nitrogen changes. Rows 20, 21 and 22 show the effect when the water content of the inlet air varies.

The values of the instrument coefficients, J, L, L', M and M' are ones expected for infrared analyzers with filters in the optical system to suppress the effects of the interfering gases. For such analyzers, Table 4-2 shows that adjustments to measured concentrations of the constituents for humidity, instrument interferences and converter efficiency have only a small effect on the calculated emission indexes.

Table 4-1. Examples of emission indexes calculated from computer and calculator programs using the data of the sample calculation from SAE AIR 1533

Constituent	Emission index AE AIR 1533 sample	•	Emission index uter or calculator program (method of calculation)		-
	calculation (page 34)	MATEI (matrix)	AIRAP (eqn. 3) ^a	AIRB (eqn. 2)b	AIRB (eqn. 2) ^c
Carbon monoxide	47.66	47.65	47.65	47.66	48.93
Carbon dioxide	3076.41 ^d	3076.41	3076.41	3077.34	3075.23
Oxides of nitrogen	3.37	3.37	3.37	3.37	3.21
Hydrocarbons $(CH_{y/x})$	11.11	11.11	11.11	-	-
Hydrocarbons (methano	e) 12.71 ^e	12.71	12.70	12.71	12.61

^a Program AIRAP uses the measured concentrations as inputs and adjusts them for the effects of humidity, instrument interference coefficients and the efficiency of the NO_X converter before calculating the emission indexes using equation (3) of Figure 4-1.

b Program AIRB uses equation (2) of Figure 4-1. In this example, before using equation (2), use equations (13), (14), (18), (20), and (58) of SAE AIR 1533 to adjust the concentrations of carbon monoxide, carbon dioxide and the oxides of nitrogen to a wet basis. The wet concentrations are: carbon monoxide, 483.3 ppm; carbon dioxide, 1.986%; oxides of nitrogen, 20.8 ppm. The hydrocarbon concentration (225 ppm) is measured on a wet basis and needs no adjustment. See Figures Al-1, Al-2 and Al-4 of Appendix A for details of these calculations.

The emission indexes in this column come from the direct substitution of the measured concentrations into equation (2) without any adjustments, i.e, carbon monoxide, 500 ppm; carbon dioxide, 2%; oxides of nitrogen, 20 ppm and hydrocarbons, 225 ppm.

d SAE AIR 1533 does not report this calculation. It was calculated using P₁ from the list of P vectors on page 35 of SAE AIR 1533.

 $^{^{\}rm e}$ SAE AIR 1533 does not report this calculation. It was calculated from equation (48) of SAE AIR 1533 and P₆ from the list of P vectors on page 35 of SAE AIR 1533.

Table 4-2. Effect of adjustments to concentrations on emission indexes

Row	J	L	L'	M	M f	h	h _{sd}	η	T	Emission indexes			
no.										СО	CO ₂	NOX	CH4
1	*	*	*	*	*	*	*	*	*	47.65	3076.41	3.37	12.71
2	0	*	*	*	*	*	*	*	*	48.41	3075.43	3.42	12.90
3	*	0	*	*	*	*	*	*	*	47.90	3076.02	3.37	12.70
4	*	*	0	*	*	*	*	*	*	48.65	3076.41	3.36	12.71
5	*	*	*	0	*	*	*	*	*	47.91	3076.01	3.37	12.70
6	*	*	*	*	0	*	*	*	*	47.65	3076.41	3.34	12.71
7	*	0	*	0	*	*	*	*	*	48.16	3075.61	3.37	12.70
8	*	*	0	*	0	*	*	*	*	47.65	3076.41	3.33	12.71
9	0	0	*	0	*	*	*	*	*	48.92	3074.64	3.42	12.90
10	0	*	0	*	0	*	*	*	*	48.41	3075.44	3.38	12.90
11	0	0	0	0	0	*	*	*	*	48.92	3074.63	3.38	12.90
12	0	0	0	0	0	0	*	*	*	48.93	3074.93	3.35	12.79
13	0	0	0	0	0	*	0	*	*	48.92	3074.72	3.40	12.98
14	0	0	0	0	0	0	0	*	*	48.93	3075.02	3.37	12.87
15	0	0	0	0	0	0	0	1	*	48.93	3075.02	3.28	12.87
16	0	0	0	0	0	*	*	*	0	48.17	3075.60	3.33	12.70
17	0	0	0	0	0	0	0	*	0	48.17	3075.94	3.32	12.67
18	0	0	0	0	0	*	*	1	*	48.92	3074.63	3.29	12.90
19	*	*	*	*	*	0	*	*	*	47.66	3076.70	3.33	12.60
20	*	*	*	*	* (0.005	5 *	*	*	47.66	3076.54	3.35	12.66
21	*	*	*	*	* (0.01	*	*	*	47.65	3076.37	3.37	12.72
22	*	*	*	*	* (0.015	5 *	*	*	47.65	3076.20	3.39	12.78
23	0	0	0	0	0	0	0	1	0	48.17	3027.08	3.23	12.67

5 EXAMPLES OF VARIATIONS OF EMISSION INDEXES

An emission index is not constant. An emission index varies during the operation of an engine at a power setting, especially as the engine is coming to a stable operating condition. An emission index varies for the same power setting at different times in a sequence of power settings, or among engines of the same type and model. Also both the performance of the instruments and the interpretation of the original data affect the emission index. This section uses examples of specific engine tests to show the variations of emission indexes (1) when sampling at the same position by two different laboratories, (Table 5-1), (2) when sampling at two different positions by two different laboratories (Table 5-2) and when ampling at two different position by the same laboratory (Table 5-3). This section also compares engine emissions with and without a ferrocene additive in the fuel (Table 5-4).

5.1 Variation of Gaseous Emissions at a Sampling Position

Table 5-1 shows the variations of emission indexes calculated from measurements by the mobile emissions laboratories of the Aircraft Environmental Support Office (AESO) and the Federal Aviation Administration (FAA). In this test a T58-GE-8F engine ran at various power settings during a three-day period. Samples from the test cell came from the point in the exhaust stack through separate sample lines to each laboratory. For each power setting, a test-coordinator, in the test cell control room, announced one-minute read periods. These periods corresponded to intervals of stable engine operation, as specified by the operators of the engine. Each laboratory reported emission indexes for the read period. The test established 50 read periods for gaseous emissions. Table 5-1 gives the emission indexes at idle, high idle, approach, cruise and maximum continuous as determined by each laboratory, during 44 of the read periods. The FAA Laboratory did not measure at the takeoff power setting.

The data from this test, as reported in Reference 14, needed interpretation before they could be used for the comparison in Table 5-1. The test plan specified that each Laboratory report the concentrations of the constituents on a wet basis. The matrix solution for the emission index uses the concentrations of carbon monoxide and carbon dioxide on a semi-dry basis. For AESO data we used our original measurements which were stated on a semi-dry basis. For FAA data we adjusted the wet measurements to semi-dry using the values of K determined for each corresponding AESO measurement.

The test plan did not address the question of the adjustment of measured concentrations for instrument interferences prior to use in the calculation of the emission indexes. The calculations for Table 5-1 use the instrument interference coefficients for the AESO laboratory to adjust all concentrations. These modifications have little effect on what Table 5-1 shows, i.e., that emission indexes vary.

Finally, the test plan specified that participants use the vendor's certification for the concentration of each calibration gas. In Table 5-1, the AESO emission indexes for the oxides of nitrogen reference the measured concentrations to Standard Reference Materials 1683 and 1684 of the National Bureau of Standards (46.0 and 93.9 ppm nitric oxide in nitrogen) rather than to the vendor's certification.

5.2 Emission Indexes at Different Sampling Positions

Tables 5-2 and 5-3 compare the measured concentrations of the constituents and the calculated emissions data from sampling at two different positions. In Table 5-2 two different laboratories measured at different positions in the exhaust stream from a J52-P-6B engine. In Table 5-3 the same laboratory measured at two different positions in the exhaust stream of a T64-GE-7 engine.

In Table 5-2, the measuring position used by Scott Environmental Technology was at the exhaust plane of the engine and the measuring position of the Aircraft Environmental Support Office was in the test cell stack, 85 feet behind the engine exhaust plane. Each group used its own set of instruments. There was no correlation of read points. Each Laboratory reported one set of values for each power setting.

Table 5-2 shows that, as expected, the fuel to air ratio (F/A) is higher at the engine exhaust plane than in the test cell stack. Thus, the measured concentrations of the constituents are much higher in the Scott measurements. The next group of data in this table show that expressing the emissions as emission indexes and emission rates brings the values of the two sets of data close to one another.

These comparisons show that for estimates, the measurement of the emission index may be at the exhaust plane of the engine or elsewhere in the exhaust stream.

Table 5-3 continues this comparison using a measurement in which the Aircraft Environmental Support Office changed the sampling position by moving the sampling line, during operation at each of the power settings, between two sampling positions in the exhaust stream.

5.3 Effect of Ferrocene on Gaseous Emissions

Table 5-4 shows how the addition of ferrocene to JP-5 fuel changes the gaseous emissions from a J79-GE-8B engine. To make the calculations for Table 5-4, the Aircraft Environmental Support Office observed the effect of ferrocene on the concentrations of the gaseous emission. During the engine run, a solution containing ferrocene was pumped into the main fuel line while the engine was operating at all power settings above idle. At each power setting, the flow of the ferrocene solution was stopped for about one minute, then resumed. Chart recorders noted the change in the concentration of each constituent.

Table 5-1. Variation of emission indexes from a T58-GE-8F engine

Test Cell - 12

Location - Naval Air Rework Facility, North Island

IDLE

Date	Time	Reading	Prior	Emission index							
June		number	power setting	Carb	on	Oxide	sof	Hydroc	arbons		
1979				monox	ide	nitro	gen	(as me	thane)		
				AESO	FAA	AESO	FAA	AESO	FAA		
				104 40	101 77		2.50		160.00		
5	1015	17	-	186.62	181.77	1.21	3.50	173.93	169.22		
5	1225	27	ΗI	183.01	174.01	1.36	2.66	159.11	147.20		
6	0833	28	I	175.95	175.23	1.19	2.51	151.46	155.15		
6	0930	34	ΗI	173.19	178.02	1.42	2.54	147.65	143.02		
6	1033	40	TO	182.50	188.33	1.40	2.68	146.88	143.36		
7	0806	54	I	177.75	172.90	1.22	2.07	159.35	149.13		
7	0939	64	HI	170.43	167.61	1.35	2.40	138.68	130.54		
7	1155	65	I	178.44	170.70	1.43	2.39	151.34	141.55		
7	1315	71	НI	172.77	170.47	1.47	2.55	136.60	129.09		
7	1412	77	то	176.69	172.43	1.40	2.20	136.50	129.26		

HIGH	IDLE
nica	INTE

Date	Time	Reading	Prior		Emission index							
June		number	power	Carb	on	Oxide	s of	Hydroc	arbons			
1979			setting	monox	ide	nitro	gen	(as me	thane)			
				AESO	FAA	AESO	FAA	AESO	FAA			
			_									
5	1050	81	I	165.20	166.01	1.30	3.35	113.16	109.00			
5	1215	26	AP	161.22	155.22	1.58	2.50	102.05	94.72			
6	0927	33	AP	150.00	157.44	1.64	2.42	93.07	87.38			
6	0955	35	I	153.04	159.31	1.65	2.57	96.37	92.11			
6	1041	41	I	155.79	156.42	1.82	1.44	102.21	87.71			
7	0815	55	I	152.36	151.68	1.62	2.37	97.09	92.69			
7	0927	63	AP	147.12	149.48	1.57	2.39	86.15	80.57			
7	1310	70	AP	145.25	150.90	1.69	2.47	84.63	80.63			
7	1325	72	I	150.82	146.54	1.65	2.03	85.94	82.04			
7	1427	78	I	152.43	152.27	1.63	2.27	89.45	85.60			

NOTE: Code for prior power setting: I - idle, FI - high idle, CR - cruise, AP - approach, MC - maximum continuous, TO - takeoff.

Table 5-1. Variation of emission indexes from a T58-GE-8F engine (continued)

Test Cell - 12 Location - Naval Air Rework Facility, North Island

APPROACH

Date	Time	Reading	Prior		1	E <u>missi</u> on	index		
June 1979		number	power setting	Carbon monoxide		Oxides of nitrogen		Hydrocarbons (as methane)	
				AESO	FAA	AESO	FAA	AESO .	FAA
5	1100	19	ні	15.72	16.57	3.98	4.36	2.02	1.49
5	1200	25	CR	15.91	16.76	4.37	4.60	1.34	0.79
6	0915	32	CR	16.15	17.47	4.52	4.63	0.94	1.04
6	1000	36	HI	17.79	18.88	4.67	4.81	1.47	1.58
7	0823	56	HI	17.28	17.68	4.47	4.45	1.30	1.32
7	0915	62	CR	16.39	16.71	4.31	4.28	1.14	0.95
7	1254	69	CR	16.05	16.96	4.42	4.71	1.01	0.85
7	1331	73	HI	17.68	18.15	4.41	4.19	1.24	1.21

CRUISE

Date	Time	Reading	Prior			Emission	index		
June 1979		number	ımber power setting	Carbon monoxide		Oxide nitro		Hydrocarbons (as methane)	
				AESO	FAA	AESO	FAA	AESO	FAA
 5	1110	20	AP	13.68	13.58	4.50	4.87	1.08	0.91
5	1150	24	MC	13.00	13.53	4.69	4.82	1.06	0.71
6	0905	31	MC	14.13	15.39	4.68	4.85	0.93	0.91
6	1010	37	AP	14.36	15.40	4.71	5.03	1.01	1.15
7	0831	57	AP	14.71	14.67	4.67	4.67	0.94	0.96
7	0910	61	MC	13.57	13.95	4.61	4.73	0.80	0.78
7	1246	68	MC	13.70	14.09	4.66	3.97	0.73	0.77
7	1339	74	AP	13.53	13.70	4.73	4.43	18.0	0.78

NOTE: Code for prior power setting: I - idle, HI - high idle, CR - cruise, AP - approach, MC - maximum continuous, TO - takeoff.

Table 5-1. Variation of emission indexes from a T58-GE-8F engine (concluded)

Test Cell - 12

Location - Naval Air Rework Facility, North Island

MAXIMUM CONTINUOUS

Date	Time	Reading	Prior			Emission			
June 1979		number	mber power setting	Carbon monoxide		Oxide nitro		Hydrocarbons (as methane)	
				AESO	FAA	AESO	FAA	AES0	FAA
		······································							
5	1100	21	CR	11.96	12.20	4.75	5.03	0.85	0.73
5	1140	23	TO	13.16	13.54	4.78	4.95	1.13	0.88
6	0855	30	TO	11.27	11.75	4.88	5.01	0.54	0.82
6	1015	38	CR	13.53	14.26	5.02	5.28	0.96	1.06
7	0840	58	CR	12.96	13.52	4.90	4.93	0.85	0.84
7	0900	60	TO	11.43	11.72	4.94	4.96	0.59	0.63
7	1238	67	MC	12.00	12.08	4.92	4.36	0.71	0.71
7	1347	75	CR	12.38	_	4.95	-	0.63	-

TAKEOFF

Dat	e Time	Reading	Prior			Emission	index		
Jun 197		number	power setting	Carbon monoxide		Oxide nitro		Hydroca (as me	
			·	AESO	FAA	AESO	FAA	AESO	FAA
5	1130	22	MC	8.61	_	5.29		0.70	_
6	0840	29	I	8.97	-	5.05	_	0.48	-
6	1023	39	MC	9.24	-	5.61	-	0.48	-
7	0851	59	MC	9.86	-	5.42	-	0.54	-
7	1230	66	I	8.43	-	5.39	-	0.63	-
7	1407	65	I	9.03	-	5.47	-	0.46	_

NOTE: Code for prior power setting: I - idle, HI - high idle, CR - cruise, AP - approach, MC - maximum continuous, TO - takeoff.

Table 5-2. Gaseous emissions from a J52-P-6B engine, comparison of emissions at two different sampling positions

Power setting		Carbon monoxide	Carbon dioxide	Oxides of nitrogen		Hydrocarbo ppmC	ns
•		ррm	7	$NO_{\mathbf{x}}$	NO		F/A
					ppm		
Idle	(AESO)	195.0	0.45	2.8	-	106.8	0.00212
Idle	(Scott)	615.89	1.24	10.66	10.26	289.00	0.006
3000 lbs Thrust	(AESO)	52.9	0.65	7.2	-	5.0	0.00294
Intermediate 1	(Scott)	185.24	1.58	21.74	20.38	29.50	0.008
75% Thrust	(AESO)	28.3	0.89	15.0	-	5.5	0.00406
Intermediate 2	(Scott)	96.95	2.20	40.04	38.68	15.90	0.011
Normal rated	(AESO)	25.3	1.04	22.3	-	5.5	0.00477
Normal	(Scott)	55.82	2.63	59.78	57.46	11.90	0.013
Military	(AESO)	19.2	1.13	29.2	-	3.5	0.00518
Military	(Scott)	37.64	2.96	79.04	76.73	10.20	0.014

Power	F	Tuel flow,	Thrust,	Emission	index,	lbs/1000 lbs	of fuel
setting		lbs/hr	lbs	СО	CO ₂	NOx	CH ₄
Idle	(AESO)	714	512	88.31	3196	2.12	28.33
Idle	(Scott)	715	511	93.68	2967	2.66	25.17
(mean,	Scott)	713	-	92.98	-	2.71	26.46
3000 lbs Thrust	(AESO)	2301	3034	16.57	3320	3.91	0.96
Intermediate 1	(Scott)	2308	3157	23.44	3141	4.52	2.14
(mean,	Scott)	2422	-	21.66	-	4.95	2.85
75% Thrust	(AESO)	3977	5446	6.07	3291	5.91	0.76
Intermediate 2	(Scott)	3997	5586	8.88	3167	6.02	0.83
(mean,	Scott)	4090	-	8.73	-	6.68	1.48
Normal rated	(AESO)	5366	7202	4.53	3276	7.48	0.65
Normal	(Scott)	5394	7355	4.29	3175	7.55	0.52
(mean,	, Scott	5444	-	4.48	-	8.02	0.96
Military	(AESO)	6328	8275	3.01	3271	9.00	0.38
Military	(Scott)	6347	8439	2.58	3178	8.89	0.40
(mean,	Scott	6390	-	3.02	-	9.07	0.79

Table 5-2. Gaseous emissions from a J52-P-6B engine, comparison of emissions at two different sampling positions (concluded)

Power setting		Emis	sions, po	unds per l	nour
		co	CO ₂	NOx	CH₄
Id le	(AESO)	63.05	2282	1.51	20.23
Idle	(Scott)	67.0	2122	1.90	18.0
	n, Scott)	71.5	-	2.09	20.5
3000 lbs Thrust	(AESO)	38.13	7639	9.01	2.20
Intermediate l	(Scott)	51.4	7249	10.43	4.93
(mea	n, Scott)	52.5	-	11.49	6.92
75% Thrust	(AESO)	24.14	13090	23.49	3.03
Intermediate 2	(Scott)	35.58	12660	24.08	3.33
(mean	n, Scott)	35.7	-	27.35	5.20
Normal Rated	(AESO)	24.31	17581	40.14	3.49
Normal	(Scott)	23.2	17128	40.75	2.83
(mea	n, Scott)	24.5	-	43.62	5.20
Military	(AESO)	19.02	20701	56.96	2.41
Military	(Scott)	16.4	20173	56.40	2.54
(mea	n, Scott)	19.4	- ·	57.83	5.00

NOTE: Each power setting has two rows of data. The numbers in the first row are data obtained by the Aircraft Environmental Support Office. See data sheets for Files J52001I, J52001B, J52001C, J52001N and J52001M in Appendix C. The numbers in the second row are data obtained by Scott Environmental Technology as reported in Reference 15. The emissions testing was at Test Cell 15, Naval Air Rework Facility, Alameda on 17 June 1976. The Aircraft Environmental Support Office used a single point probe 85 feet behind the exhaust plane of the engine. Scott Environmental Technology used a probe at the exhaust plane of the engine. The 'read times' of the two groups was not correlated. The numbers in the third row of data are the means reported by Scott Environmental Technology for 7 observations during the testing of production engines. The tests by Scott Environmental Technology were performed under the direction of the Naval Air Propulsion Center.

Table 5-3. Gaseous emissions from a T64-GE-7 engine, comparison of emissions at two different sampling positions

	Sampling position	Carbon monoxide	Carbon dioxide		les of ogen	Hydrocarbo ppmC	ons
		ppm	z	ио _х	NO ppm		F/A
-		 					
Idle	(0.81)	576.7	2.09	19.1	-	274.1	0.01001
Idle	(40')	371.7	1.36	10.6	-	194.3	0.00652
75% Horsepowe:	r (0.8')	53.8	3.06	84.7	_	6.6	0.01419
75% Horsepowe	r (40')	40.0	2.00	51.1	-	5.6	0.00926
Normal rated	(0.8')	44.4	3.37	105.5	-	8.2	0.01562
Normal rated	(40')	35.7	2.20	63.5	-	6.9	0.01019
Intermediate	(0.8')	45.9	3.64	126.9	-	8.2	0.01683
Intermediate	(40')	35.7	2.37	75.0	-	6.9	0.01098
Maximum	(0.8')	48.8	3.75	137.2	-	8.0	0.01737
Maximum	(40')	37.1	2.42	80.2	-	6.1	0.0112

Power S	ampling	Fuel flow,	Shaft,	Emission	index,	lbs/1000 lbs	of fuel
setting p	osition	lbs/hr	hp	CO	CO ₂	NOX	CH4
Idle	(0.8')	262	81	53.38	3106	3.02	15.31
Idle	(40')	262	81	52.84	3129	2.52	16.71
75% Horsepowe	r (0.8')	1300	2697	2.08	3214	9.48	0.26
75% Horsepowe	r (40')	1300	2697	2.21	3231	8.79	0.34
Normal rated	(0.8')	1504	3279	1.19	3211	10.72	0.30
Normal rated	(40')	1504	3279	1.47	3228	9.92	0.38
Intermediate	(0.81)	1676	3729	1.10	3210	11.93	0.27
Intermediate	(40')	1676	3726	1.26	3225	10.87	0.35
Maximum	(0.8')	1731	3870	1.19	3209	12.51	0.26
Maximum	(40')	1731	3870	1.32	3224	11.02	0.31

Table 5-3. Gaseous emissions from a T64-GE-7 engine, comparison of emissions at two different sampling positions

Power setting		Emis	sions, po	unds per l	nour
		co .	CO ₂	NOX	CH₄
Idle	(0.8')	13.99	814	0.79	4.01
Idle	(40')	13.84	820	0.68	4.38
75% Horsepower	(0.8')	2.70	4178	12.32	0.34
75% Horsepower	(40')	2.88	4201	11.43	0.44
Normal rated	(0.8')	1.80	4830	16.12	0.45
ormal rated	(40')	2.46	5409	16.63	0.64
Intermediate	(0.8')	1.84	5379	19.99	0.46
Intermediate	(40')	2.11	5404	18.22	0.59
Maximum	(0.8')	2.06	5554	21.66	0.45
Maximum	(40')	2.29	5580	19.70	0.53

NOTE: Each power setting has two rows of data. The numbers in the first row are data obtained at a sampling position of 0.8 feet from the engine exhaust. The numbers in the second row are data obtained at a sampling position 40 feet behind the engine exhaust. The emissions testing was at Test Cell 9, Naval Air Rework Facility, North Island on 29 January 1974. See data sheets for Files T64002I, T64003I, T64002B, T64003B, T64002N, T64003N, T64002M, T64003M, T64002X, and T64003X in Appendix C.

Table 5-4. Gaseous emissions from a J79-GE-8B engine, comparison of emissions without and with ferrocene added to the fuel

Power		Carbon monoxide	Carbon dioxide		es of ogen	Hydrocarb ppmC	ons
setting	•	ppm	Z Z	$NO_{\mathbf{x}}$	NO pm	pputo	F/A
	· - 						
Id le	(no ferrocene)	167.7	0.62	4.1	-	100.6	0.002903
75% rpm	(no ferrocene)	69.2	0.49	4.2	-	17.3	0.002203
75% rpm	(ferrocene)	88.9	0.49	3.2	-	25.7	0.002216
87% rpm	(no ferrocene)	23.4	0.73	11.5	-	2.2	0.003304
87% rpm	(ferrocene)	31.5	0.73	10.0	-	2.2	0.003308
90% rpm	(no ferrocene)	18.5	0.97	22.3	-	2.7	0.004431
90% rpm	(ferrocene)	25.9	0.97	20.8	•••	2.7	0.004435
95% rpm	(no ferrocene)	15.8	1.01	24.5	-	1.1	0.004617
95% rpm	(ferrocene)	19.4	1.01	23.9	-	1.1	0.004619
Military	(no ferrocene)	16.3	1.08	32.9		1.6	0.004946
	(ferrocene)	20.9	1.08	30.7	-	1.6	0.004949

Power		Fuel flow,	Thrust,	Emission	index, lbs	/1000_1ь	s of fuel
setting		lbs/hr	lbs	СО	CO ₂	NOx	CH.
Idle	(no ferrocene) 1188	233	55.18	3210.50	2.26	19.52
75% rpm	(no ferrocene) 1567	863	29.41	3345.65	3.05	4.42
75%	(ferrocene)	1567	863	37.86	3325.27	2.3i	6.53
87% rpm	(no ferrocene) 4689	6015	6.07	3319.84	5.57	0.38
87% rpm	(ferrocene)	4689	6015	8.44	3315.94	4.84	0.37
90% rpm	(no ferrocene) 8213	9659	3.40	3286.69	8.05	0.34
90% rpm	(ferrocene)	8213	9659	5.01	3284.08	7.50	0.34
95% rpm	(no ferrocene) 8412	10291	2.69	3283.97	8.79	0.13
95% rpm	(ferrocene)	8412	10291	3.44	3282.76	8.27	0.13
Military	(no ferrocene) 9225	10939	2.59	3276.97	10.63	0.18
	(ferrocene)	9225	10939	3.49	3275.52	9.91	0.18

Table 5-4. Gaseous emissions from a J79-GE-8B engine, comparison of emissions with and without ferrocene added to the fuel (concluded)

Power etting		Emis	sions. po	unds per	hour
		co	CO ₂	NOX	CH₄
dle	(no ferrocene)	65. 25	3814	2.69	23.19
75% rpm	(no ferrocene)	46.09	5243	4.78	6.93
5% rpm	(ferrocene)	59.33	5211	3.62	18.8
37% rpm	(no ferrocene)	28.48	15567	26.11	1.76
17% rpm	(ferrocene)	39.58	15548	22.68	1.76
0% rpm	(no ferrocene)	27.93	26994	66.08	2.82
0% rpm		41.18	26972	61.58	2.82
95% rpm	(no ferrocene)	22.61	27625	73.97	1.13
5% rpm		28.96	27615	69.58	1.13
Military	(no ferrocene)	23.92	30230	98.06	1.68
-	(ferrocene)	32.21	30217	91.46	1.68

NOTE: See data sheets for Files J79002I, J79002B, J79002C, J79002D, J79002E, J79002M, J79F02B, J79F02C, J79F02D, J70F02E and J79F02M in Appendix C.

6 USE OF EMISSION INDEXES AND EMISSION RATES

The emission index, the fuel flow rate and the length of time at an engine power setting determine the amount of a constituent discharged to the atmosphere at any power setting. The emission index and the fuel flow rate may be expressed together as an emission rate. The addition of the amounts of each constituent from each power setting used in a test or an operating sequence determines the total amount of the constituent formed during that test/operation.

6.1 Calculation of Emissions

Equation (4) determines the amount of a constituent formed at any power setting.

$$W_{z} = EI_{z} \times F/1000 \times hr \tag{4}$$

where W_z is the pounds (kilograms) of a constituent z produced by operation at the power setting for a specified time,

 ${\rm EI_{Z}}$ is the emission index of the constituent z in units of mass per 1000 units of mass of the fuel, i.e., pounds (kilograms) per 1000 pounds (kilograms) of fuel used,

F is the fuel flow rate at the power setting in pounds (kilograms) per hour, and

hr is the time in hours at the engine power setting.

The operation of an engine normally uses several different power settings. The summation of the amounts of the constituent from each power setting gives the amount of the constituent produced by operation at a group of power settings (i.e., an engine test).

The emissions data may include an emission rate such as pounds of constituent per hour. This emission rate can be used instead of the emission index to calculate the amount of a constituent formed.

Programs MATEI, AIRAP and AIRA calculate both emission indexes and emission rates.

6.2 Selection of Emission Indexes and Emission Rates

The tables of section 7 give emission indexes and emission rates at various power settings for specific engines. Typically, these tables include emission indexes and rates for the constituents of the exhaust at idle, at a high power setting such as military or IRP (intermediate rated power), at one or more power settings between idle and military, and at afterburner (if applicable). To calculate emissions for other engines of the same type at similar power settings, substitute appropriate values of the emission indexes from these tables. This assignment is an estimate as emission indexes for different engines of the same type may vary.

6.3 Selection of an Emission Index by Curve Fitting of Existing Data

If sufficient data exist, curve fitting using thrust and emission index as variables, defines a plot and generates descriptive constants. Then, these constants determine the emission index at any engine power setting from the measured thrusts. For example, the Naval Air Propulsion Center reported thrusts and emission indexes at 14 different power settings (Reference 13). Table F404.1 of section 7 records these data. The Aircraft Environmental Support Office used the Hewlett-Packard Advantage Advanced Solutions Pac to determine that the thrust vs. emission index plot, from 15% thrust to IRP, best fit an exponential curve. Paragraph A4.7 of Appendix A lists the data plotted. The curve fitting program generated constants a and b (a = 2.983926 and b = 2.0093 x 10^{-4}) for use in the equation

$$y = ae^{bx}$$
,

where y = emission index and x = thrust in pounds.

The coefficient of determination was found to be 0.9983. Using the constants a and b, the preceding equation determines the emission index at any thrust level from 15% to IRP. For example solving this equation for y (emission index) using a thrust of 5945 pounds for a power setting of 89% rpm,

$$y = 2.9839 e(2.0093 \times 10^{-4} \times 5945) = 9.85.$$

Generally, the emission index and thrust at idle fit poorly on the curve describing the higher thrusts. The emission index for idle is best selected by the direct substitution of a known emission index. We also use direct substitution for the addition of afterburner data.

6.4 Sample Calculation

Table 6-1 records the emissions of the oxides of nitrogen from the simulated testing of an F404-GE-400 engine. It shows, for each power setting, an identification (column 1), a duration (column 2), a thrust (column 3), a fuel flow rate (column 4), an emission index as calculated by equation (4) or from direct substitution of a known value (column 5), the pounds of fuel used (column 6), and the pounds of the oxides of nitrogen produced at each power setting (column 7).

Equation (5) determines the amount of nitrogen dioxide produced at an engine power setting, for example at 89%,

$$W_z = 9.85 \times 4850/1000 \times 5/60 = 3.98$$
.

Thrust values vary within limits from engine to engine and from test to test. This changes, slightly, the value of the emission index used. For example, in this table a power setting of IRP uses a thrust of 10,190 pounds and an emission index of 23.12. Reference 13 reports these values for IRP as 10,548 and 25.16

TABLE 6-1. Emissions of oxides of nitrogen from an F404-GE-400 Engine

Power setting	Time in mode, min.	•	Fuel flow, pounds/hr.		Fuel use per mode, pounds	Pounds of nitrogen dioxide/mode
Flight Idle	5	<u> </u>	996	1.16	83.0	0.10
89% rpm	5	5945	4850	9.85	404.4	3.98
IRP	10	10190	8514	23.12	1419.0	32.81
Afterburner	3	-	29750	9.22	1487.5	13.71
		Pounds of	fuel used in nitrogen dio nitrogen dio ed in test		50.60	

NOTE: By convention, the oxides of nitrogen are expressed as if all of the oxides were nitrogen dioxide, i.e., the calculation of the emission index uses the concentration of the oxides of nitrogen and the molecular weight of nitrogen dioxide.

For the group of power settings, Table 6-1 concludes with a summation of (1) the pounds of fuel used, (2) the pounds of nitrogen dioxide formed per test, and (3) an emissions to fuel ratio, i.e., the pounds of the nitrogen dioxide produced for each pound of fuel used.

6.5 Use of an Averaging Technique to Estimate an Emission Rate

For the oxides of nitrogen, an averaging technique may be used to estimate an emission rate (pounds of constituent per pound of fuel). The use of this technique needs operational records (fuel flow rates and durations of operation at each power setting) from a group of tests which represent the testing of a specific engine at a test facility. The evaluation of each test as described in paragraph 6.4 gives an emissionsto-to-fuel ratio for each test. Averaging this ratio for all of the tests gives a mean value (correlation coefficient) for the amount of the oxides of nitrogen formed for each pound of fuel used. Then, for any test, multiply the total fuel used in the test by the correlation coefficient to get an estimate of the amount of the oxides of nitrogen formed during the test.

For a group of thirteen test of F404 engines at Naval Air Station Lemoore, the Aircraft Environmental Support Office (Reference 16) prepared a series of tables in the format of Table 6.1. The emissions-to-fuel ratios (pounds of oxides of nitrogen per pound of fuel) ranged from 0.01331 to 0.01742 with a mean value of 0.01556. This correlation coefficient can be used to estimate the amount of nitrogen dioxide produced in any test from the amount of fuel used.

7 SUMMARY TABLES OF GASEOUS EMISSIONS FROM AIRCRAFT ENGINES

The tables of this section summarize gaseous emissions data from aircraft engines. The purpose of these tables is to present, on a single page, the most significant emissions data for a group of power settings of an engine. The power settings are those which normally are used in the testing or the operation of an engine. Each table gives emissions data for a specific engine. In the opinion of the Aircraft Environmental Support Office, each table represents the data suitable for estimating emissions from other engines of the same type indicator and type numeral. The tables include emission indexes, fuel flow rates and emission rates. Thus, anyone knowing the engine run times at various power settings can estimate the total gaseous emissions from most of the gas turbine engines in the Navy inventory. Many users of this Handbook need only this section.

7.1 Engine Type Indicator/Numeral and Model Indicator

Whenever possible, a single table gives data suitable for use with all models of an engine type indicator/numeral. Some engines have tables for more than one model indicator. For example, the user of this Handbook consults Table J79.1 to estimate emissions from any J79-GE-8 or J79-GE-10/10A engine and Table J79.4 to estimate emissions from a J79-GE-10B engine. The J79-GE-10B engine has low smoke combustors. Emissions of carbon monoxide and hydrocarbons from it are significantly higher, at idle, than for the J79-GE-8/10 engines.

Another example of multiple tables for an engine type occurs for the T58 engine. The T58-GE-16 engine is rated at 1870 shaft horsepower with fuel consumption of about 1100 pounds per hour at military power. The T58-GE-8F engine is rated at 1350 shaft horsepower with fuel consumption of about 785 pounds per hour at military. The T58-GE-16 engine operates at a higher temperature than the T58-GE-8F engine and consequently produces greater amounts of the oxides of nitrogen.

7.2 Sources of Emissions Data

The summary tables use data obtained from emission measurements by the Aircraft Environmetal Support office and emissions data reported by other organizations. The selection of measurement data for the tables favors those data obtained by the Aircraft Environmental Support Office, because we knew the various details needed to apply the matrix method for the calculation of the emissions parameters.

7.2.1 Emissions Data from Sources other than the Aircraft Environmental Support Office

The summary tables prepared from the reports of other organizations record their data as presented. Normally these reports do not indicate how the the various adjustments were made to the measured concentrations.

7.2.2 Emissions Data from the Aircraft Environmental Support Office

For our emissions measurements, we intend to prepare a data sheet, such as shown as Figure 4-3 of paragraph 4.5.1, for each power setting of each engine test. At the date of the first printing of this Handbook some of our measurements had not yet been converted. The data sheet features a record of the measured concentrations of the constituents, all of the variables used to adjust them and the calculated emissions parameters from the matrix solution of the combustion equations.

The number of data sheets prepared for a test may be only one or two, representing a high and low power setting during a short test. By contrast, the operation of a single engine during an endurance test of eight hours may produce more than fifty data sheets for only five different power settings. Also, for any group of power settings, the emissions data may include a data sheet for each occurrence of a power setting or it may use a single data sheet to represent all occurrences of the power setting. We select from the data sheets the ones to be used for the preparation of the summary table.

7.3 Description of Summary Tables

The table number consists of the engine type indicator and type numeral, followed by a period and another number. This number serves only to distinguish one table from another. The engine manufacturer's symbol and model indicator appear in the captions of the tables. The caption contains either a reference to an AESO file or several words/characters coding a test by another group.

Each table contains three groups of data. Each table contains data entries as available.

The first group of data gives the measured concentrations needed to calculate the emission indexes. The column headers include the basis of measurement if known. The measured concentration tells nothing about the amount of correction needed for instrument interferences. Only Appendix C gives this information. For oxygen, this group gives the calculated and measured concentrations of oxygen.

The second group of data gives the engine operating data and the emission indexes of carbon monoxide, carbon dioxide, oxides of nitrogen, and hydrocarbons.

The third group of data gives the concentration of oxides of nitrogen expressed as if the concentration of oxygen in the exhaust were 3%, the emissions of the pollutants in pounds per hour, the combustion efficiency and the fuel/air ratio.

The table concludes with a record of who did the work, the place of the measurement, the date, the kind of measurement (test cell, test stand or airframe), position of probe and engine serial number.

Each table starts on an odd-numbered page. For groups of more than nine power settings, the table continues on the next page. Most summary tables fit on a single page.

The summary tables are arranged as follows:

turbofan engines - F101, F404, TF30, TF34, TF41;

turbojet engines - J52, J57, J65, J79, J85, LM1500, 7LM2500;

turboprop and turboshaft engines - T53, T56, T58, T64, T76, T400;

auxiliary power units - GTC85-72, GTPC95-2, GTCP100-54, Solar

T-62T-27, WR27.

7.4 Description of Appendix C

If the Aircraft Environmental Support Office made the emissions measurements, Appendix C contains the data sheets used to prepare the tables of section 7. The Summary tables include the most important information from the data sheets of Appendix C. Those needing the instrument interference coefficients, humidity data, molecular constants for the fuel, converter efficiency, calculated dry/semi-dry/wet concentrations, calculated concentrations of water and nitrogen, calculated emissions of sulfur, the constant K, and engine exhaust temperatures must refer to the individual data sheets of Appendix C.

The pages of Appendix C are not numbered. An index at the beginning of the Appendix lists the data sheets it contains.

TABLE F101.1. GASEOUS EMISSIONS FROM AN F101DFE ENGINE (GE TM 82-697)

Reading number	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides nitrog NO _X measu ppm, semi	gen NO ced,	Hydrocarbons measured, ppm, wet	Oxy meas., %	_
199	245.6	1.12	8.6	_	39.4	_	_
201	192.9	1.14	9.1	-	24.1	-	-
203	46.3	1.08	13.9	-	7.3	-	-
205	34.8	1.15	17.4	-	6.1	-	-
207	14.6	2.91	92.3	-	4.4	-	-
211	14.3	3.13	109.4	-	4.1	_	-
209	17.0	3.71	177.6	-	4.0	-	-
213	17.2	3.82	217.5	-	3.5		-

Reading number	Fuel flow, lb/hr	Thrust, lb	Speed,	Emis CO	sion index,	1b/1000 NO _X	lb of fuel Hydrocarbons
				· · · · · · · · · · · · · · · · · · ·			
199	867	628	2305	44.2	-	2.58	4.1
201	947	731	2483	34.3	-	2.71	2.5
203	1558	1869	3877	8.9	-	4.44	0.8
205	1849	2447	4378	6.2	-	5.22	0.6
207	5880	9301	7219	1.0	-	10.90	0.2
211	6586	10369	7448	0.9	_	12.04	0.2
209	8872	13549	7992	0.9	-	16.54	0.1
213	10073	15083	8221	0.9	-	19.69	0.1

Reading number	Oxides of correc	nitrog	en, ——	Emissions,	pounds	per hour	Combustion efficiency	,
	3% oxygo meas. ————	en, ppm calc.	, CO	CO ₂	NO ₂	Hydrocarbon	s %	
199	_	-	38.3	_	2.2	3.6	98.61	0.0053 ⁻
201	-	-	32.5	-	2.6	2.4	98.98	0.0054
203	-	-	13.9	-	6.9	1.2	99.72	0.0050
205	-	-	11.5	-	9.7	1.1	99.80	0.0053
207	-	-	5.9	-	64.1	1.2	99.96	0.0137
211	-	-	5.9	-	79.3	1.3	99.96	0.0148
209	-	-	8.0	-	146.7	0.9	99.97	0.0175
213	-	-	9.1	-	198.3	1.0	99.97	0.0180

NOTE: Values in this table taken from S. P. Seto, Emission Characteristics of F101DFE Engine 5009003/4 at Ground Level, General Electric Technical Memorandum 82-697. Emission rates calculated by AESO from emission index and fuel flow rates.

TABLE F402.N1. GASEOUS EMISSIONS FROM AN F402 ENGINE (NAPC)

Idle 1075.2 1.770 10.7 - 376.4 85% 124.7 3.044 73.9 - 17.5 100% 56.4 3.956 175.9 - 11.6
100% 56.4 3.956 175.9 - 11.6
100% 50.4 5.750 175.7

Power setting	Fuel flow, lb/hr	Thrust, lb	Speed,	Emiss CO	sion index,	1b/1000 NO _x) lb of fuel Hydrocarbons
						X	
Idle	1137	589	-	106.3	2935.7	1.7	18.8
85%	6186	8871	-	8.2	3146.9	8.0	0.7
100%	10712	15084	-	2.7	3156.6	14.8	0.4
100%	10/12	15084	-	2.7	3156.6	14.8	0.4

Power setting	3% oxyg	cted t	om, CO	Emissions CO ₂	, pounds NO ₂	per hour Hydrocarbo	Combustion efficiency, ons %	F/A
Idle	-	-	120.9	3337.9	1.9	21.4	-	-
85%	-	-	50.7	19466.7	49.5	4.5	-	_
100%	-	-	28.9	33813.5	158.5	4.4	-	-

NOTE: values in this table are preliminary data from NAPC using JP-5 fuel and a simulated altitude of 5,000 feet.

TABLE F404.N1. GASEOUS EMISSIONS FROM AN F404-GE-400 ENGINE (NAPC)

Power setting	Carbon monoxide	Carbon dioxide	Oxide nitro	ogen	Hydrocarbons measured,	Oxy meas.,	calc.,
	measured, ppm	measured, %	NO _X measure		ppm	%	%
Ground idle	1352.1	1.721	6.9	-	1232.4	-	-
Flight idle	1046.7	1.518	-	-	811.3	-	-
15%	261.9	2.118	25.7	-	58.5	-	-
20%	139.1	2.297	32.0	-	30.0	-	-
26%	73.1	2.538	39.7	-	18.0	-	-
37%	62.3	2.899	56.5	-	15.0	_	-
46%	28.5	3.209	81.5	-	< 15.0	-	-
63%	21.2	3.677	131.3	-	< 15.0	_	-

el flow, lb/hr	Thrust, lb	Speed, rpm	Emission CO	n index,	1b/1000 NO _X	lb of fuel Hydrocarbons
623.9	78	-	· · ·		1.16	58.18
1666.4	1597	-	24.49	3112	3.95	44.50 2.54
2422.5	2782	-	5.77	3148	5.15	1.21 0.66
005.2	4883	-	1.78	3155	8.37	0.48 < 0.44 < 0.38
	lb/hr	1b/hr 1b 623.9 78 814.8 234 666.4 1597 989.2 2069 2422.5 2782 8108.4 3845 6005.2 4883	1b/hr 1b rpm 623.9 78 - 814.8 234 - 666.4 1597 - 989.2 2069 - 2422.5 2782 - 3108.4 3845 - 6005.2 4883 -	1b/hr 1b rpm CO 623.9 78 - 137.34 814.8 234 - 123.52 666.4 1597 - 24.49 989.2 2069 - 12.09 2422.5 2782 - 5.77 8108.4 3845 - 4.31 4005.2 4883 - 1.78	1b/hr 1b rpm CO CO ₂ 623.9 78 - 137.34 2747 814.8 234 - 123.52 2815 2666.4 1597 - 24.49 3112 2989.2 2069 - 12.09 3136 2422.5 2782 - 5.77 3148 3108.4 3845 - 4.31 3151 2005.2 4883 - 1.78 3155	1b/hr 1b rpm CO CO ₂ NO _X 623.9 78 - 137.34 2747 1.16 814.8 234 - 123.52 2815 - 666.4 1597 - 24.49 3112 3.95 989.2 2069 - 12.09 3136 4.56 9422.5 2782 - 5.77 3148 5.15 8108.4 3845 - 4.31 3151 6.42 6005.2 4883 - 1.78 3155 8.37

Power setting	Oxides of correct	nitro	•	Emissions,	pounds	per hour	Combustion efficiency,	F/A
·	3% oxyg meas.			CO ₂	NO ₂	Hydrocarbon	as %	
Ground idle	-	-	85.69	1714	0.72	36.30	-	-
Flight idle	-	-	100.64	2294	-	36.26	-	-
15%	-	-	40.81	5186	6.58	4.23	-	-
20%	-	-	24.05	6238	9.07	2.41	-	-
26%	-	-	13.98	7626	12.48	1.60	-	-
37%	-	-	13.40	9795	19.96	1.49	-	-
46%	-	-	7.13	12636	33.52	< 1.76	-	-
63%	-	-	6.48	17631	65.52	< 2.12	-	-

NOTE: values in this table are taken from Naval Air Propulsion Center letter NAPC-LR-81-10 of 30 November 1981; except emissions, pounds per hour, which were calculated from emission indexes and fuel flow rates.

TABLE F404.N2. GASEOUS EMISSIONS FROM AN F404-GE-400 ENGINE (NAPC)

Power setting	Carbon monoxide	Carbon dioxide	0xide nitr	ogen	Hydrocarbons measured,	Oxy meas.,	calc.,
	measured, ppm	measured, %	NO _X measure	NO ed, ppm	ppm	% 	%
76%	21.7	3.988	178.9	-	< 15.0	-	-
Max. cont.	25.0	4.304	244.1	-	< 15.0	-	-
94%	26.8	4.423	286.7	-	< 15.0	-	-
IRP	24.0	4.579	349.2	-	< 15.0	-	-
A/B min.	1678.7	4.300	281.4	-	354.0	-	-
A/B mid.	1704.4	7.550	296.6	-	311.0	-	-
A/B max.	1234.3	10.610	299.2	-	15.0	_	-

Power	Fuel flow,	Thrust,	Speed,	Emiss	ion index,	lb/1000	lb of fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NOX	Hydrocarbons
76%	6541.3	8031	_	1.09	3156	14.80	< 0.35
Max. cont.	7495.1	9201	-	1.17	3156	18.71	< 0.33
94%	8082.6	9957	-	1.22	3156	21.38	< 0.32
IRP	8586.9	10548	-	1.05	3156	25.16	< 0.31
A/B min.	10250.0	10996	-	74.95	2017	20.64	7.35
A/B mid.	19071.0	14110	-	44.21	2077	12.64	3.75
A/B max.	28396.5	15254	-	23.12	3122	9.22	0.13

Power setting	Oxides of corre	nitrog	-	Emission	s, pounds	per hour	Combustion efficiency,	F/A
	3% oxyg meas.	gen, ppm calc.	ı, CO	CO ₂	NO ₂	Hydrocarbon	s %	
76%	-	-	7.13	20644	96.81	< 2.29	-	-
Max. cont.	-	-	8.77	23655	140.23	< 2.27	-	-
94%	-	-	9.86	25509	172.81	< 2.59	-	_
IRP	-	-	9.02	27100	216.05	< 2.66	•	-
A/B min.	-	-	768.24	20674	211.56	75.34	-	-
A/B mid.	-	-	843.13	39610	241.06	71.52	•	-
A/B max.	-	-	656.53	88654	261.82	3.69	_	_

NOTE: values in this table are taken from Naval Air Propulsion Center letter NAPC-LR-81-10 of 30 November 1981; except emissions, pounds per hour, which were calculated from emission indexes and fuel flow rates.

TABLE TF30.1. GASEOUS EMISSIONS FROM A TF30-P-6C ENGINE (SUMMARY OF FILES TF30020I, TF30020B, TF30020C, TF30020N, TF30020M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of cogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxymeas., %, semi- dry	ygen calc., %, wet
Idle	116.9	0.35	2.0	-	42.2	-	20.25
30% Thrust	35.9	0.49	6.5	-	8.3	-	20.05
75% Thrust	17.2	0.66	13.7	-	3.3	-	19.79
Normal rated	11.2	0.78	21.8	-	5.1	-	19.61
Military	10.1	0.97	36.8	-	8.3	-	19.33

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NOX	CH _{y/x}	CH₄
Idle	670	645	_	70.58	3339.56	2.03	12.92	14.99
30% Thrust	2030	3400	-	14.87	3376.83	4.77	1.84	2.13
75% Thrust	3560	6275	-	4.75	3337.67	7.38	0.54	0.62
Normal rated	4830	8395	-	2.31	3314.95	9.86	0.70	0.81
Military	6700	11025	_	1.56	3287.67	13.28	0.91	1.09

Power (Oxides of correct			ions, pound	s per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	-	51	47.29	2237.50	1.36	10.04	97.07	0.001577
30% Thrust	-	129	30.19	6854.97	9.68	4.33	99.47	0.002182
75% Thrust	-	212	16.92	11882.12	26.26	2.22	99.84	0.002972
Normal rate	d -	291	11.18	16011.20	47.64	3.91	99.88	0.003535
Military	-	405	10.48	22027.41	88.98	7.05	99.87	0.004430

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 15, Naval Air Rework Facility, Alameda on 1 July 1976, single point probe, 85 feet behind the engine. Engine serial number 652061.

TABLE TF30.2. GASEOUS EMISSIONS FROM A TF30-P-412A ENGINE (SUMMARY OF FILES TF30021I, TF30021B, TF30021N, TF30021A)

• •	m, %, -dry semi-c		x NO asured, semi-dry	ppmC, wet	%, semi- dry	%, wet
Idle 6	4.7 0.2	5 2.2	! -	71.1	-	20.37
75% Thrust	9.6 0.4	6 13.6	-	6.2	-	20.06
Normal rated	6.7 0.5	6 25.0	-	6.2	-	19.91
Military	6.7 0.6	35.2	! -	4.6	-	19.79
Afterburner Z5 24	6.6 4.5	64.4		8.8	-	14.06

Power !	Suel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	920	595	10278	55.51	3440.59	3.22	31.42	36.46
75% Thrust	4300	7070	13441	3.43	3413.00	10.74	1.48	1.72
Normal rated	5980	9550	14105	1.62	3371.58	16.02	1.20	1.39
Military	7050	10900	14505	1.38	3347.82	19.60	0.77	0.90
Afterburner Z	5 47800	18850	14460	10.77	3188.56	4.79	0.20	0.24

Power 0 setting			nitrogen ted to	=	ions, pound	ds per h	our	Combustion efficiency,	F/A
	3% or mea		calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle		-	69	51.07	3165.34	2.96	33.54	95.57	0.001094
75% Thrust		-	275	14.74	14675.89	46.19	7.38	99.77	0.002027
Normal rated		-	431	9.66	20162.07	95.82	8.34	99.84	0.002497
Military		-	544	9.71	23602.14	138.20	6.34	99.89	0.002874
Afterburner	Z5 ·	-	162	514.91	152413.20	229.04	11.31	99.73	0.021252

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 16, Naval Air Rework Facility, Alameda on 24 June 1976, single point probe, 85 feet behind the engine. Engine serial number 679326.

TABLE TF34.1. GASEOUS EMISSIONS FROM A TF34-GE-400 ENGINE (SUMMARY OF FILES TF34001I, TF34001B, TF34001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X meas	es of cogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	•	gen calc., %, wet
Idle	211.9	0.41	2.0	-	58.9	-	20.14
75% rpm	102.2	0.44	4.2	-	10.7	-	20.10
Military	60.2	0.81	17.3	-	3.0	-	19.55

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	485	950	11600	90.98	3248.66	1.69	14.99	17.40
75% rpm	460	960	12000	33.57	3369.69	3.42	2.63	3.06
Military	3800	9275	16500	5.95	3304.70	7.51	0.39	0.46

Power setting	Oxides of correc	_		ions, pound	ls per h	our_	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	СО	CO ₂	NO ₂	CH₄	%	
Idle	-	44	44.13	1575.60	0.82	8.44	96.39	0.001899
75% rpm	-	89	15.44	1550.06	1.58	1.41	98.96	0.001964
Military	-	221	22.62	12557.87	28.56	1.74	99.82	0.003682

Emissions measurements by the Aircraft Environmental Support Office at TF34 Test Cell, Naval Air Station, North Island on 29 January 1974, single point probe. Engine serial number 202110.

TABLE TF41.1. GASEOUS EMISSIONS FROM A TF41-A-2 ENGINE (SUMMARY OF FILES TF410011, B, C, D, E, N, and TF41003M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of cogen NO cured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	267.3	0.55	2.9	-	287.1	-	19.90
8000 rpm	236.5	0.53	3.6	-	201.8	_	19.93
9000 rpm	166.3	0.56	4.7	-	124.5	-	19.90
10000 rpm	121.4	0.59	6.2	-	73.0	-	19.86
75% Max. cont.	12.4	0.93	44.7	-	6.4	-	19.36
90% Max. cont.	11.0	1.04	67.5	-	8.2	-	19.19
Intermediate	12.4	1.19	76.8	_	7.2	19.0	18.92

1b 595 820	7100 8000	94.80 88.70	CO ₂	NO _x	CH _{y/x}	CH ₄
						59.48
						37.40
		00.70	3112.35	2.25	38.14	44.26
1210	9020	60.41	3200.23	2.86	22.90	26.58
1800	10029	42.30	3253.88	3.64	12.96	15.04
9550	12056	2.17	3292.14	16.85	0.73	0.85
11500	12460	1.62	3280.21	22.67	0.84	0.97
14000	-	1.64	3267.64	22.46	0.64	0.74
	1800 9550 11500	1800 10029 9550 12056 11500 12460	1800 10029 42.30 9550 12056 2.17 11500 12460 1.62	1800 10029 42.30 3253.88 9550 12056 2.17 3292.14 11500 12460 1.62 3280.21	1800 10029 42.30 3253.88 3.64 9550 12056 2.17 3292.14 16.85 11500 12460 1.62 3280.21 22.67	1800 10029 42.30 3253.88 3.64 12.96 9550 12056 2.17 3292.14 16.85 0.73 11500 12460 1.62 3280.21 22.67 0.84

	des of correct	nitrogen		ions, pound	ls per h	our	Combustion efficiency,	F/A
	% oxyge meas.	en, ppm, calc.	СО	CO ₂	NO ₂	CH₄	%	
Idle	_	49	103.33	3325.03	1.87	64.83	92.67	0.002711
8000 rpm	-	63	109.10	3828.19	2.77	54.43	94.13	0.002561
9000 rpm	-	80	90.62	4800.34	4.29	39.86	96.31	0.002631
10000 rpm	-	101	79.53	6117.30	6.84	28.28	97.72	0.002726
75% Max. cont.	-	500	13.01	19752.85	101.09	5.09	99.88	0.004242
90% Max. cont.	-	684	12.15	24535.96	169.56	7.25	99.88	0.004759
Intermediate	594	671	14.63	29212.69	200.76	6.65	99.90	0.005464

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 15, Naval Air Rework Facility, Alameda on 24 June and 8 July 1976, single point probe. 85 feet behind the engine exhaust. Engine serial numbers 141917/141369.

TABLE J52.1. GASEOUS EMISSIONS FROM A J52-P-6B ENGINE (SUMMARY OF FILES J52001I, J52001B, J52001C, J52001N, J52001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nit: NO _X meas	es of rogen NO sured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	rgen calc., %, wet
Idle	195.0	0.46	2.8	-	106.8	20.3	20.03
3000 lbs Thrus	t 52.9	0.65	7.2	-	5.0	20.1	19.76
75% Thrust	28.3	0.90	15.0	-	5.5	19.9	19.39
Normal rated	25.3	1.04	22.3	-	5.5	-	19.18
Military	19.2	1.13	29.2	-	3.5	19.7	19.05

Power I	Fuel flow,	Thrust,	Speed,	Emis	sion index	, 1b/100	0 lb of	fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	714	512	6926	86.37	3196.13	2.07	23.88	27.71
3000 lbs Thru	st 2301	3034	9770	16.57	3319.80	3.91	0.82	0.96
75% Thrust	3977	5446	10641	6.00	3290.12	5.84	0.65	0.75
Normal rated	5366	7202	11177	4.53	3276.40	7.48	0.56	0.65
Military	6328	8275	11500	3.01	3271.29	9.00	0.33	0.38

		nitrogen, ted to	Emiss	ions, pound	ls per h	our	Combustion efficiency,	F/A
	oxyge eas.	en, ppm, calc.	CO	CO ₂	NO ₂	CH₄	% 	· · · · · · · · · · · · · · · · · · ·
Idle	59	54	61.67	2282.03	1.48	19.79	95.61	0.002165
3000 lbs Thrust	119	108	38.13	7638.86	9.01	2.20	99.53	0.002943
75% Thrust	202	171	23.85	13084.82	23.22	3.00	99.80	0.004108
Normal rated	-	224	24.31	17581.18	40.14	3.49	99.84	0.004765
Military	333	273	19.02	20700.70	56.96	2.41	99.90	0.005183

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 15, Naval Air Rework Facility, Alameda on 17 June 1976, single point probe, 85 feet behind the engine. Engine serial number 649773.

TABLE J52.10. GASEOUS EMISSIONS FROM A J52-P-8B ENGINE (SUMMARY OF FILES J52010I, J52010MI, J52010B, J52010C, J52010N, J52010M)

1	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X meas	es of ogen NO ured, emi-dry	Hydrocarhons measured, ppmC, wet	Oxymeas., %, semi- dry	ygen calc., %, wet
Idle	149.1	0.47	2.5	-	194.6	20.2	20.02
Manual idle	139.1	0.40	2.2	-	221.7	-	20.13
3000 lbs Thrust	36.1	0.68	12.2	-	10.9	19.9	19.72
75% Thrust	17.0	0.99	28.6	-	5.4	19.5	19.26
Normal rated	8.3	1.23	42.9	-	6.9	19.4	18.90
Military	8.1	1.40	52.7	-	12.3	19.1	18.65

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	1b, hc	1b	rpm	СО	CO ₂	NO _X	CH _{y/x}	CH ₄
Idle	680	475	6625	63.78	3166.50	1.79	42.20	48.96
Manual idle	640	-	6350	69.51	3149.76	1.84	56.16	65.16
3000 lbs Thru	st 2300	3005	9866	10.54	3319.15	6.34	1.72	1.99
75% Thrust	4320	5900	10869	3.00	3284.13	10.10	0.58	0.67
Normal rated	6130	8030	11478	0.87	3266.06	12.13	0.59	0.69
Military	7370	9200	11906	0.71	3254.59	13.05	0.93	1.08

	des of correct	nitrogen, ted to		ions, pound	s per h	our	Combustion efficiency,	Γ,/A
	% oxyge meas.	calc.	СО	CO ₂	NO ₂	CH ₄	%	
Idle	47	48	43.37	2153.22	1.22	33.30	94.30	0.002233
Manual idle	-	48	44.48	2015.85	1.18	41.70	92.77	0.00191
3000 lbs Thrus	t 170	177	24.23	7634.04	14.58	4.58	99.58	0.003079
75% Thrust	294	301	12.98	14187.45	43.64	2.90	99.87	0.004526
Normal rated	408	372	5.35	20020.96	74.36	4.22	99.92	0.005649
Military	426	406	5.22	23986.31	96.16	7.93	99.89	0.006449

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 15, Naval Air Rework Facility, Alameda on 29 June 1976, single point probe, 85 feet behind the engine. Engine serial number 661421.

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TABLE J52.20. GASEOUS EMISSIONS FROM A J52-P-408 ENGINE (NAPC Scott)

Intermediate 1 92.59 1.68 31.29 28.17 20.40 -	Power	Carbon	Carbon	Oxid	es of	Hydrocarbons	Оху	gen
Intermediate 1 92.59 1.68 31.29 28.17 20.40 -	setting	measured,	measured,	$NO_{\mathbf{X}}$	NO	•	•	calc.
	ſdle	361.98	1.24	9.39	9.20	320.00	-	-
Intermediate 2 44.27 2.82 71.08 67.23 16.30 -	Intermediate 1	92.59	1.68	31.29	28.17	20.40	-	-
	Intermediate 2	44.27	2.82	71.08	67.23	16.30	-	-
Normal 31.59 3.28 101.70 99.11 17.40 -	Normal	31.59	3.28	101.70	99.11	17.40	-	-
Military 26.88 3.70 137.18 137.18 18.20 -	1ilitary	26.88	3.70	137.18	137.18	18.20	-	-

Power	Fuel flow,	Thrust,	Speed,	Emiss	ion index	, lb/1000) lb of fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NO_X	Hydrocarbons
Idle	779	548	_	55.96	3018	2.38	28.33
Intermediate		3420	-	11.12	3162	6.17	1.40
Intermediate 2	2 5752	7629	-	3.18	3177	8.38	0.67
Normal	8078	10142	-	1.95	3179	10.29	0.61
Military	9479	11349	-	1.47	3180	12.32	0.57

Power setting	Oxi	ldes of correc			Emissions	, pounds	per hour	Combustion efficiency,	F/1
		meas.			CO ₂	NO ₂	Hydrocarbo	ns %	
Idle		-	-	43.6	2351	1.86	22.07	_	0.00
Intermediate	1	-	-	28.3	8054	15.71	3.57	-	0.00
Intermediate	2	-	-	18.3	18272	48.21	3.85	-	0.01
Normal		-	-	15.7	25678	83.13	4.96	-	0.01
Military		-	-	13.9	30104	116.76	5.40	-	0.01

NOTE: values in this table are taken from Scott Env. Tech., Individual Engine Test & Model Summary Reports, Mod. 6, Alameda Testing, USAF Contract F29601-75-C-46, October 20, 1976.

TABLE J57.1. GASEOUS EMISSIONS FROM A J57-P-10 ENGINE (SUMMARY OF FILES J57001I, J57001B, J57001N, J57001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides nitro NO _X measu prm, ser	gen NO red,	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	237.4	0.55	3.3	-	564.3	-	19.87
75% Thrust	18.3	1.01	21.4	-	7.2	-	19.21
Normal rated	13.0	1.16	30.0	_	11.0	19.0	18.99
Military	10.2	1.26	37.6	_	10.3	19.0	18.84

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index,	lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NO_X	CH _{y/x}	CH ₄
Idle	1100	555	6009	80.52	2920.94	1.87	96.60	112.10
75% Thrust	5670	7040	8958	3.21	3281.02	7.40	0.76	0.88
Normal rated	7250	9050	9267	1.79	3268.55	9.00	1.00	1.16
Military	8370	10310	9468	1.16	3262.61	10.37	0.86	1.00

Power (Oxides of correct	•		ions, pound	ls per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	-	55	88.57	3213.04	2.05	123.31	88.47	0.00283
75% Thrust	-	219	18.20	18603.40	41.97	4.98	99.85	0.00462
Normal rate	d 235	272	13.00	23696.99	65.26	8.44	99.86	0.005325
Military	292	316	9.74	27308.07	86.78	8.40	99.89	0.005792

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 15, Naval Air Rework Facility, Alameda on 9 July 1976, single point probe, 85 feet behind the engine. Engine serial number 606306.

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TABLE J57.21. GASEOUS EMISSIONS FROM A J57-P-420 ENGINE (SUMMARY OF FILES J57021I, J57021B, J57021C, J57021D, J57021N, J57021M, J57021A)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X meas	es of cogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	252.2	0.56	2.7	_	444.2	-	19.83
30% Thrust	63.5	0.65	8.2	-	27.6	-	19.72
75% Thrust	36.5	0.82	16.3	-	8.4	-	19.46
96% rpm	27.0	1.00	27.4	-	10.2	-	19.20
Normal rated	27.0	0.98	25.7	-	6.5	-	19.23
Intermediate	24.1	1.21	45.1	-	5.6	-	18.89
Afterburner	336.1	4.29	65.4	-	103.0	-	14.40

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	lb/hr	lb	rpm	CO	CO ₂	NO_X	CH _{y/x}	CH₄
Idle	1322	393	6794	80.74	2985.39	1.53	76.46	88.73
30% Thrust	3413	3577	8407	14.83	3310.23	4.45	4.54	5.27
75% Thrust	5767	6946	9090	4.32	3303.38	6.99	1.09	1.27
96% rpm	7667	9139	9569	1.17	3284.34	9.58	1.09	1.26
Normal rated	7701	9241	9508	1.23	3287.72	9.18	0.71	0.82
Intermediate	10570	12007	10090	0.34	3268.72	12.97	0.49	0.57
Afterburner	39721	18240	10085	14.20	3177.14	5.16	2.54	2.94

Power 0: setting	xides of correc	nitrogen ted to		ions, pound	ds per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	CO	CO ₂	NO ₂	CH ₁	%	
Idle	-	43	106.74	3946.69	2.03	117.29	90.48	0.00282
30% Thrust	-	118	50.62	11297.80	15.17	17.98	99.20	0.00295
75% Thrust	-	195	24.91	19050.60	40.32	7.33	99.79	0.00372
96% rpm	-	277	8 96	25181.04	73.46	9.65	99.86	0.00457
Normal rated	-	265	9.49	25318.72	70.70	6.31	99.90	0.00447
Intermediate	-	387	3.58	34550.36	137.13	6.02	99.94	0.00555
Afterburner	-	173	563.93	126199.20	205.13	116.87	99.42	0.02004

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 20, Naval Air Rework Facility, North Island on 16 January 1974, single point probe, 95 feet behind the engine. Engine serial number 634012.

TABLE J65.1. GASEOUS EMISSIONS FROM A J65-W-5F ENGINE (SUMMARY OF FILES J65001I, J65001B, J65001C, J65001D, J65001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X	ured,	Hydrocarbons measured, ppmC, wet	Ox meas., %, semi- dry	ygen calc., %, wet
Idle	201.7	0.87	6.3	-	82.5	20.0	19.44
7450 rpm	55.9	0.89	18.6	-	8.0	18.8	19.42
8000 rpm	41.3	1.09	17.9	-	7.4	-	19.13
8300 rpm	29.7	1.22	18.1	-	3.8	-	18.93
Military	35.6	1.28	19.3	-	7.4	19.5	18.84

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	1320	450	4020	47.16	3196.99	2.46	9.78	11,35
7450 rpm	4370	4710	7450	12.61	3279.73	7.30	0.95	1.10
8000 rpm	5970	6380	8000	7.39	3266.45	5.71	0.72	0.83
8300 rpm	7040	7330	8300	4.57	3261.68	5.15	0.33	0.38
Military	6946	7250	8311	5.31	3255.43	5.23	0.61	0.71

Power setting	Oxides of correct	_		ions, pound	ls per h	our	Combustion efficiency,	F/A
	3% oxyg∈ meas.	en, ppm, calc.	CO	CO ₂	NO ₂	CH ₄	%	
Idle	94	74	62.25	4220.02	3.25	14.98	97.93	0.004087
7450 rpm	139	217	55.11	14332.42	31.89	4.82	99.61	0.004075
8000 rpm	-	175	44.13	19500.71	34.10	4.96	99.76	0.005008
8300 rpm	-	160	32.19	22962.25	36.28	2.68	99.86	0.005611
Military	195	163	36.86	22612.21	36.31	4.91	99.82	0.005897

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 1, Naval Air Rework Facility, Alameda on 22 June 1976, single point probe. Engine serial number 503118.

TABLE J79.1. GASEOUS EMISSIONS FROM A J79-GE-8D ENGINE (SUMMARY OF FILES J79001I, J79001B, J79001D, J79001D, J79001M, J79020A)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of rogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	169.3	0.62	4.3	-	101.7	-	19.84
75% rpm	72.0	0.49	4.1	-	20.1	-	20.04
87% rpm	24.3	0.72	11.4	-	2.0	-	19.70
90% Nor. rated	16.8	0.96	23.2	-	1.0	-	19.34
Military	13.5	1.07	32.0	-	1.4	-	19.18
Afterburner	281.3	3.81	52.9	-	32.7	15.7	15.10

Power Fu	el flow,	Thrust,	Speed,	Emis	sion index	, 1b/100	0 1b of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NOX	CH _{y/x}	CH ₄
Idle	1205	259	5012	55.70	3209.27	2.37	16.93	19.64
75% rpm	1520	1022	5763	30.61	3341.62	2.98	4.40	5.11
87% rpm	4545	5933	6662	6.43	3321.47	5.60	0.30	0.34
90% Nor. rated	8206	9700	7155	3.06	3289.04	8.46	0.11	0.13
Military	9453	10838	7690	2.07	3278.84	10.44	0.14	0.16
Afterburner	34315	17222	7464	13.25	3186.92	4.72	0.91	1.05

	les of correct	nitrogen ed to		ions, pound	ds per h	our	Combustion efficiency,	F/A
	oxyge neas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	-	69	67.12	3867.17	2.86	23.67	97.01	0.002904
75% rpm	-	81	46.53	5079.26	4.52	7.77	98.85	0.00220
87% rpm	-	163	29.23	15096.06	25.45	1.57	99.82	0.00325
90% Nor. rated	-	257	25.15	26989.87	69.45	1.05	99.92	0.004383
Military	-	322	19.54	30994.88	98.70	1.52	99.94	0.00489
Afterburner	156	157	454.56	109359.20	161.87	36.05	99.60	0.01777

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 20. Naval Air Rework Facility, North Island, 10 May 1977 and 12 June 1974, single point probe, 95' behind engine. Engine serial numbers 401917 and 433996.

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TABLE J79.10. GASEOUS EMISSIONS FROM A J79-GE-10B ENGINE (SUMMARY OF FILES J79BB01I, J79BB01B, J79BB01C, J79BB01D, J79BB01M, J79BB01A)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxide nitro NO _X measu ppm, se	NO NO red,	Hydrocarbons measured, ppmC, wet	Oxymeas., %, semi- dry	ygen calc., %, wet
Idle	415.6	0.70	2.9	_	281.1	20.0	19.63
30% Thrust	67.9	0.57	6.8	-	15.6	20.2	19.86
85% rpm	57.6	0.66	8.6	-	14.3	20.1	19.73
75% Thrust	31.3	0.99	23.4	-	14.9	19.7	19.24
Intermediate	29.3	1.19	35.1	-	13.6	19.4	18.94
Afterburner	294.3	3.70	49.1	-	18.3	15.7	15.27

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NO_X	CH _{y/x}	CH ₄
Idle	1250	265	5077	111.41	3023.18	1.33	39.19	45.47
30% Thrust	3422	3381	6340	20.04	3331.43	4.23	2.94	3.41
85% rpm	3640	4243	6496	13.63	3317.03	4.60	2.32	2.69
75% Thrust	7578	9000	7171	2.74	3281.22	8.26	1.60	1.85
Intermediate	10000	11248	7475	1.60	3265.84	10.26	1.21	1.40
Afterburner	35000	17500	7475	14.56	3186.88	4.51	0.52	0.60

Power 0 setting	xides of correct	0		ions, pound	ds per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	44	39	139.26	3778.97	1.67	56.84	93.50	0.003480
30% Thrust	121	112	68.59	11400.14	14.48	11.67	99.24	0.002573
85% rpm	142	126	49.63	12074.00	16.75	9.79	99.45	0.002991
75% Thrust	270	243	20.74	24865.06	62.58	14.04	99.78	0.004530
Intermediate	333	311	15.97	32658.38	102.58	14.03	99.84	0.005467
Afterburner	145	150	509.57	111540.90	157.78	21.15	99.61	0.017267

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 19. Naval Air Rework Facility, North Island on 12 June 1974, single point probe. Engine serial number 433421.

TABLE J85.N1. GASEOUS EMISSIONS FROM A J85-GE-2 ENGINE (NAPC-F973)

Power setting	Carbon monoxide measured, ppm	Carbon dioxide measured, %	nitr NO _X	es of ogen NO ed, ppm	Hydrocarbons measured, ppm	Oxy, meas.,	gen calc., %
Ground idle	>1500	2.50	30	28	318	-	-
15%*	1330	2.44	27	22	148	-	-
20%*	1267	2.44	27	21	130	-	-
30%*	832	2.45	31	22	61	-	-
40%*	680	2.51	35	24	44	-	-
60%*	505	2.77	44	31	27	-	-

Power setting	Fuel flow, lb/hr	Thrust, lb	EGT, °F.	Emissi CO	on index,	1b/1000 NO _X	lb of fuel Hydrocarbons
Ground idle	560 785	200 503	945 838	>111.86	-	3.68	11.86 5.72
20%*	810 1045	540 838	840 857	98.23 65.53	-	3.44	5.04 2.40
40% * 60% *	1220 1700	1062 1658	867 950	52.66 35.78	-	4.46 5.13	1.70 0.959

Power setting	Oxides of correc		_	١,	Emissions,	pounds	per hour	Combustion efficiency	,
	3% oxyg meas.			СО	CO ₂	NO ₂	Hydrocarbon	as %	
Ground idle	-	_	> 6	52.64	-	2.06	6.64	-	0.01219
15%*	-	-	8	30.69	-	2.69	4.49	-	0.0111
20%*	-	-	7	79.57	-	2.79	4.08	-	0.0111
30%*	-	-	6	8.48	-	4.20	2.51	-	0.01144
40%*	-	-	6	64.25	-	5.44	2.08	-	0.01204
60%*	-	-	ϵ	50.82	-	8.72	1.63	-	0.0137

^{*} Normal rated power

NOTE: values in this table are taken from Naval Air Propulsion Test Center letter PE71:GES:ss, 10340 SER F973, of 24 April 1974.

TABLE J85.N2. GASEOUS EMISSIONS FROM A J85-GE-2 ENGINE (NAPC-F973)

Power	Carbon	Carbon		es of	Hydrocarbons	0xy	
setting	monoxide measured, ppm	dioxide measured, %	$NO_{\mathbf{X}}$	ogen NO ed, ppm	measured, ppm	meas., %	calc. %
75%*	445	3.09	54	37	20	_	-
90%*	420	3.44	65	44	18	-	-
90%**	418	3.48	66	45	17	-	-
Normal rated	412	3.74	73	50	17	-	-
Military	410	3.76	74	51	17	-	-

Power	Fuel flow,	Thrust,	EGT,	Emissi	on index,	1b/1000	lb of fuel
setting	lb/hr	1b	°F.		CO ₂	NO _X	Hydrocarbons
75%*	2155	2178	1058	28.38	-	5.67	0.636
90%*	2615	2655	1176	24.11	-	6.14	0.516
90%**	2655	2694	1196	23.73	-	6.16	0.482
Normal rated	2875	2893	1271	21.78	-	6.35	0.449
Military	2890	2905	1276	21.56	-	6.40	0.446

Power setting	Oxides of correc	nitroge ted to	en,	Emissions,	pounds	per hour	Combustion efficiency	,
		en, ppm, calc.	CO	CO ₂	NO ₂	Hydrocarbon	is %	 .
75%*	-	-	61.15	_	12.21	1.37	-	0.01508
90%*	-	-	63.05	-	16.05	1.35	-	0.01654
90%**	•	-	62.99	-	16.36	1.28	-	0.01667
Normal rated	-	-	62.62	-	18.25	1.29	-	0.01790
Military	-	-	62.32	-	18.50	1.29	-	0.01814

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TABLE LM15.1. GASEOUS EMISSIONS FROM A 7LM1500-PB-104A ENGINE (SUMMARY OF FILES LM1501I, LM1501B, LM1501N, LM1501M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry		ıred,	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	gen calc., %, wet
Idle	124.1	0.43	1.6	-	41.5	-	20.09
75% Thrust	56.4	0.63	6.7	-	8.0	-	19.80
Normal rated	54.7	0.82	13.9	-	7.6	-	19.51
Intermediate	53.2	0.83	15.2	-	8.0	-	19.50

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	1237	565	5026	40.86	3336.90	1.32	10.36	12.02
75% Thrust	4597	6041	6957	4.14	3344.09	3.79	1.37	1.59
Normal rated	7903	10024	7453	2.26	3307.09	5.97	0.99	1.15
Intermediate	8356	10509	7564	1.82	3306.05	6.45	1.03	1.19

Power 0 setting	xides of correct	_		ions, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	-	33	50.54	4127.74	1.63	14.87	98.02	0.001938
75% Thrust	-	104	19.02	15372.79	17.40	7.30	99.77	0.002833
Normal rated	, -	172	17.87	26135.91	47.17	9.07	99.85	0.00372
Intermediate	-	186	15.25	27625.34	53.86	9.97	99.85	0.00377

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 13, Naval Air Rework Facility, North Island on 10 February 1975, single point probe, 50 feet behind the engine. Engine serial number 417214.

TABLE LM25.1. GASEOUS EMISSIONS FROM AN LM2500 ENGINE (SUMMARY OF FILES LM2501I, LM2501B, LM2501C, LM2501D, LM2501E, LM2501F)

Power setting	Carbon monoxide measured, ppm, semi-dry	%,	nitr NO _X meas	es of ogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	259.1	0.65	2.3	-	334.8	-	19.77
7235 rpm	124.7	0.70	5.3	-	64.2	-	19.71
7708 rpm	64.6	0.82	10.3	-	16.7	-	19.53
7814 rpm	47.6	0.89	12.6	-	9.9	-	19.43
7949 rpm	26.9	0.97	17.3	-	5.2	-	19.31
8046 rpm	18.3	1.03	20.8	-	4.2	-	19.23

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	1b	rpm	СО	CO ₂	NOX	CH _{y/x}	CH₄
Idle	800	_	5000	77.73	3051.92	1.15	50.60	58.72
7235 rpm	1745	-	7235	36.51	3245.36	2.62	9.58	11.12
7708 rpm	2958	-	7708	15.96	3280.82	4.39	2.15	2.50
7814 rpm	3431	-	7814	10.65	3282.17	4.95	1.18	1.37
7949 rpm	4097	-	7949	5.23	3282.84	6.23	0.57	0.66
8046 rpm	4621	-	8046	3.14	3280.10	7.05	0.43	0.50

Power setting	Oxides of correc			ions, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
Idle	-	35	62.18	2441.54	0.92	46.97	93.14	0.00320
7235 rpm	-	76	63.72	5663.16	4.56	19.41	98.19	0.00324
7708 rpm	-	130	47.20	9704.67	12.98	7.39	99.41	0.00375
7814 rpm	-	148	36.52	11261.14	16.97	4.69	99.64	0.00407
7949 rpm	-	188	21.43	13449.79	25.54	2.70	99.82	0.00443
8046 rpm	-	215	14.52	15157.32	32.59	2.32	99.88	0.00471

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 20, Naval Air Rework Facility, North Island on 19 June 1977, single point probe, 95 feet behind the engine. Engine serial number GG018.

TABLE LM25.2. GASEOUS EMISSIONS FROM AN LM2500 ENGINE (SUMMARY OF FILES LM2501G, LM2501H, LM2501J, LM2501K, LM2501L, LM2501N)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry		ured,	Hydrocarbons measured, ppmC, wet	Oxymeas., %, semi- dry	%,
8190 rpm	9.9	1.16	29.1	-	4.5	-	19.03
8210 rpm	9.3	1.17	29.8	-	4.1	-	19.02
8297 rpm	6.8	1.25	35.6	-	4.5	-	18.90
8415 rpm	5.1	1.33	45.4	-	5.6	-	18.78
8643 rpm	5.3	1.52	63.7	-	8.6	-	18.50
8752 rpm	4.5	1.58	73.0	-	6.9	_	18.41

Power	Fuel flow,	Thrust,	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	lb/hr	1b	rpm	CO	CO ₂	NOX	CH _{y/x}	CH₄
8190 rpm	5647	-	8190	1.23	3271.41	8.74	0.41	0.48
8210 rpm	5710	-	8210	1.11	3270.93	8.87	0.37	0.4
8297 rpm	6385	-	8297	0.60	3265.79	9.90	0.38	0.4
8415 rpm	7470	-	8415	0.28	3260.89	11.85	0.44	0.5
8643 rpm	9130	-	8643	0.25	3250.35	14.51	0.60	0.69
8752 rpm	10080	-	8752	0.13	3248.32	15.98	0.46	0.5

Power setting	Oxides of correct	_	Emiss	ions, pound	ds per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	СО	CO ₂	NO ₂	CH₄	%	
8190 rpm	-	270	6.95	18473.62	49.35	2.69	99.93	0.00532
8210 rpm	-	274	6.34	18677.01	50.66	2.45	99.94	0.00536
8297 rpm	-	309	3.85	20852.07	63.24	2.82	99.95	0.00574
8415 rpm	-	372	2.12	24358.85	88.55	3.85	99.95	0.00611
3643 rpm	-	461	2.28	29675.70	132.45	6.31	99.93	0.00700
3/52 rpm	-	509	1.27	32743.01	161.12	5.38	99.95	0.00728

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 20, Naval Air Rework Facility, North Island on 19 June 1977, single point probe, 95 feet behind the engine. Engine serial number GG018.

TABLE T53.1. GASEOUS EMISSIONS FROM A T53-L-11D ENGINE (SUMMARY OF FILES T53001I, T53001B, T53001N, T53001M, T53001T)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of rogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Ground idle	572.0	3.14	15.6	_	1856.9	-	16.01
Flight idle	542.0	2.60	19.8	-	344.6	-	16.79
Normal rated	186.0	3.79	71.5	-	20.4	-	15.12
Military	133.0	4.30	79.9	-	10.6	-	14.41
Takeoff	142.0	4.23	96.1	-	10.8	=	14.50

Power Fu	uel flow,	Shaft	Speed,	Emis	sion index.	1b/100	0 lb of	fuel
setting	lb/hr	hp	% rpm	CO	CO ₂	NO_X	CH _{y/x}	CH ₄
Ground idle	145	35	42	31.51	2979.79	1.58	58.09	67.41
Flight idle	222	110	62	37.79	3119.75	2.53	13.57	15.75
Normal rated	645	410	95	6.83	3198.31	6.43	0.57	0.66
Military	685	569	98	3.34	3201.57	6.34	0.26	0.30
Takeoff	690	600	100	3.85	3201.13	7.75	0.27	0.32

Power 0 setting	xides of correc	nitrogen, ted to	Emissi	ons, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	СО	CO ₂	NO ₂	CH ₄	%	
Ground idle	-	55	4.57	432.07	0.23	9.77	93.46	0.01570
Flight idle	-	83	8.39	692.58	0.56	3.50	97.77	0.01244
Normal rated	-	213	4.40	2062.91	4.15	0.43	99.78	0.01761
Military	-	211	2.29	2193.08	4.35	0.21	99.90	0.01993
Takeoff	-	258	2.66	2208.78	5.35	0.22	99.88	0.01961

Emissions measurements by the Aircraft Environmental Support Office at MCAS Camp Pendleton on 26 August 1975, single point probe at engine exhaust plane, engine on test stand. Engine serial number L-E 12771.

TABLE T56.1. GASEOUS EMISSIONS FROM A T56-A-16 ENGINE (SUMMARY OF FILES T56001I, T56001B, T56001D, T56001B, T56001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxide nitro NO _X measu ppm, se	ogen NO red,	Hydrocarbons measured, ppmC, wet	0x; meas., %, semi- dry	%,
L/S Gr. idle	206.4	1.37	14.4	-	259.0	19.1	18.73
H/S Gr. idle	30.0	1.01	18.4	-	11.7	19.5	19.29
Flight idle	27.0	1.11	20.8	-	10.0	19.4	19.14
75%	8.2	2.07	59.7	-	3.3	18.0	17.72
100%	11.1	2.14	64.0	-	2.5	17.9	17.62
Military	11.1	2.21	67.1	-	2.9	17.6	17.51

asttina			Speed,		SION INCK	, 10/100	0 lb of	ruer
setting	1b/hr 	hp	rpm	СО	CO ₂	NOx	CH _{y/x}	CH ₄
L/S Gr. idle	599	130	9964	30.11	3149.25	3.53	19.24	22.32
H/S Gr. idle	756	245	13485	5.65	3275,53	6.35	1.22	1.42
Flight idle	836	510	13380	4.54	3268.50	6.52	0.95	1.10
75%	1996	3550	13820	0.42	3232.84	9.93	0.17	0.19
100%	2136	3890	13820	0.68	3230.89	10.29	0.12	0.14
Military	2219	4090	13820	0.65	3229.32	10.45	0.14	0.16

Power Or setting	xides of correct	_		ons, pound	s per ho	our_	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	СО	CO ₂	NO ₂	CH₄	%	
L/S Gr. idle	120	116	18.04	1886.40	2.11	13.37	97.38	0.00652
H/S Gr. idle	196	198	4.27	2476.30	4.80	1.07	99.75	0.00462
Flight idle	207	205	3.80	2732.46	5.45	0.92	99.80	0.00509
75%	318	327	0.84	6452.74	19.82	0.39	99.97	0.00957
100%	330	340	1.45	6901.18	21.99	0.30	99.97	0.00990
Military	318	345	1.45	7165.85	23.18	0.35	99.97	0.01023

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 11, Naval Air Rework Facility, Alameda on 23 June 1976, single point probe. Engine serial number 102138.

TABLE T58.1. GASEOUS EMISSIONS FROM A T58-GE-8F ENGINE (SUMMARY OF FILES T58A65I, T58A55B, T58A56C, T58A31D, T58A58N, T58A76M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of cogen NO ured, wet	Hydrocarbons measured, ppmC, wet	Ox meas., %, semi- dry	ygen calc., %, wet
Idle	1100.9	1.02	5.2	-	1595.6	-	19.03
High idle	927.0	1.08	5.8	-	1008.5	-	18.96
Approach	153.2	1.79	22.7	-	19.1	-	18.01
Cruise	129.9	1.85	24.5	-	14.1	-	17.92
Max. cont.	125.9	1.95	27.0	-	13.6	-	17.77
Takeoff	96.4	2.12	32.7	-	8.0	-	17.53

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	lb/hr	hp	rpm	СО	CO ₂	NO _X	CH _{y/x}	CH ₄
Idle	132	15	15016	178.44	2569.31	1.43	130.42	151.34
High idle	149	27	16987	152.36	2760.33	1.62	83.67	97.09
Approach	581	918	24578	17.28	3210.80	4.47	1.12	1.30
Cruise	627	1027	24983	14.13	3214.97	4.68	0.80	0.93
Max. cont.	685	1159	25592	12.96	3214.12	4.90	0.73	0.85
Takeoff	786	1360	26689	9.03	3217.15	5.47	0.40	0.46

Power setting	Oxides of correct	_		ons, pound	s per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	СО	CO ₂	NO ₂	CH ₄	%	
Idle	-	49	23.55	339.15	0.19	19.98	82.82	0.00596
High idle	-	53	22.70	411.29	0.24	14.47	88.10	0.00587
1pproach	-	140	10.04	1865.47	2.60	0.75	99.49	0.00834
Cruise	-	147	8.86	2015.79	2.94	0.58	99.59	0.00861
Max. cont.	-	155	8.88	2201.67	3.36	0.58	99.63	0.00907
Takeoff	-	174	7.10	2528.68	4.30	0.36	99.75	0.00985

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 12, Naval Air Rework Facility, North Island on 6-7 June 1979, single point probe, 15 feet behind the engine. Engine serial number 271178.

TABLE T58.N1. GASEOUS EMISSIONS FROM A T58-GE-16 ENGINE (NAPC F991)

Power	Carbon	Carbon	Oxid	es of	Hydrocarbons	Оху	gen
setting	monoxide measured, ppm	dioxide measured, %	$NO_{\mathbf{X}}$	ogen NO ed, ppm	measured, ppm	meas., %	calc.
Ground idle	1125	1.41	15	13	641	-	
60% Normal	155	2.07	51	50	8	-	-
75% Normal	124	2.22	66	63	14	-	-
90% Normal	109	2.32	73	70	20	-	-
90% Military	104	2.37	78	75	20	-	-
Military	98	2.45	89	86	33	-	-

Power setting	Fuel flow, lb/hr	Torque, ft-lb	EGT,	Emissi CO	CO ₂	, 1b/1000 NO _X	lb of fuel Hydrocarbons
Ground idle	150	29	1059	139.73	-	3.03	40.91
60% Normal 75% Normal	656 779	284 358	1200 1301	14.56 10.89	-	7.88 9.47	0.384 0.628
90% Normal	890	431	1394	9.10	-	10.07	0.828
90% Military	924	453	1416	8.52	-	10.45	0.819
Military	1020	503	1482	7.73	-	11.60	1.32

Power setting	Oxides of correct	nitroge cted to	en,	Emissions,	pounds	per hour	Combustion efficiency,	F/A
		en, ppm, calc.	CO	CO ₂	NO ₂	Hydrocarbon	s %	
Ground idle	-	-	20.96	-	0.454	6.14	-	-
60% Normal	-	-	9.55	-	5.17	0.252	-	-
75% Normal	-	-	8.48	-	7.37	0.489	-	_
90% Normal	-	-	8.10	-	8.96	0.745	-	-
90% Military	-	-	7.87	-	9.65	0.756	-	-
Military	-	-	7.89	-	11.84	1.35	=	_

NOTE: Emissions measurements by the Naval Air Propulsion Center, PE71:GES:ss, 10340, Ser F991, 13 June 1974.

TABLE T63.N1B. GASEOUS EMISSIONS FROM A T63-A-5A ENGINE (NAPTC)

Power setting	Carbon monoxide	Carbon dioxide		es of ogen	Hydrocarbons measured,	Oxy meas.,	_
	measured, ppm	measured, %	NO _X measur	NO ed, ppm	ppm	%	%
Ground idle	825	1.96	-	9.0	423	_	-
Flight idle	645	2.00	-	12.0	218	-	-
30%	460	2.33	-	21.0	78	-	-
60%	308	2.93	-	37.0	20	-	-
75%	235	3.26	-	46.0	8	-	-
Military	145	3.83	-	61.0	3	-	_

Fuel flow, lb/hr	Shaft hp	Speed, rpm	Emissio CO	n index, CO ₂	1b/1000 NO _X	lb of fuel Hydrocarbons
61	23.4	32850	79.15	-	1.420	20.30
105	96	42090	38.59	-	2.898	3.272 0.6752
175 215	238 305	49220 52020	14.31	-	4.608 5.07	0.2434 0.0781
	1b/hr 61 70 105 157 175	1b/hr hp 61 23.4 70 23.7 105 96 157 218 175 238	1b/hr hp rpm 61 23.4 32850 70 23.7 36330 105 96 42090 157 218 47050 175 238 49220	1b/hr hp rpm CO 61 23.4 32850 79.15 70 23.7 36330 61.83 105 96 42090 38.59 157 218 47050 20.79 175 238 49220 14.31	1b/hr hp rpm CO CO ₂ 61 23.4 32850 79.15 - 70 23.7 36330 61.83 - 105 96 42090 38.59 - 157 218 47050 20.79 - 175 238 49220 14.31 -	1b/hr hp rpm CO CO2 NOx 61 23.4 32850 79.15 - 1.420 70 23.7 36330 61.83 - 1.893 105 96 42090 38.59 - 2.898 157 218 47050 20.79 - 4.109 175 238 49220 14.31 - 4.608

Power setting	Oxides of	nitroge eted to		Emissions,	pounds		Combustion fficiency,	F/A
		en, ppm, calc.	CO	CO ₂	NO ₂	Hydrocarbons	_ % 	
Ground idle	-	-	4.828	-	0.0866	1.238	-	0.0105
Flight idle	-	-	4.328	-	0.1325	0.7314	-	0.0108
30%	-	-	4.052	-	0.3043	0.3436	-	0.0116
60%	-	-	3.264	-	0.6451	0.1060	-	0.0156
75%	-	-	2.504	-	0.8064	0.0426	-	0.0163
Military	-	-	1.622	-	1.09	0.0168	~	0.0188

NOTE: values in this table are taken from Naval Air Propulsion Test Genter letter PE:GS:ss, 10340 SER 910, of 14 September 1972. Measurements of carbon monoxide, carbon dioxide and oxides of nitrogen are reported on a dry basis. JP-4 fuel.

TABLE T64.1. GASEOUS EMISSIONS FROM A T64-GE-6B ENGINE (SUMMARY OF FILES T64001I, T64001B, T64001N, T64001N)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	niti NO _X meas	es of cogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	ygen calc., %, wet
Idle	417.2	1.39	11.5	-	182.0	•	18.66
75% hp	61.7	1.78	40.3	-	7.0	-	18.12
Normal rated	49.7	1.96	51.1	-	9.0	-	17.86
Military	43.7	2.05	58.4	-	10.0	-	17.73
Max. cont.	40.8	2.10	61.7	-	11.0	-	17.66

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	00 lb of	fuel
setting	lb/hr	hp	rpm	СО	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	321	119	13459	57.27	3124.03	2.75	13.24	15.36
75% hp	1063	2052	16650	4.27	3234.24	7.80	0.41	0.48
Normal rated	1262	2679	17096	2.66	3231.12	8.97	0.48	0.56
Military	1370	3004	17544	1.87	3229.91	9.80	0.51	0.59
Max. cont.	1428	3167	17761	1.50	3229.15	10.11	0.55	0.64

Power C setting	xides of correc	_		ons, pound	ls per h	our	Combustion efficiency,	F/A
	3% oxyge meas.	en, ppm, calc.	СО	CO ₂	NO ₂	CH ₄	%	
Idle	-	89	18.38	1002.81	0.88	4.93	97.35	0.006671
75% hp	-	253	4.54	3437.99	8.29	0.51	99.86	0.008240
Normal rated	i -	293	3.35	4077.68	11.32	0.71	99.89	0.009076
Military	-	321	2.56	4424.98	13.43	0.81	99.91	0.009493
Max. cont.	-	331	2.14	4611.22	14.43	0.91	99.91	0.009726

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 9, Naval Air Rework Facility, North Island on 10 January 1974, single point probe, 40 feet behind the engine. Engine serial number 262265.

TABLE T64.31. GASEOUS EMISSIONS FROM A T64-GE-413 ENGINE (SUMMARY OF FILES T64031I, T64031B, T64031N, To4031M, T64031X)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X meas	es of ogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	380.5	1.37	10.8	-	234.7	-	18.71
75% hp	47.8	1.90	47.1	-	6.3	-	17.96
Normal rated	43.4	2.09	58.6	-	6.6	-	17.68
Intermediate	39.7	2.24	71.1	-	7.3	-	17.46
Maximum	38.4	2.31	76.7	_	5.9	-	17.36

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	0 1b of	fuel
setting	lb/hr	hp	rpm	СО	CO ₂	NO_X	CH _{y/x}	CH ₄
Idle	260	64	11985	51.83	3120.68	2.62	17.28	20.05
75% hp	1287	2699	16875	1.94	3234.40	8.54	0.35	0.40
Normal rated	1511	3345	17274	1.20	3230.58	9.65	0.33	0.38
Intermediate	1661	3779	17472	0.67	3227.98	10.92	0.34	0.40
Maximum	1 721	3937	17589	0.49	3227.08	11.42	0.27	0.31

Power O setting	xides of correct	9		ons, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH ₄	%	
Idle	-	86	13.48	811 38	0.68	5.21	97.07	0.00658;
75% hp	-	279	2.50	4162.67	10.99	0.52	99.92	0.008793
Normal rated		317	1.81	4881,40	14.58	0.58	99,94	0.00967:
Intermediate		360	1.12	5361.68	18.13	0.66	99.95	0.010373
Maximum	-	378	0.85	5553.80	19.65) 54	99,96	0.01069.

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 9. Naval Air Rework Facility, North Island on 28 January 1974, single point probe, 40 feet behind the engine. Engine serial number 264274.

TABLE T64.51. GASEOUS EMISSIONS FROM A T64-GE-415 ENGINE (SUMMARY OF FILES T640511, T64051B, T64051N, T64051N, T64051X)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nit: NO _X meas	es of rogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	gen calc., %, wet
Idle	573.2	1.40	9.1	-	343.8	-	18.61
75%	75.2	2.51	59.2	-	3.2	-	17.03
Normal rated	70.7	2.72	73.7	-	2.0	-	16.73
Military	69.2	2.82	82.2	-	7.5	-	16.58
Max. rated	72.2	2.87	90.7	-	5.3	-	16.51

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	hp	rpm	СО	CO ₂	NOX	CH _{y/x}	CH₄
Idle	269	41	11755	74.33	3059.84	2.12	24.35	28.25
75%	1493	3066	17170	2.10	3221.31	8.09	0.13	0.16
Normal rated	1730	3660	17536	1.50	3219.21	9.29	0.08	0.09
Military	1916	4100	17750	1.29	3217.52	9.99	0.28	0.33
Max. rated	2005	4372	17910	1.47	3216.87	10.83	0.19	0.23

Power (Oxides of correct			ons, pound	s per h	our	Combustion efficiency,	F/A
	3% oxyg€ meas.		СО	CO ₂	NO ₂	CH₄	%	
Idle	-	69	20.00	823.10	0.57	7.60	95.84	0.006860
75%	-	266	3.14	4809.41	12.09	0.23	99,94	0.011636
Normal rate	d -	307	2.60	5569.23	16.08	0.16	99.96	0.012609
Military	-	331	2.48	6164.77	19.15	0.62	99,94	0.013075
Max. rated	-	359	2.94	6449.83	21.72	0.45	99,95	0.013307

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 9. Naval Air Rework Facility, North Island on 23 October 1975, single point probe. 40 feet behind the engine. Engine serial number 264453.

TABLE T76.1. GASEOUS EMISSIONS FROM A T76-G-12A ENGINE (SUMMARY OF FILES T76001B, T76001B)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	$NO^{\mathbf{X}}$	ogen NO ured,	Hydrocarbons measured, ppmC, wet	meas., %, semi- dry	gen calc., %, wet
Ground start	303.8	1.84	23.5	-	182.0	-	17.92
High idle	323.4	2.26	30.1	-	133.5	-	17.30
Military	95.6	4.23	88.9	_	1.9	_	14.50

Power	Fuel flow,	Shaft	Speed,	Emis	sion index,	1b/100	0 1b of	fuel
setting	lb/hr	hp	rpm	CO	CO ₂	NO_X	CH _{y/x}	CH ₄
Ground start	180	-	40500	28.29	3162.13	4.30	10.21	11.85
High idle	212	-	40100	24,59	3170.73	4.50	6.13	7.12
Military	382	-	41700	1.69	3205.27	7.18	0.05	0.06

	•	Emissi	ons, pound	s per h	our_		F/A
		CO	CO ₂	NO ₂	CH₄	%	
-	136	5.09	569.18	0.77	2.13	98.32	0.008710
-	145	5.21	672.19	0.95	1.51	98.82	0.010654
-	239	0.65	1224.41	2.74	0.02	99.96	0.019591
	correct 3% oxygemeas.	corrected to 3% oxygen, ppm, meas. calc. - 136 - 145	3% oxygen, ppm, CO meas. calc. - 136 5.09 - 145 5.21	corrected to Emissions, pound 3% oxygen, ppm, calc. - 136 5.09 569.18 - 145 5.21 672.19	corrected to Emissions, pounds per house of the second sec	corrected to $\frac{\text{Emissions, pounds per hour}}{3\% \text{ oxygen, ppm, meas. calc.}}$ $\frac{\text{CO}}{\text{CO}_2} \frac{\text{NO}_2}{\text{NO}_2} \frac{\text{CH}_4}{\text{CH}_4}$ $\frac{-136}{-145} \frac{5.09}{5.21} \frac{569.18}{672.19} \frac{0.77}{0.95} \frac{2.13}{1.51}$	corrected to Emissions, pounds per hour efficiency, 3% oxygen, ppm, meas. calc. $\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Emissions measurements by the Aircraft Environmental Support Office at MCAS Camp Pendleton on 26 August 1975, single point probe at engine exhaust plane, engine on test stand. Engine serial number 000427,

TABLE T400.1. GASEOUS EMISSIONS FROM A T400-CP-400 ENGINE (SUMMARY OF FILES T400011, T40001B, T40001C, T40001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X meas	es of ogen NO ured, emi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	ygen calc., %, wet
Ground idle	511.0	3.09	28.2	-	268.3	_	16.11
Flight idle	520.0	3.06	28.1	-	220.5	-	16.15
Cruise	108.0	3.75	53.8	-	5.4	-	15.20
Military	79.0	4.31	84.2	-	4.5	-	14.41

Power	Fuel flow,	Torque	Speed,	Emis	sion index	, lb/100	0 lb of	fuel
setting	lb/hr	ft-lb	rpm	CO	CO ₂	NOx	CH _{y/x}	CH₄
Ground idle	138	3	3366	29.78	3141.05	3.05	8.98	10.42
Flight idle	143	6	4105	30.71	3144.78	3.08	7.46	8.65
Cruise	283	20	5735	2.64	3206.59	4.90	0.15	0.18
Military	412	37	6310	0.75	3206.10	6.68	0.11	0.13

Power C setting	xides of correct	nitrogen, ted to	Emissi	ons, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	calc.	СО	CO ₂	NO ₂	CH ₄	% 	
Ground idle	-	102	4.11	433.47	0.42	1.44	98.41	0.01466
Flight idle	-	102	4.39	449.70	0.44	1.24	98.54	0.01450
Cruise	-	163	0.75	907.46	1.39	0.05	99.92	0.01738
Military	-	223	0.31	1320.91	2.75	0.05	99.97	0.01995

Emissions measurements by the Aircraft Environmental Support Office at MCAS Camp Pendleton on 25 August 1975, single point probe at engine exhaust plane, engine on test stand. Engine seria number 64100.

TABLE GT.10. GASEOUS EMISSIONS FROM A GTC85-72 ENGINE (SUMMARY OF FILES GT8501I, GT8501M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides nitrog NO _X measure ppm, semi	en measured, NO ppmC, wet ed,	Oxy meas., %, semi- dry	gen calc., %, wet
No load	176.1	0.96	9.2 -	49.4	_	19.25
Load	157.6	2.14	24.3 -	2.7	-	17.51

setting	lb/hr	hp						
·			r.bw		CO ₂	NO _x	CH _{y/x}	CH ₄
No load	105	-	42400	37.43	3215.88	3.28	5.36	6.22
Load	210	-	42050	14.83	3208.28	3.88	0 13	0.15

Power setting	Oxides of correct		Emissi	ons, pound	s per ho	our	Combustion efficiency,	F/A
	3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	·
No load	-	96	3.93	337.67	0.34	0.65	98.60	0.004482
Load	-	124	3.11	673.74	0.81	0.03	99.64	0.009974

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 103, Naval Air Rework Facility, Alameda on 29 July 1976, single point probe. Engine serial number 126P2245.

TABLE GT.20. GASEOUS EMISSIONS FROM A GTPC95-2 ENGINE (SUMMARY OF FILES GT9501I, GT9501M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides of nitrogen NO _X NO measured, ppm, semi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Idle	86.7	0.94	11.9 -	19.3	-	19.37
100%	35.5	2.05	33.7 -	7.0	-	17.73

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	00 lb of :	fuel
setting	lb/hr	hp	rpm	СО	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	131	-	-	18.75	3259.21	4.39	2.16	2.50
100%	293	-	-	3.20	3228.29	5.65	0.36	0.42

3% oxyge meas.	n, ppm, calc.	CO	CO ₂	NO ₂	CH₄	%	
	Carc.						
_	135	2.46	426.96	0.58	0.33	99.35	0.004333
•	185	0.94	945.89	1.66	0.12	99.89	0.009498
		=					

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 115, Naval Air Rework Facility, Alameda on 15 June 1976, single point probe. Engine serial number P-28735.

TABLE GT.30. GASEOUS EMISSIONS FROM A GTCP100-54 ENGINE (SUMMARY OF FILES GT1001I, GT1001M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides of nitrogen NO _X NO measured, ppm, semi-dry	Hydrocarbons measured, ppmC, wet	-	gen calc., %, wet
Idle	56.0	0.90	16.3 -	13.7	-	19.40
100%	52.3	1.72	29.7 -	2.7	-	18.19

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, 1b/100	0 lb of 1	fuel
setting	lb/hr	hp	rpm	CO	CO ₂	NOx	CH _{y/x}	CH ₄
Idle	225	-	35730	12.48	3276.38	6.32	1.61	1.87
100%	413	-	35190	5.89	3234.53	5.95	0.16	0.19

	_	Emissi	ons, pound	s per ho	our	Combustion efficiency,	F/A
3% oxygen, ppm, meas. calc.	СО	CO ₂	NO ₂	CH₄	% 		
-	188	2.81	737.19	1.42	0.42	99.55	0.004125
-	190	2.43	1335.86	2.46	0.08	99.85	0.007963
	correct 3% oxyge meas.	meas. calc.	corrected to Emissi 3% oxygen, ppm, CO meas. calc.	corrected to Emissions, pound 3% oxygen, ppm, CO CO_2 meas. calc.	corrected to Emissions, pounds per homogeness, ppm, and considering the contract of the contr	corrected to Emissions, pounds per hour 3% oxygen, ppm, meas. calc. CO $_{2}$ NO $_{2}$ CH $_{4}$	corrected to Emissions, pounds per hour efficiency, 3% oxygen, ppm, meas. calc. CO CO_2 NO $_2$ CH $_4$ % $\%$

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 114, Naval Air Rework Facility, Alameda on 28 June 1976, single point probe. Engine serial number P9907.

TABLE 62T.1. GASEOUS EMISSIONS FROM A T-62T-27 ENGINE (SUMMARY OF FILES T6201I, T6201M)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	nitr NO _X	ured,	Hydrocarbons measured, ppmC, wet	0xy meas., %, semi- dry	%,
Idle	149.0	1.03	15.9	-	29.2	-	19.20
100%	344.2	1.62	19.0	-	123.2	-	18.30

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	0 lb of :	fuel
setting	lb/hr 	hp	rpm	CO	CO ₂	NOx	CH _{y/x}	CH₄
Idle	50	-	4330	29.53	3228.98	5.31	2.96	3.43
100%	102	100	4240	42.77	3154.46	3.94	7.79	9.04

Power setting	8 ,			ons, pound	s per h	our	Combustion efficiency,	F/A
	3% oxygen, ppm, meas. calc.	СО	CO ₂	NO ₂	CH ₄	% 	·	
Idle	-	161	1.48	161.45	0.27	0.17	99.02	0.004788
100%	•	127	4.36	321.76	0.40	0.92	98.23	0.007693

Emissions measurements by the Aircraft Environmental Support Office at Test Cell 116, Naval Air Rework Facility, Alameda on 28 June 1976, single point probe. Engine serial number S-424421.

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TABLE WR27.1. GASEOUS EMISSIONS FROM A WR27-1 ENGINE (SUMMARY OF FILES WR2701B, WR2701C)

Power setting	Carbon monoxide measured, ppm, semi-dry	Carbon dioxide measured, %, semi-dry	Oxides of nitrogen NO _X NO measured, ppm, semi-dry	Hydrocarbons measured, ppmC, wet	Oxy meas., %, semi- dry	%,
Low flow	76.6	1.49	9.3 -	8.5	-	18.47
High flow	121.7	2.37	32.5 -	4.8	-	17.13

Power	Fuel flow,	Shaft	Speed,	Emis	sion index	, lb/100	0 lb of 1	fuel
setting	lb/hr	hp	np % rpm	CO	CO ₂	NOx	CH _{y/x}	CH ₄
Low flow	140	85	103	3.48	3199.86	2.13	0.60	0.69
High flow	140	85	102	5.66	3171.54	4.63	0.21	0.24

Power setting	Oxides of correct	nitrogen, ted to		ons, pound	s per ho	our_	Combustion efficiency,	F/A
	3% oxygen, ppm, meas. calc.	CO	CO ₂	NO ₂	CH₄	% 		
Low flow	•	67	0.49	447.98	0.30	0.10	99.86	0.006974
High flow	-	150	0.79	444.02	0.65	0.03	99.85	0.01115

Emissions measurements by the Aircraft Environmental Support Office at APU Test Stand, Naval Air Station, North Island on 10 December 1975, single point probe, at engine exhaust plane, engine on test stand. Engine serial number 121.

8 SUMMARY

8.1 Conclusions

Either a matrix solution of simultaneous equations or a linear combustion equation, derived from the matrix solution, is satisfactory for the calculation of the emission indexes of carbon monoxide, carbon dioxide, oxides of nitrogen, and hydrocarbons in the exhaust from gas turbine engines.

Assuming contemporary instruments, adjustments for instrument interferences, the basis of measurement (wet, dry, or semi-dry), the humidity of the inlet air and NO_{X} converter efficiency are technically desirable, but cause only small changes in the values of the emission indexes.

8.2 Recommendations

The Aircraft Environmental Support Office recommends either the comprehensive matrix solution (as defined by Reference 1), or equation (3) (Figure 4-1 of paragraph 4.2 of this Handbook) as the best methods for the calculation of an emission index of a constituent z.

$$EI_{z} = \left(\frac{[z]}{[CO] + [CO_{2}] + [C_{x}H_{y}]}\right) \left(\frac{10^{3} M_{z}}{MC + \alpha MH}\right) (1 + TX/m)$$
(3)

where z is CO, CO₂, NO_X, or C_XH_Y .

The best method for making a quick estimation of an emission index is by use of equation (2) (Figure 4-1 of Paragraph 4.2).

$$EI_{z} = \left(\frac{[z]}{[CO] + [CO_{2}] + [C_{x}H_{y}] - T}\right) \left(\frac{10^{3} M_{z}}{M_{C} + \alpha M_{H}}\right)$$
 (2)

When using equation (2) make the adjustments for instrument interferences, basis of measurement, humidity and NO_{X} converter efficiency before substitution in the equation.

Use the comprehensive matrix solution whenever a computer, capable of efficient matrix solution, is available; otherwise use a small programmable calculator and equations (2) or (3).

When using either computer or calculator, arrange the program to give a print-out of the numbers entered and the results of the calculation. See Figures 4-3 and 4-4 of this Handbook for examples of print-outs.

8.3 Additional Information

The Aircraft Environmental Support Office is glad to furnish additional information about gaseous emissions from aircraft engines.

For those calculating emission indexes, we can copy our computer and calculator programs to your disk or tape. The computer programs need either a $5\ 1/2$ or a $5\ 1/4$ -inch disk. The calculator programs need a $3\ 1/2$ disk, a mini data cassette, or program cards. We will help you modify our programs to meet your specific needs.

Those needing additional information should contact:

Commanding Officer
Attn. Aircraft Environmental Support Office, Code 61001
Naval Aviation Depot
North Island
San Diego, California 92135-5112

Commercial (619) 545-2901, Autovon 735-2901, FAX (619) 545-2910

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APPENDIX A

Calculator Programs

A1. PROGRAM AIRAP (HP-41C/41CV/41CX)

Al.l Description of Program AIRAP

Program AIRAP calculates:

- (1) emission indexes of carbon monoxide, carbon dioxide, oxides of nitrogen, and hydrocarbons as mass units per 1000 mass units of fuel, for example, as pounds per 1000 pounds (or grams per kilogram) of fuel;
- (2) the concentrations of the constituents of the exhaust, adjusted to a wet basis;
- (3) the concentration of oxygen in the exhaust;
- (4) the concentration of the oxides of nitrogen in the exhaust, adjusted to a concentration of 3% oxygen;
- (5) the concentration of water in the exhaust;
- (6) the fuel to air ratio;
- (7) the combustion efficiency; and
- (8) the emission rates for the formation of the constituents, in pounds (or kilograms) per hour, for a specified fuel flow rate.

Program AIRAP uses a group of equations to make calculations which are comparable to those made using the comprehensive matrix solution of ten combustion equations as explained in Reference Al. (See Paragraph Al.8) Program AIRAP uses a printer.

Al.2 Definitions

- EIz = the emission index of the constituent z in units of mass per 1000 units of mass of the fuel, i.e., pounds per 1000 pounds (or grams per kilogram) of fuel
- [z] = the mole fraction concentration of a constituent z in the exhaust, specifically the mole fraction concentration of carbon monoxide, carbon dioxide, oxides of nitrogen, nitric oxide, nitrogen dioxide, hydrocarbons, oxygen or water
- |z|s = the mole fraction concentration where s is 'ms' for measured,
 'w' for wet, 'sd' for semi-dry, 'd' for dry and 'c' for
 corrected
- M_z = the molecular weight of the constituent, specifically: carbon monoxide (28.0104), carbon dioxide (44.0098), nitrogen dioxide (46.0055), CHy/x (14.027, when y/x = 2/1); or methane (16.043)

- M_C = the atomic weight of carbon (12.011)
- $M_{\rm H}$ = the atomic weight of hydrogen (1.008)
- M_{AIR} = the molecular weight of air (28.965)
- α = the hydrogen-carbon ratio of the fuel, about 2 for JP-4 and about 1.8 for JP-5
- T = the mole fraction of carbon dioxide in the dry inlet air (0.00032)
- X = the number of moles of dry air per mole of fuel in the initial air-fuel mixture
- m, n = the molecular constants for carbon and hydrogen in the fuel $C_m H_n$
- x, y = the molecular constants for carbon and hydrogen in the exhaust hydrocarbons C_mH_n ; m is assumed equal to x and n to y
- h = the humidity of inlet air as moles of water vapor per mole of dry inlet air
- F = the fuel flow rate in pounds (or kilograms) of fuel per hour
- F/A = the fuel to air ratio
- J = the pressure-broadening coefficient for the effect of oxygen on carbon dioxide
- the interference coefficient for the effect of carbon dioxide on carbon monoxide
- L' = the interference coefficient for the effect of carbon dioxide on the oxides of nitrogen
- M = the interference coefficient for the effect of water on carbon monoxide
- M' = the interference coefficient for the effect of water on the oxides of nitrogen
- K = the ratio of wet concentration of a constituent to the completely dry concentration
- K_{sd} = the ratio of the completely dry concentration of a constituent to the semi-dry concentration
- S = the mole fraction of nitrogen plus argon in dry inlet air (0.7902)

- X/m, Z = intermediate numbers needed for calculations
- the efficiency of the converter for changing nitrogen dioxide into nitric oxide, expressed as the fraction of nitrogen dioxide converted

Al.3 Calculation of Emission Indexes

The program needs inputs of (a) the instrument interference coefficients, (b) the molecular constants for the fuel; (c) the humidity of the inlet air as moles of water vapor per mole of dry inlet air [or relative humidity, temperature (or dew point) and barometric pressure from which the program calculates the humidity of the inlet air]; (d) the concentrations of carbon monoxide, carbon dioxide, oxides of nitrogen, nitric oxide and hydrocarbons in the exhaust; and (e) the fuel flow rate. For convenience, the program accepts the concentrations in the units measured (ppm or %), and then converts them to the mole fraction concentrations.

For this program, the concentrations of carbon monoxide and carbon dioxide must be on the semi-dry basis, the concentration of hydrocarbons, wet and the concentration of the oxides of nitrogen either wet or semi-dry.

The user of the program makes the following operations:

- (1) selects either a wet or a semi-dry basis for the measurement of the oxides of nitrogen;
- (2) accepts the values of the instrument coefficients stored in registers 11 to 15 by the program, or changes them;
- (3) accepts the values of $(1 + h_{sd})$ and the efficiency of the oxides of nitrogen converter stored in registers 01 and 02 by the program, or changes them;
- (4) sets the molecular constants for carbon and hydrogen in the fuel;
- (5) either enters a value for h, or lets the program calculate it from an an entry of the appropriate combination of the relative humididy, dew point, temperature and barometric pressure; and
- (6) enters the concentrations of carbon monoxide, carbon dioxide, oxides of nitrogen, nitric oxide (if measured), hydrocarbons and fuel flow rate.

The program is complicated in that the concentration of oxygen is unknown and the concentrations of carbon dioxide and oxygen are interdependent. The program uses two iterations. It first determines approximate values for K, X/m, Z and the concentrations of oxygen and water. The

instrument interference coefficients and the concentrations of oxygen and water adjust the measured concentrations of carbon dioxide, carbon monoxide and the oxides of nitrogen. The adjusted measured concentrations determine new values for K, X/m, Z and the concentrations of oxygen and water, which again adjust the originally measured concentrations. The adjusted concentrations, on a wet basis, determine the emission indexes.

Figures Al to A5 give examples of the calculations. Most of the equations used in these calculations are those derived by Reference Al. For correlation, this paragraph identifies these equations with the notation 'SAE AIR 1533', for Reference Al; and a number in parenthesis, for the number assigned to the equation by Reference Al. These equations use the data of the 'Sample Calculation' on pages 34 and 35 of Reference Al.

These data are as follows:

```
J = 0.09
                   = 9.5
                                  carbon monoxide
                                                     = 500 ppm, semi-dry
L = -0.00013
                   = 19.0
                                  carbon dioxide
                                                        2.00%, semi-dry
               n
                   = 0.008843
L' = 0.14
               h
                                  oxides of nitrogen = 20 ppm, wet
               h_{sd} = 0.00607
M = -0.00045
                                  nitric oxide
                                                       9 ppm, wet
M' = 0.28
                   = 0.95
                                                     = 225 ppm, wet
                                  hydrocarbons
```

In addition, to show the capabilities of program AIRAP, one option uses relative humidity, ambient temperature and barometric pressure to calculate the value of h, and another option uses an arbitrary fuel flow rate to calculate the emission rates of the constituents.

A matrix solution of the combustion equations by the HP-41 calculator is possible but too slow for practical use. One of the steps, the inversion of the 10×10 matrix, takes about 19 minutes. Therefore, programs for this calculator use the derived algebraic equations.

CALCULATION OF Ksd

$$K_{sd} = 1 + h_{sd}$$
 SAE AIR 1533 (52)
= 1 + 0.00607 = 1.00607

CALCULATION OF $[CO]_d$, $[CO_2]_d$ AND $[NO_2]_d$ (These examples use concentrations adjusted for instrument interferences)

$$[z]_d = [z]_{sd} \times K_{sd}$$
 SAE AIR 1533 (53)
 $[CO]_d = 0.0004946 \times 1.00607 = 0.0004976$
 $[CO_2]_d = 0.02032 \times 1.00607 = 0.02044$
 $[NO_2]_d = ([NO_x]_{sd} - [NO]_{sd}) \times K_{sd}$
 $= (0.00002 - 0.000009) \times 1.00607 = 0.00001107$

(The calculation of $[NO_2]_d$ is needed only if $[NO_x]_{ms}$ is semi-dry.)

CALCULATION OF K (oxides of nitrogen measured wet)

When x = m and y = n, the last term in the numerator of equation SAE AIR 1533 (55), $[2+h][(y/2x)-(\alpha/2)][C_xH_y]_w$, is zero. The following example uses equation SAE AIR 1533 (55) without this term.

$$K = \frac{(2 + h) + (\alpha T/2 - h)(1 + [NO_2]_w - (2/x)[C_xH_y]_w)}{(2 + h)((\alpha/2)([CO]_d + [CO_2]_d) + 1) - (\alpha T/2 - h)(1 - [CO]_d)}$$
 SAE AIR 1533 (55)

when
$$(\alpha/2)([CC]_d + [CO_2]_d) + 1) = (2/2)(0.0004976 + 0.02044) + 1 = 1.02094$$

= $\frac{2.008843 + [(2 \times 0.00032/2) - 0.008843][1 + 0.00001172 - 2/9.5)(0.000225)]}{2.008843 \times 1.02094 - (2 \times 0.00032/2 - 0.008843)(1 - 0.0004976)}$

= 0.9713

Figure Al-1. Calculation of K_{sd} , $[CO]_d$, $[CO_2]_d$, $[NO_2]_d$ and K_{sd}

$$[O_2]_w = \left(\frac{[(1-S)(X/m)-\alpha/4]([CO]_w + [CO_2]_w + [C_XH_Y]_w)}{(1+TX/m)}\right)$$

 $-\frac{1}{2}[CO]_{w} - [CO_{2}]_{w} + (y/4x)[C_{x}H_{y}] - [NO_{2}]_{w} - \frac{1}{2}[NO]_{w}$

SAE AIR 1533 (78)

$$= \frac{((1 - 0.7902) \times 48.43 - 2/4)(0.0004833 + 0.01986 + 0.000225)}{(1 + 0.00032 \times 48.43)}$$

- $-\frac{1}{2}(0.0004883) 0.01986 + (19/38)(0.000225 0.00001172 \frac{1}{2}(0.0000091)$
- = 0.01757

CALCULATION OF [H20]

$$[H_2O]_w = \left(\frac{(\alpha/2 + hX/m) ([CO]_w + [CO_2]_w + [C_xH_y]_w)}{1 + TX/m}\right) - (y/2x)[C_xH_y]_w$$
SAE AIR 1533 (77)

$$= \frac{(2/2 + 0.008843 \times 48.43)(0.0004833 + 0.01986 + 0.000225)}{1 + 0.00032 \times 48.43} - (19/19)(0.000225)$$

= 0.0287

CALCULATION OF [02]sd

$$[0_2]_{sd} = [0_2]_d / K_{sd}$$
 SAE AIR 1533 (53)
= 0.1809/1.00607 = 0.1798

CALCULATION OF [CO2]c/sd

$$\{CO_2\}_{c} = [CO_2]_{ms} (1 + J[O_2])$$
 SAE AIR 1533 (18)
= 0.02 (1 + 0.09 x 0.1798) = 0.02032

Figure A1-3. Calculation of $[0_2]_w$, $[H_20]$, $[0_2]_{sd}$, and $[C0_2]_{c/sd}$

CALCULATION OF [CO]c/sd

$$[CO]_{c}$$
 = $[CO]_{ms}$ + $L[CO_{2}]$ + $M[H_{2}O]$ SAE AIR 1533 (13)
 $[CO]_{c/sd}$ = $[CO]_{ms}$ + $L[CO_{2}]$ + $M[H_{2}O]$
= 0.0005 + $(-0.00013 \times 0.02032)$ + $(-0.00045 \times 0.00607)$ = 0.0004946

$$[NO_x]_c = [NO_x]_{ms} \times (1 + L'[CO_2] + M'[H_2O])$$
 SAE AIR 1533 (14)
 $= 0.00002 \times (1 + 0.14 \times 0.02032 + 0.28 \times 0.0287) = 0.00002023$
 $[NO]_c = 0.000009 \times (1 + 0.14 \times 0.02032 + 0.28 \times 0.0287) = 0.0000091.$
 $[NO_2]_c = \frac{1}{\eta} \times [NO_2]_c$ SAE AIR 1533 (20)
 $= (1/0.95) \times (0.00002023 - 0.0000091) = 0.00001172.$

Then:

$$[NO_x]_c = [NO_2]_c + [NO]_c = 0.00001172 + 0.0000091 = 0.00002082$$

Note: When correcting $[NO_x]_{sd}$, use $[H_2O]$ as 0.00607.

CALCULATION OF EMISSION INDEX FOR CARBON MONOXIDE

$$EI_{CO} = \left(\frac{[CO]}{[CO] + [CO_2] + [C_xH_y]}\right) \left(\frac{10^3 \text{ M}_{CO}}{\text{M}_C + \alpha \text{M}_H}\right) (1 + TX/m)$$

$$= \frac{0.0004833}{(0.0004833 + 0.01986 + 0.000225)} \frac{1000 \times 28.011}{12.011 + 2 \times 1.008} \times (1 + 0.00032 \times 48.44)$$

$$= 47.65$$

Figure Al-4. Calculation of $[CO]_{c/sd}$, $[NO_x]_c$ and EI_{CO}

CALCULATION OF OXIDES OF NITROGEN AT 3% OXYGEN

[NO_X] at 3% oxygen = [NO_X]_m x
$$\frac{\text{oxygen in air (\%)} - 3\%}{\text{oxygen in air (\%)} - \text{oxygen in sample (\%)}}$$

[NO_X] at 3% oxygen = 20.8 x $\frac{20.948 - 3}{20.948 - 17.57}$ = 110.5 ppm

CALCULATION OF FUEL TO AIR RATIO (F/A)

$$F/A = \left(\frac{1}{X/m}\right) \left(\frac{M_C + \alpha M_H}{M_{air}}\right)$$

$$= \frac{1}{48.43} \left(\frac{12.011 + 2.016}{28.965}\right) = 0.009999$$
SAE AIR 1533 (59)

CALCULATION OF COMBUSTION EFFICIENCY

Combustion efficiency =
$$[1.00 - 4.346 \text{ (EI}_{CO}/H_c) - \text{EI}_{CxHy}/1000] \times 100$$

SAE AIR 1523 (75)
= $(1.00 - 4.346 \times 47.65/18370 - 11.11/1000) \times 100$
= 99.78%

where H_c is 18,730 Btu per pound.

Figure A1-5. Calculation of oxides of nitrogen at 3% oxygen, fuel to air ratio (F/A) and the combustion efficiency

Al.4 Description of Labels Used in Program AIRAP

LABEL USE

- A Initiates the input of data when the concentration of the oxides of nitrogen is measured on a wet basis.
- B Initiates the input of data when the concentration of the oxides of nitrogen is measured on a semi-dry basis.
- C Starts the calculation with the input of m, n and h using the set of instrument coefficients most recently stored.
- D Starts the program with the printing of the instrument coefficients, the values of m, n and h most recently stored, and the assigned values of h_{sd} and the efficiency of the nitrogen dioxide to nitric oxide converter.
- E Starts the program with the input of the concentration of the constituents. Label E does not print the instrument coefficients, the variables m, n, h, h_{sd} and the efficiency of the nitrogen dioxide to nitric oxide converter. Use Label E to continue a series of calculations for the same engine at different power settings.
- F Sets all instrument coefficients at zero and starts the program with the input of m, n and h.
- G Prints values for the constant K, and the intermediate numbers Z and X/m.

Al.5 Instructions for using program AIRAP

KEYSTROKES DISPLAY

REMARKS

MINIMUM SIZE 045

XEQ AIRAP	KEY A OR B	Program AIRAP needs inputs of the concentrations of carbon monoxide and carbon dioxide measured semi-dry, of hydrocarbons measured wet, and of oxides of nitrogen measured either wet (label A) or semi-dry (label B). This example uses a wet measurement of the concentration of the oxides of nitrogen. Key in A.
A	SET 11-15	The program sets the instrument coefficients at $J = -0.07$, $L = -0.00013$, $L' = 0.14$, $M = -0.00045$, and $M' = 0.28$, and stores them in registers 11 to 15. To use different coefficients change the numbers in registers 11 to 15. For example, to change the value of J to 0.09, key in .09 then STO 11. To set all instrument coefficients to zero, key in label F. This label uses the function 'CL Σ ' to clear registers 11 to 16, which are the ones normally assigned as statistical registers and which, in this program, store the instrument coefficients.
.09	•00	Key in STO 11.
STO 11	.0900	Label A (or label B) also sets the values of other variables. The user may wish to change some of these numbers. Either make changes in the program, or make changes by storing new values for the variables in the appropriate registers. See list on page Al-15. Key in R/S to continue.
P/S	м?	Key in the the molecular constant m for the fuel $c_m \mbox{H}_n$.
9.5	9.5	Key in R/S to continue.
R/S	N?	Key in the molecular constant n.
19	19	Key in R/S to continue.
R/S	HUMIDITY?	Key in the humidity of the inlet air. If it is not known, key in zero and use option l elsewhere in this program. This demonstration continues as if the humidity

of the inlet air is known.

demonstration continues as if the humidity

Instructions for using program AIRAP (continued)

KEYSTROKES	DISPLAY	REMARKS
.008843	.008843	Key in R/S to continue.
R/S	CO?	The first two lines of the print-out show the input values of the instrument coefficients in the order
		J L L' M M'.
		The third line shows the input values of m, n and the humidity of the inlet air. The fourth line shows the values assigned to the humidity of the gas sample (semidry) and the converter efficiency. Key in the concentration of carbon monoxide as ppm.
500	500	Key in R/S to continue.
R/S	CO2?	Key in the concentration of carbon dioxide as x .
2	2	Key in R/S to continue.
R/S	NOX?	Key in the concentration of oxides of nitrogen as ppm.
20	20	Key in R/S to continue.
R/S	NO?	Key in the concentration of nitric oxide as ppm. Or, if the concentration of nitric oxide was not measured, either make no entry or key in zero.
ò	9	Key in R/S to continue. If there is no entry for the concentration of nitric oxide, 'key in R/S' sets the concentration of nitric oxide at 97% of the concentration of the oxides of nitrogen.
R/S	СХНҮ?	The print-out shows the inputs of the concentrations of carbon monoxide, carbon dioxide, oxides of nitrogen and nitric oxide. Key in the concentration of hydrocarbons as ppm.
225	225	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate if known, other- wise make no entry. See option 2. This

Instructions for using program AIRAP (continued)

KEYSTROKES	DISPLAY	REMARKS
		demonstration uses a sample calculation from Reference Al for which a fuel flow rate was not specified.
		Key in R/S to continue.
R/S	CO?	The first print-out shows the concentration of hydrocarbons. The program continues to run. The second print-out, after about 32 seconds, shows the emission indexes of the constituents; the concentrations of the constituents on a wet basis, corrected for instrument interferences; the concentration of oxygen in the exhaust (% wet); the concentration of oxides of nitrogen (ppm) adjusted to 3% oxygen; the concentration of water (%) in the exhaust; the fuel to air ratio and the combustion efficiency (%). Continue with another set of concentrations (the program is at label E) or select A, B, C, or D. Refer to Paragraph Al.4 for the use of each label. Key in C to restart the calculation using the instrument coefficients of the previous calculation.
С	M?	Key in the the molecular constant m for the fuel $\mathrm{C}_{\mathfrak{m}}\mathrm{H}_{n}$.
9.5	9.5	Key in R/S to continue.
R/S	N?	Key in the molecular constant n.
19	19	Key in R/S to continue.
R/S	HUMIDITY?	Assume an unknown humidity for the inlet air. Use option I to calculate it.
		Option 1
		Key in zero.
0	0	Zero indicates that the humidity of the inlet air is not known. The program must calculate it. Key in R/S to continue.
R/S	RH?	Key in the relative humidity as percent. To use a dew point instead of a relative humidity, key in 100 for the relative humidity.

Instructions for using program AIRAP (continued)

KEYSTROKES	DISPLAY	REMARKS
30	30	Key in R/S to continue.
R/S	T?	Key in the temperature as degrees F.
75	75	Key in R/S to continue.
R/S	В?	Key in the barometric pressure as inches of mercury.
29.92	29.92	Key in R/S to continue.
R/S	co?	The first two lines of print-out show the input values of the instrument coefficients. The third line shows the input values of m, n and the humidity of the inlet air as calculated from the relative humidity. The fourth line shows the values assigned to the humidity of the gas sample (semi-dry) and the converter efficiency. The fifth line shows the relative humidity, temperature and barometric pressure. Key in the concentrations of carbon monoxide, carbon dioxide, the oxides of nitrogen, nitric oxide and hydrocarbons as directed in the preceding paragraphs, then

R/S	FUEL?	Key in a fuel flow rate. For this demonstration use an arbitrary fuel flow rate of 1000 pounds per hour.
1000	1000	Key in R/S to continue.
R/S	co?	The next print-out shows the concentration of hydrocarbons and the fuel flow rate. The print-out continues as previously described adding the emissions of the constituents, in pounds per hour. Note that the print-out also gives the amount of sulfur dioxide calculated as if all of the sulfur content of the fuel (estimated at 0.02%) changed to sulfur dioxide. To use a different concentration of sulfur in the fuel, change the number in program step 32.

Option 2

Instructions for using program AIRAP (concluded)

KEYSTROKES	DISPLAY	REMARKS		
		Option 3	-	
G	co?	Label G prints the values of K, Z, used in the preceding calculation turns the program to label E.		

Some of the registers contain variables which the user may want to change before running the program. These are as follows.

Register	Program line	Variable
01	11	1.00607 1 + h _{sd}
02	13	97.95 This register contains two variables. The format is xx.yy where xx is the percent (97) of nitrogen oxide in the oxides of nitrogen, and yy is the percent (95) of nitrogen dioxide changed to nitrogen oxide by the converter.
11	15	-0.07 Instrument coefficient J
12	17	-0.00013 Instrument coefficient L
13	19	0.14 Instrument coefficient L'
14	21	-0.00045 Instrument coefficient M
15	23	0.28 Instrument coefficient M'
32	25	0.02 Percent sulfur in the fuel
39	27	0.00032 T, the mole fraction of carbon dioxide in dry inlet air

Al.6 Program Listing for AIRAP

01+LBL "AIRAP"	51 RCL 39	101 1	151 GTO 19
92 KEY A OR 8"	52 *	102 -	152+LBL 17
93 PROMPT	53 STO 90	193 FIX 5	153 .038251
94+LBL A	54 "HUMIDITY?"	184 ACX	154 *
05 SF 03	55 PROMPT	195	155 EtX
96 GTO 29	56+LBL 16	186 ACA	156 .053226
97+LBL B	57 STO 93	187 RCL 82	157 GTO 19
98 CF 93	58 ST+ 09	108 FRC	158+LBL 18
09+LBL 20	59 -	109 FIX 2	159 .035264
19 FIX 4	60 STO 10	110 ACX	160 *
11 1.00607	61 RCL 09	111 PRBUF	161 EtX
12 STO 01	62 2	112 FC? 88	162 .061928
13 97.95	63 X=Y?	113 GTO E	163+LBL 19
14 STO 92	64 GTO "RH"	114 ADY	164 *
1507	65+LBL D	115 FIX 0	165 RCL 36
16 STO 11	66 FIX 2	116 RCL 36	166 1 E2
1700013	67 RCL 11	117 ACX	167 /
18 STO 12	68 ACX	118 • •	168 *
19 .14	69 • •	119 ACA	169 ENTERT
20 STO 13	79 ACA	120 RCL 37	179 "8?"
2100045	71 RCL 12	121 ACX	171 PROMPT
22 STO 14	72 ACX	122	172 STO 38
23 .28	73 • •	123 ACA	173 X<>Y
24 STO 15	74 ACA	124 FIX 2	174 -
25 .02	75 RCL 13	125 RCL 38	175 /
26 STO 32	76 ACX	126 RCX	176 PRBUF
27 .00032	77 PRBUF	127 PRBUF	177 ADY
28 STO 39	78 • •	128 ADV	178 RCL 90
29 GTO 11	79 ACA	129 CF 00	179 X<>Y
39+LBL F	80 RCL 14	139 GTO E	180 GTO 16
31 CLS	81 ACX	131+LBL -RH-	181+LBL E
32 GTO C	82	132 SF 00	182 ADV
33+LBL 11	83 ACA	133 *RH?*	183 FIX 1
34 "SET 11-15"	84 RCL 15	134 PROMPT	184 °C0?"
35 PROMPT	85 ACX	135 STO 36	185 PROMPT
36+LBL C	86 PRBUF	136 *1?*	186 ACX
37 FIX 1	87 ADY	137 PROMPT	187 1 E6
38 -M?-	88 FIX 1	138 STO 37	188 /
39 PROMPT	89 RCL 87	139 50	189 STO 21
40 STO 07	90 ACX	140 RCL 37	190 STO 41
41 STO Y	91 RCL 8 8	141 X<=Y?	191 °C02?"
42 "N?"	92 ACX	142 GTO 17	192 PROMPT
43 PROMPT	93 RCL 03	143 75	193 FIX 2
44 STO 88	94 FIX 6	144 X()Y	194 ACX
45 X<>Y	95 ACX	145 X(=Y?	195 1 E2
46 /	96 FIX 1	146 GTO 18	196 /
47 STO 96	97 PRBUF	147 .031767	197 STO 22
48 2	98	148 *	198 STO 42
49 STO 09	99 ACA	149 EtX	199 FIX 1
50 /	100 RCL 01	150 .080455	200 NOX?"

Program Listing for AIRAP (continued)

	ACT UCA 10	701 001 04	751 4
201 PROMPT	251 XEQ 10	391 RCL 24	351 *
292 FIX 1	252 RCL 41	302 STO 31	352 STO 31
293 ACX	253 STO 21	393 -	353+LBL *Z*
294 1 E6	254 RCL 42	304 +	354 2
285 /	255 STO 22	305+LBL 12	355 RCL 28
	256 RCL 43	306 RCL 25	356 -
286 STO 23		387 2	
287 STO 43	257 STO 23		357 2
208 .	258 RCL 44	308 *	358 RCL 97
289 -NO?*	259 STO 24	309 RCL 07	359 /
210 PROMPT	260 XEQ 95	310 /	360 RCL 08
211 X=9?	261 XEQ 18	311 -	361 RCL 97
212 GTO 93	262 GTO 96	312 RCL 18	362 /
213 GTO 84	263+LBL 19	313 *	363 2
214+LBL 93	264+LBL *K*	314 RCL 09	364 /
215 RCL 23	265 RCL 21	315 +	365 -
	266 RCL 01	316 STO 88	366 RCL 25
216 1 E6			
217 *	267 *	317 RCL 17	367 *
218 RCL 02	268 STO 35	318 RCL 09	369 -
219 IHT	269 LASTX	319 *	369 RCL 38
229 1 E2	270 RCL 22	329 RCL 10	378 RCL 31
221 /	271 *	321 1	371 -
222 *	272 STO 36	322 RCL 35	372 +
223+LBL 94	273 FS? 83	323 -	373 RCL 28
224 ACX	274 GTO 21	324 FS? 83	374 RCL 29
225 1 E6	275 RCL 23	325 GTO 13	375 RCL 25
225 / 20	276 RCL 81	326 RCL 48	376 +
	277 *	327 +	377 +
227 STO 24			
228 STO 44	278 510 37	328 • LBL 13	378 STO 95
229 PRBUF	279 LASTX	329 *	379 /
238 -CXHY?-	280 RCL 24	339 -	389 STO 19
231 PROMPT	281 *	331 RCL 99	381 2
232 ACX	282 STO 38	332 X(>Y	382 *
233 1 E6	283 -	333 /	383 RCL 86
234 /	284 STO 49	334 STO 18	384 -
235 STO 25	285+LBL 21	335 RCL 35	385 1
	286 RCL 35	336 X()Y	386 RCL 83
•••	287 RCL 36	337 *	387 +
237 .		338 STO 28	388 RCL 19
238 *FUEL?*	288 +		
239 PROMPT	289 RCL 96	339 RCL 36	389 RCL 39
249 STO 27	290 2	348 LASTX	398 *
241 X=9?	291 /	341 *	391 2
242 GTO 14	292 *	342 STO 29	392 /
243 * FUEL =*	293 l	343 FS? 03	393 -
244 ACA	294 +	344 GTO "Z"	394 4
245 ACX	295 STO 17	345 RCL 37	395 *
246+LBL 14	296 1	346 LRSTX	396 /
247 PRBUF	297 FC? 83	347 *	397 STO 20
248 ADY	298 GTO 12	348 STO 30	398 RCL 39
249 XEQ 19	299 RCL 23	349 RCL 38	399 *
	300 STO 30	350 LASTX	400 1
259 XEQ 95	300 310 30	JJ9 ENJIA	700 1

Program Listing for AIRAP (continued)

401 +	451 /	501 ADY	551 12011
402 STO 34	452 2	502 FIX 6	552 RCL 96
403+LBL 22	453 /	503 °K =-	553 1008
404 RCL 20	454 -	504 RCL 18	554 +
405 .2098	455 STO 33	505 XEQ 02	555 +
486 *	456 RTH	506 °Z ="	556 RCL 25
407 RCL 06	457+LBL 05	507 RCL 19	557 STO 16
408 4	458 RCL 26	508 XEQ 02	558 XEQ 91
409 /	459 RCL 01	509 RCL 20	559 "CXHY, CH4 ="
410 -	469 /	518 "X/"	560 RCL 2 5
411 RCL 05	461 RCL 18	511 ACA	561 16943
412 *	462 /	512 SF 13	562 XEQ 81
413 RCL 34	463 RCL 11	513 TH =-	563 ADV
414 /	464 *	514 XEQ 02	564 "CO HET ="
415 RCL 28	465 1	515 CF 13	565 RCL 28
416 2	466 +	516 ADV	566 1 E6
417 /	467 ST* 22	517 GTO E	567 *
418 -	468 RCL 22	518+LBL 06	568 FIX 1
419 RCL 29	469 RCL 12	519 RCL 06	569 XEQ 02
429 -	479 *	529 1.998	570 °CO2 WET ="
421 RCL 06	471 RCL 14 472 RCL 81	521 * 522 12.011	571 RCL 29 572 1 E2
422 4 423 /	473 1	523 +	573 *
424 RCL 25	474 -	524 STO 84	574 FIX 3
425 *	475 *	525 RCL 38	575 XEQ 02
426 +	476 +	526 RCL 31	576 "NOX WET ="
427 RCL 30	477 ST+ 21	527 -	577 RCL 31
428 RCL 31	478 RCL 22	528 RCL 02	578 1 E6
429 -	479 RCL 13	529 FRC	579 *
430 -	489 *	530 /	589 FIX 1
431 RCL 31	481 RCL 15	531 ST+ 31	581 XEQ 02
432 2	482 FS? 03	532 21	582 "CXHY WET ="
433 /	483 GTO 07	533 STO 00	583 RCL 16
434 -	484 GTO 98	534 " EI "	584 1 E6
435 STO 26	485+LBL 97	535 ACA	585 *
436 RCL 93	486 RCL 33	536 FIX 2	586 XEQ 92
437 RCL 20	487 GTO 99	537 ADV	587 ADV
438 *	488+LBL 98	538 °C0 = °	588 *% OXYGEN, WET =*
439 RCL 06	489 RCL 01	539 RCL 28	589 FIX 2
449 2	499 1	540 28911	590 RCL 26
441 /	491 - 492•LBL <i>9</i> 9	541 XEQ 01	591 1 E2
442 + 443 RCL 05	493 *	542 *CO2 =* 543 RCL 29	592 * 593 XEQ 02
444 *	494 +	544 44009.8	594 RCL 31
445 RCL 34	495 1	545 XEQ 91	595 1 E6
446 /	496 +	546 *NOX =*	596 *
447 RCL 16	497 ST* 23	547 RCL 31	597 FIX 1
448 RCL 88	498 ST* 24	548 46005.5	598 RCL Y
449 *	499 RTN	549 XEQ 81	599 20.948
450 RCL 07	500+LBL G	550 TCXHY, CHY/XT	600 -
		ees willing and it	

Program Listing for AIRAP (concluded)

691 CHS 692 17.948 692 17.948 692 17.948 693 XCY 653 STO 80 694 / 654 ADV 793*LBL 26 694 / 655 RCL Y 655 RCL Y 655 RCL 27 795 * 696 * 656 X=8? 796 KEQ 92 697 FIX 9 698 * HOX AT 3% 02 = * 658 FIX 2 699 XEQ 92 651 POUNDS PER HOUR* 611 1 E2 661 ADV 612 * 662 1 E3 661 RCL 613 662 AC2 614 "HATER = * 664 STO Y 615 ACA 665 *CO = * 616 ACA 617 *%* 617 *%* 618 ACA 667 *CO2 = * 618 ACA 668 XEQ 26 617 *%* 669 XEQ 26 621 *F/A = * 671 *CHY/X = * 622 I G72 XEQ 26 621 *F/A = * 623 ENTER† 624 RCL 20 625 *A XEQ 26 625 / 675 RCL 27 626 RCL 04 637 *CO2 = * 630 XEQ 02 631 1 631 XEQ 02 632 ENTER† 633 RCL 21 633 RCL 21 634 XEQ 02 635 *CO2 = * 631 1 631 XEQ 02 632 ENTER† 633 RCL 21 633 RCL 21 634 XEQ 02 635 *CO2 = * 635 *A 346 648 CQ 068 649 *CQ 649 *CQ 649 *CQ 644 * 649 *CQ 640 *CQ 64			704 0811
683 X(>Y	601 CHS		
683 X(>Y	602 17.948	652 21	
685 RCL Y 686 * 686 * 686 * 687 FIX 9 687 FIX 9 688 *NOX AT 3% 02 = * 688 FIX 2 688 RCL 33 689 RCL 33 689 RCL 33 689 RCL 34 681 I E2 681 RCL 33 681 RCL 33 681 RCL 34 681 RCL 33 681 RCL 34 681 RCL 35 681 RCL 36 681 RCL 36 681 RCL 36 681 RCL 37 681 RCL 38 682 RCL 38 683 RCL 38 684 RCL 38 685 RCL 38 686 RCL 38 686 RCL 38 687 RCL 38 687 RCL 38 688 RCL 38	603 X<>Y		
686 * 656 X=9? 796 XEQ 92 687 FIX 8 657 GTO E 787 X()Y 688 "NOX AT 37 32 02 = 658 FIX 2 798 STO Y 689 XEQ 82 659 "POUNDS PER HOUR" 789 ISG 88 611 I E2 661 RIV 711 RTN 612 * 662 I E3 712 .ENB. 613 FIX 2 663 / 614 "NATER = 664 STO Y 615 RCA 665 "CO = 665 "CO = 666 KEQ 26 617 "2" 667 "CO2 = 667 "CO2 = 618 RCA 668 KEQ 26 619 RDV 669 "NO2 = 620 ENTERN 669 "NO2 = 620 ENTERN 669 "NO2 = 620 FIX 6 670 KEQ 26 621 "F/A = 571 "CHY/X = 622 I 672 KEQ 26 622 I 672 KEQ 26 623 ENTERN 673 "CH4 = 624 KCQ 26 624 RCL 20 674 KEQ 26 625 / 675 RCL 27 626 RCL 84 676 RCL 32 627 * 677 "R2 628 28.965 678 * 629 / 679 * 630 KEQ 92 680 "SO2 = 631 I 681 KEQ 82 631 I 681 KEQ 82 633 RCL 21 683*LBL 81 634 18739 684 RCA 635 / 685 * 636 4.346 686 RCL 84 637 * 687 / 638 - 688 RCL 85 639 RCL 24 689 / 649 1809 699 RCL 34 641 / 691 * 642 - 692 RCX 643 I E2 693 STO IND 80 644 * 694 ISG 80 645 FIX 2 695*LBL 80 646 *CCMB. EFF. = 696 RDV 647 RCA 648 RCX 699*LBL 82 649 "%" 699 RCA			
687 FIX 0 688 *MOX AT 3% 02 = * 658 FIX 2 788 STO Y 689 *MOX AT 3% 02 = * 658 FIX 2 788 STO Y 689 *XEQ 92 659 *POUNDS PER HOUR* 789 ISG 08 618 RCL 33 668 RCA 71094LBL 08 611 I E2 661 RDV 711 RTN 612 * 662 I E3 712 .END. 613 FIX 2 663 / 614 *MATER = * 664 STO Y 615 RCA 665 *CO = * 616 RCX 666 XEQ 26 617 *Z* 667 *CO2 = * 618 RCA 668 XEQ 26 619 RDV 669 *NO2 = * 620 FIX 6 670 XEQ 26 621 *F/A = * 571 *CHY/X = * 622 I 672 XEQ 26 621 *F/A = * 571 *CHY/X = * 622 I 672 XEQ 26 623 ENTER1 673 *CH4 = * 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 688 *SO2 = * 631 I 681 XEQ 02 632 ENTER1 682 GTO E 633 RCL 21 683*LBL 01 633 RCL 21 683*LBL 01 634 18730 684 RCA 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCA 643 I E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695*LBL 00 646 *COMB. EFF. = * 696 RDV 647 RCA 649 *Z* 699 RCA			
608 *NOX AT 3% 02 = 658 FIX 2 708 STO Y 609 XEQ 02 659 *POUNDS PER HOUR* 709 ISC 00 610 RCL 33 660 ACA 719*LBL 00 611 1 E2 661 ADV 711 RTN 612 * 662 1 E3 712 .END. 613 FIX 2 663 / 614 *NATER = 664 STO Y 615 ACA 665 *CO = 665 *CO = 661 ADV 669 *NO2 = 661 ADV 66			
609 XEQ 02 610 RCL 33 660 RCA 710+LBL 08 611 1 E2 661 RDV 711 RTN 612 * 662 1 E3 712 .END. 614 "MATER =" 664 STD Y 615 RCR 665 "CO =" 616 RCX 666 KEQ 26 617 "2" 667 "CO2 =" 618 RCR 668 KEQ 26 619 RDV 669 "NO2 =" 620 FIX 6 621 "F/R = " 671 "CHY/X =" 622 1 672 XEQ 26 623 ENTER1 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 626 RCL 04 677 .02 628 28.965 678 * 629 / 628 ENTER1 673 "CH4 =" 624 RCL 20 675 RCL 27 626 RCL 04 677 .02 628 28.965 678 * 629 / 630 XEQ 02 631 1 631 XEQ 02 631 1 631 XEQ 02 633 RCL 21 633 RCL 21 634 18730 685 * 636 4.346 686 RCL 04 637 * 638 - 638 CL 05 639 RCL 24 669 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 644 * 649 1000 645 FIX 2 646 *COMB. EFF. = " 696 RCR 697 RCN 648 RCX 699 RCR 649 "2" 699 RCR			
619 RCL 33 669 RCA 719 LBL 08 611 1 E2 661 RDV 711 RTN 612 * 662 1 E3 712 .END. 613 FIX 2 663 / 614 "MATER = 664 STO Y 615 RCR 665 "CO = 667 "CO2 = 668 KEQ 26 617 "\" 667 "CO2 = 667 "CO2 = 668 KEQ 26 619 RDV 669 "NO2 = 669 "NO2 = 622 FIX 6 621 "F/A = 670 KEQ 26 621 "F/A = 670 KEQ 26 621 "F/A = 670 KEQ 26 622 I 672 KEQ 26 623 ENTER† 673 "CH4 = 674 KEQ 26 625 / 675 RCL 27 626 RCL 04 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 KEQ 02 631 1 681 KEQ 02 632 ENTER† 633 RCL 21 633 RCL 21 634 18730 684 RCR 635 / 685 * 636 4.346 637 * 638 - 688 RCL 04 637 * 638 - 688 RCL 05 639 RCL 24 669 / 669 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 644 "COMB. EFF. = 696 RDV 645 FIX 2 646 "COMB. EFF. = 696 RDV 646 "COMB. EFF. = 696 RDV 647 RCR 648 RCX 649 "\" 649 "\" 649 RCR 649 "\"	608 "NOX AT 3% 02 ="		
611 1 E2 661 ADV 711 RTN 612 * 662 1 E3 712 .END. 613 FIX 2 663 / 614 "NATER =" 664 STO Y 615 ACR 665 "CO =" 616 ACX 666 XEQ 26 617 "%" 667 "CO2 =" 618 ACR 668 XEQ 26 619 ADV 669 "NO2 =" 620 FIX 6 670 XEQ 26 621 "F/A = " 571 "CHY/X =" 622 1 672 XEQ 26 621 "F/A = " 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 "R2 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 6834LBL 01 633 RCL 21 6834LBL 01 633 RCL 21 6834LBL 01 634 18730 684 ACR 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 649 1000 690 RCL 34 641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695 CRC 646 COMB. EFF. = " 696 ADV 647 ACR 697 RTN 648 ACX 698+LBL 02 649 "%" 699 ACR	609 XEQ 02		
612 * 662 1 E3 712 .END. 613 FIX 2 663 / 614 "NATER =" 664 STO Y 615 ACA 665 "CO =" 616 ACX 666 KEQ 26 617 "2" 667 "CO2 =" 618 ACA 668 KEQ 26 619 ADV 669 "NO2 =" 620 FIX 6 670 KEQ 26 621 "F/A = " 571 "CHY/X =" 622 1 672 KEQ 26 623 ENTER† 673 "CH4 =" 624 RCL 20 674 KEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 KEQ 02 631 1 681 KEQ 02 631 1 681 KEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683*LBL 01 634 18730 684 ACA 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 LSC 00 645 FIX 2 695*LBL 00 646 "COMB. EFF. = " 696 ADV 647 ACA 698*LBL 02 649 "%" 699 RCA			
613 FIX 2 614 "NATER =" 664 STO Y 615 ACR 665 "CO =" 616 ACX 666 XEQ 26 617 "2" 667 "CO2 =" 618 ACR 669 XEQ 26 619 ADV 669 "NO2 =" 620 FIX 6 621 "F/A = " 621 1 672 XEQ 26 622 1 673 "CH4 =" 623 ENTER† 624 RCL 20 625 / 626 RCL 04 627 * 627 * 628 28.965 639 XEQ 02 631 1 681 XEQ 02 632 ENTER† 633 RCL 21 634 18730 635 / 636 4.346 637 * 638 - 639 RCL 24 640 1000 641 / 642 - 643 1 E2 644 * 645 FIX 2 646 "COMB. EFF. = " 659 ACR 647 RCL 648 ACR 649 "%" 659 ACR 649 "%" 659 ACR 649 "%" 659 ACR 650 ACR	611 1 E2		
614 *MATER =" 664 STO Y 615 ACR 665 *CO =" 616 RCX 666 *EQ 26 617 *Z** 667 *COZ =" 618 ACR 668 *EQ 26 619 RDY 669 *MOZ =" 620 FIX 6 670 XEQ 26 621 *F/R = " 571 *CHY/X =" 622 1 672 XEQ 26 623 ENTER† 673 *CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 *QZ 628 28.965 678 * 629 / 679 * 638 XEQ 02 680 *SOZ =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683*LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695*LBL 00 646 *COMB. EFF. = " 696 RDY 647 RCR 648 RCX 698*LBL 02 649 *Z** 699 RCR	612 *		712 .END.
615 ACR 665 *CD = * 616 RCX 666 XEQ 26 617 *Z** 667 *CD2 = * 618 ACR 668 XEQ 26 619 RDV 669 *ND2 = * 620 FIX 6 678 XEQ 26 621 *F/A = * 571 *CHY/X = * 622 1 672 XEQ 26 623 ENTER† 673 *CH4 = * 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 *SD2 = * 631 1 681 XEQ 02 631 1 681 XEQ 02 631 1 681 XEQ 02 633 RCL 21 683*LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STD IND 00 644 * 694 ISC 00 645 FIX 2 695*LBL 00 646 *CDMB. EFF. = * 696 RDV 647 RCR 697 RTN 648 RCX 698*LBL 02 649 *Z** 699 RCR	613 FIX 2		
615 ACR 665 *CD = * 616 RCX 666 XEQ 26 617 *Z** 667 *CD2 = * 618 ACR 668 XEQ 26 619 RDV 669 *ND2 = * 620 FIX 6 678 XEQ 26 621 *F/A = * 571 *CHY/X = * 622 1 672 XEQ 26 623 ENTER† 673 *CH4 = * 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 *SD2 = * 631 1 681 XEQ 02 631 1 681 XEQ 02 631 1 681 XEQ 02 633 RCL 21 683*LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STD IND 00 644 * 694 ISC 00 645 FIX 2 695*LBL 00 646 *CDMB. EFF. = * 696 RDV 647 RCR 697 RTN 648 RCX 698*LBL 02 649 *Z** 699 RCR	614 "WATER ="		
617 "2" 667 "CO2 =" 618 ACA 668 XEQ 26 619 ADV 669 "NO2 =" 620 FIX 6 670 XEQ 26 621 "F/A = " 571 "CHY/X =" 622 1 672 XEQ 26 623 ENTER† 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 19730 684 ACA 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 680 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 ADV 647 ACA 697 RTH 648 ACX 698+LBL 02 649 "%" 699 ACA	615 ACA		
618 RCR 668 XEQ 26 619 RDV 669 "HO2 =" 620 FIX 6 670 XEQ 26 621 "F/A = " 571 "CHY/X =" 622 1 672 XEQ 26 623 ENTER† 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 RDV 647 RCR 697 RTH 648 RCX 698+LBL 02 649 "%" 699 RCR	616 ACX		
619 RDV 669 "NO2 =" 620 FIX 6 670 XEQ 26 621 "F/A = " 571 "CHY/X =" 622 1 672 XEQ 26 623 ENTER† 673 "CH4 =" 624 RCL 29 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR	617 *%*		
629 FIX 6 621 "F/A = " 621 "F/A = " 622 1 623 ENTER1 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER1 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCL 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 RDV 647 RCR 648 RCX 698+LBL 02 649 "%" 699 RCR	618 ACA		
621 "F/A = "	619 ADV		
622 1 672 XEQ 26 623 ENTER† 673 "CH4 =" 624 RCL 20 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = 696 RDV 647 RCR 648 RCX 698+LBL 02 649 "%" 699 RCR	620 FIX 6		
623 ENTER† 624 RCL 20 625 / 626 RCL 84 627 * 627 RCL 27 628 28.965 629 / 630 XEQ 82 631 1 631 XEQ 82 632 ENTER† 632 ENTER† 633 RCL 21 634 18738 634 18738 635 / 636 4.346 637 * 638 - 638 RCL 84 637 * 638 - 639 RCL 24 640 1000 641 / 642 - 643 1 E2 643 1 E2 644 * 644 - 645 FIX 2 646 "COMB. EFF. = " 648 RCX 649 "2" 649 RCC 649 R	621 *F/A = *		
624 RCL 29 674 XEQ 26 625 / 675 RCL 27 626 RCL 04 676 RCL 32 627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 *SO2 =* 631 1 681 XEQ 02 632 ENTER1 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 ACA 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 **COMB. EFF. = ** 696 ADY 647 ACA 697 RTN 648 ACX 698+LBL 02 649 *2* 699 ACA	622 1		
625 / 675 RCL 27 626 RCL 84 676 RCL 32 627 * 677 .82 628 28.965 678 * 629 / 679 * 630 XEQ 82 688 "SO2 =" 631 1 681 XEQ 82 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 81 634 18738 684 RCR 635 / 685 * 636 4.346 686 RCL 84 637 * 687 / 638 - 688 RCL 85 639 RCL 24 689 / 640 1800 698 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 80 644 * 694 ISG 80 645 FIX 2 695+LBL 80 646 "COMB. EFF. = " 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 82 649 "%" 699 RCR	623 ENTERT		
626 RCL 84 627 * 628 28.965 629 / 630 XEQ 82 631 1 631 XEQ 82 631 1 632 ENTER† 633 RCL 21 634 18738 635 / 636 4.346 637 * 638 - 638 RCL 24 640 1980 690 RCL 34 641 / 642 - 643 1 E2 643 1 E2 644 * 645 FIX 2 646 "COMB. EFF. = " 648 RCX 649 "%" 657 RCR 657 RCR 657 RCR 657 RCR 658 RCR 658 RCR 658 RCR 658 RCR 659 RCR	624 RCL 20		
627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 *SO2 = 631 1 681 XEQ 02 631 1 682 GTO E 633 RCL 21 683*LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695*LBL 00 646 *COMB. EFF. = 696 RDV 647 RCR 697 RTN 648 RCX 698*LBL 02 649 *% 699 RCR	625 /		
627 * 677 .02 628 28.965 678 * 629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 632 ENTER1 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 646 "COMB. EFF. = 696 RDV 647 RCR 697 RTH 648 RCX 698+LBL 02 649 "%" 699 RCR	626 RCL 94		
629 / 679 * 630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 631 1 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = 696 RDY 647 RCR 698+LBL 02 649 "%" 699 RCR			
630 XEQ 02 680 "SO2 =" 631 1 681 XEQ 02 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 RCR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 RDY 647 RCR 698+LBL 02 649 "%" 699 RCR	628 28.965		
631 1 681 XEQ 62 632 ENTER† 682 GTO E 633 RCL 21 683+LBL 01 634 18730 684 ACR 635 / 685 * 636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = "696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR	629 /		
632 ENTER† 633 RCL 21 634 18730 635 / 636 4.346 637 * 638 - 639 RCL 24 640 1000 641 / 642 - 643 1 E2 643 1 E2 644 * 645 FIX 2 646 "COMB. EFF. = " 648 GCR 649 "%" 649 RCR 649 RCR 649 RCR 640 RCR 640 RCR 641 / 642 - 644 * 645 FIX 2 646 "COMB. EFF. = " 646 RCR 647 RCR 648 RCR 648 RCR 649 "%" 649 RCR 649 RCR 640 RCR 641 RCR 641 RCR 642 RCR 644 RCR 645 FIX 2 646 RCR 646 RCR 647 RCR 647 RCR 648 RCR 648 RCR 649 RCR			
633 RCL 21 683+LBL 01 634 18730 684 RCA 635 / 685 * 636 4.346 686 RCL 04 637 * 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = "696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR			
634 18739 684 ACR 635 / 685 * 636 4.346 686 RCL 04 637 * 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 *COMB. EFF. = * 696 ADV 647 ACR 697 RTN 648 ACX 698+LBL 02 649 *%* 699 ACR			
635 / 636 4.346 686 RCL 04 637 * 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 **COMB. EFF. = ** 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 **%** 699 RCR			
636 4.346 686 RCL 04 637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 **COMB. EFF. = ** 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 *%** 699 RCR			
637 * 687 / 638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = 696 RDY 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR			
638 - 688 RCL 05 639 RCL 24 689 / 640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695*LBL 00 646 "COMB. EFF. = 696 RDY 647 RCR 697 RTN 648 RCX 698*LBL 02 649 "%" 699 RCR	636 4.346		
639 RCL 24 640 1000 690 RCL 34 641 / 642 - 643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 646 "COMB. EFF. = " 696 RDV 647 RCR 648 RCX 649 "%" 699 RCR	637 *		
640 1000 690 RCL 34 641 / 691 * 642 - 692 RCX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR	638 -		
641 / 691 * 642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = "696 ADY 647 ACA 697 RTN 648 ACX 698+LBL 02 649 "%" 699 ACA	639 RCL 24		
642 - 692 ACX 643 1 E2 693 STO IND 00 644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = 696 ADY 647 ACA 697 RTN 648 ACX 698+LBL 02 649 "%" 699 ACA	640 1000		
643 1 E2 693 STO IND 00 644 * 694 ISC 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = 696 RDV 647 RCR 697 RTN 648 RCX 698+LBL 02 649 "%" 699 RCR	641 /		
644 * 694 ISG 00 645 FIX 2 695+LBL 00 646 "COMB. EFF. = "696 RDY 647 ACR 697 RTN 648 ACX 698+LBL 02 649 "%" 699 ACR	642 -		
645 FIX 2 695+LBL 00 646 "COMB. EFF. = " 696 ADY 647 ACA 697 RTH 648 ACX 698+LBL 02 649 "%" 699 ACA	643 1 E2		
646 -COMB. EFF. = - 696 ADV 647 ACA 697 RTN 648 ACX 698+LBL 02 649 -%- 699 ACA	644 *		
647 ACA 697 RTN 648 ACX 698+LBL 02 649 *% 699 ACA			
648 ACX 698+LBL 02 649 -%- 699 ACA	646 -COMB. EFF. = -		
649 -%- 699 RCR	647 ACA		
477	648 ACX		
650 ACA 700 ACX	649 ***		
	650 ACA	700 ACX	

Al.7 Example of print-out from program AIRAP

Using h = 0.008843	Option 1 combined with Option 2	Option 3
	0.09 -1.30-04 0.14 -4.50-04 0.28	K = 0.971317 Z = 97.220045
0.09 -1.30-04 0.14 -4.50-04 0.28	9.5 19.0 0.008820 0.00607 0.95	X/m = 48.436237
9.5 19.0 0.008843 0.00607 0.95	30 75 29.92	
500.0 2.00 20.0 9.0 225.0	500.0 2.00 20.0 9.0 225.0 FUEL = 1000.0	
EI CO = 47.65 CO2 = 3076.41 NOX = 3.37 CXHY, CHY/X 11.11 CXHY, CH4 = 12.71 CO NET = 483.3 CO2 NET = 1.986 NOX NET = 20.8	EI C0 = 47.65 C02 = 3076.41 NOX = 3.37 CXHY, CHY/X 11.11 CXHY, CH4 = 12.70 C0 MET = 483.4 C02 MET = 1.986 NOX MET = 20.8	
CXHY WET = 225.0 % OXYGEN, WET = 17.57 NOX AT 3% 02 = 111 WATER = 2.87% F/A = 0.009998 COMB. EFF. = 97.78%	CXHY WET = 225.0 7 OXYGEN, WET = 17.57 NOX AT 3% 02 = 111 WATER = 2.87% F/A = 0.009998 COMB. EFF. = 97.78%	
	POUNDS PER HOUR CO = 47.65 CO2 = 3076.41 NO2 = 3.37 CHY/X = 11.11 CH4 = 12.79 SO2 = 0.40	

Example of print-out from program AIRAP (concluded)

Content of the storage registers 00 to 44 after running program AIRAP using Options 1 and 2

R89=	26.000000	R12= -	0.009130	R23=	3.368495	R34=	1.015500
R01=	1.006070	R13=	0.140000	R24=	11.108414	R35=	0.000498
R92=	97.959900	R14= -	9.999459	R25=	12.784947	R36=	9.020447
R03=	0.008820	R15=	0.280000	R26=	0.175696	R37=	75.000000
R94=	14.927999	R16=	0.999225	R27=	1,989.999998	R38=	29.928888
R05=	0.020569	R17=	1.020945	R28=	0.000483	R39=	0.009320
R06=	2.000000	R18=	0.971317	R29=	0.019861	R49=	0.000000
R97=	9.500000	R19=	97.220045	R30=	0.000020	R41=	0.000500
R98=	19.000000	R20=	48.436237	R31=	0.999921	R42=	0.020000
R89=	2.908829	R21=	47.654944	R32=	0.020000	R43=	0.009020
R19=	-0.008500	R22=	3,076.411496	R33=	0.028683	R44=	0.000009
R11=	0.090000						

Al.8 Reference

Al. Aerospace Information Report, AIR 1533, "Procedure for the Calculation of Basic Emission Parameters for Aircraft Engines," Society of Automotive Engineers Inc., 400 Commonwealth Drive, Warrendale, PA 15096, April 30, 1982.

A2. PROGRAM AIRA (HP-41C/41CV/41CX)

A2.1 Description of Program AIRA

Program AIRA makes the same calculations as program AIRAP. Program AIRAP needs a printer, program AIRA does not.

A2.2 Definitions

Program AIRA uses the same definitions as program AIRAP.

A2.3 Calculation of Emission Indexes

Program AIRA uses the same formulas as program AIRAP.

A2.4 Description of Labels Used in Program AIRA

Program AIRA does not use Label D. Otherwise, the use of the labels is the same as in Program AIRAP.

A2.5 Instructions for Using Program AIRA

KEYSTROKES DISPLAY

REMARKS

MINIMUM SIZE 045

XEQ AIRA	KEY A OR B	Follow the instructions for AIRAP. Use option I (page AI-13) and enter relative humidity, temperature and barometric pressure. After entering the concentrations of the constituents, use option 2 (page AI-14) and a fuel flow rate of 1000 pounds per hour.
1000	1000	Key in R/S to continue.
R/S	EI CO =	Key in R/S to continue.
R/S	47.65	The display shows the emission index for carbon monoxide. Key in R/S to continue.
R/S	EI CO2 =	Key in R/S to continue.
R/S	3076.41	The display shows the emission index for carbon dioxide. Key in R/S to continue.
R/S	EI NOX =	Key in R/S to continue.
R/S	3.37	The display shows the emission index for the oxides of nitrogen as nitrogen dioxide. Key in R/S to continue.
R/S	EI CHY/X =	Key in R/S to continue.
R/S	11.11	The display shows the emission index for hydrocarbons as $\text{CH}_{y/x}$. Key in R/S to continue.
R/S	EI CH4 =	Key in R/S to continue.
R/S	12.70	The display shows the emission index for hydrocarbons as methane. Key in R/S to continue.
R/S	CO WET =	Key in R/S to continue.
R/S	483.4	The display shows the concentration of carbon monoxide (ppm, wet). Key in R/S to continue.
R/S	CO2 WET =	Key in R/S to continue.

Instructions for Using Program AIRA (continued)

KEYSTROKES	DISPLAY	REMARKS
R/S	1.986	The display shows concentration of carbon dioxide (%, wet). Key in R/S to continue.
R/S	NOX WET =	Key in R/S to continue.
R/S	20.8	The display shows the concentration of the oxides of nitrogen (ppm, wet). Key in R/S to continue.
R/S	CXHY WET =	Key in R/S to continue.
R/S	225.0	The display shows the concentration of hydrocarbons (ppm, wet). Key in R/S to continue.
R/S	% OXYGEN WET =	Key in R/S to continue.
R/S	17.57	The display shows the concentration of oxygen (% wet). Key in R/S to continue.
R/S	NOX AT 3% 02=	Key in R/S to continue.
R/S	110.5	The display shows the concentration of the oxides of nitrogen (ppm, wet) at a concentration of 3% oxygen. Key in R/S to continue.
R/S	% WATER =	Key in R/S to continue.
R/S	2.87	The display shows the concentration of water (%). Key in R/S to continue.
R/S	F/A =	Key in R/S to continue.
R/S	0.009998	The display shows the fuel to air ratio. Key in R/S to continue.
R/S	COMB. EFF.	Key in R/S to continue.
R/S	97.78	The display shows the combustion efficiency (%). Key in R/S to continue.
R/S	LBS CO =	Key in R/S to continue.
R/S	47.65	The display shows the pounds of carbon monoxide per hour. Key in R/S to continue.
R/S	LBS CO2 =	Key in R/S to continue.

Instructions for Using Program AIRA (concluded)

KEYSTROKES	DISPLAY	REMARKS
R/S	3076.41	The display shows the pounds of carbon di- oxide per hour. Key in R/S to continue.
R/S	LBS NOX =	Key in R/S to continue.
R/S	3.37	The display shows the pounds of oxides of nitrogen (as nitrogen dioxide) per hour. Key in R/S to continue.
R/S	LBS CHY/X =	Key in R/S to continue.
R/S	11.11	The display shows the pounds of hydrocarbons per hour (as $\mathrm{CH}_{y/x}$). Key in R/S to continue.
R/S	LBS CH4 =	Key in R/S to continue.
R/S	12.70	The display shows the pounds of hydrocarbons per hour (as methane). Key in R/S to continue.
R/S	LBS SO2 =	Key in R/S to continue.
R/S	0.40	The display shows the pounds of sulfur di- oxide per hour. Key in R/S to continue.
R/S	co?	Execution of the program returns to label E.
		Option 3
G	co?	The display shows successively the values of K, Z, and X/m . Execution of the program returns to label E.

A2.6 Program Listing for AIRA

01+LBL -AIRA-	52 STO 00	103 "8?"	154 "CXHY?"
02 "KEY A OR B"	53 "HUMIDITY?"	104 PROMPT	155 PROMFT
03 PROMPT	54 PROMPT	1 05 STO 38	156 1 E6
94+LBL A	55+LBL 16	106 X<>Y	157 /
95 SF 93	56 STO 93	197 -	158 STO 25
06 GTO 20	57 ST+ 89	108 /	159 STO 16
97 +LBL B	58 -	109 RCL 60	160 .
98 CF 93	59 STO 10	118 X<>Y	161 *FUEL?*
89+L8L 28	68 RCL 99	111 GTO 16	162 PROMPT
19 FIX 4	61 2	112+LBL E	163 STO 27
11 1.00607	62 X=Y?	113 FIX 1	164 XEQ 18
12 STO 01	63 GTO "RH"	114 "CO?"	165 XEQ 05
13 97.95	64 GTO E	115 PROMPT	166 XEQ 10
14 STO 02	65+LBL "RH"	116 1 E6	167 RCL 41
1507	66 "RH?"	117 /	168 STO 21
16 STO 11	67 PROMPT	118 STO 21	169 RCL 42
1700013	68 STO 36	119 STO 41	170 STO 22
18 STO 12	69 • 72 •	120 "CO2?"	171 RCL 43
19.14	70 PROMPT	121 PROMPT	172 STO 23
20 STO 13	71 STO 37	122 FIX 2	173 RCL 44
2100845	72 50	123 1 E2	174 STO 24
22 STO 14	73 RCL 37	124 /	175 XEQ 95
23.28	74 X(=Y?	125 STO 22	176 XEQ 10
24 STO 15	75 GTO 17	126 STO 42	177 GTO 06
25 .02	76 75	127 "HOX?"	178+LBL 19
26 STO 32	77 X()Y	128 PROMPT	179+LBL *K*
27 .00032	78 X<=Y?	129 FIX 1	180 RCL 21
28 STO 39	79 GTO 18	130 1 E6	181 RCL 01
29 GTO 11	80 .031767	131 /	182 *
30+LBL F	81 *	132 570 23	183 \$10 35
31 CLE	82 EtX	133 STO 43	184 LASTX
32 GTO C	83 .080455	134 .	185 RCL 22
33+LBL 11	84 GTO 19 85+LBL 17	135 "NO?" 136 PROMPT	186 *
34 "SET 11-15"	86 .938251	137 X=9?	187 570 36
35 PROMPT	87 *	138 GTO 03	188 FS? 83 189 GTO 21
36+LBL C	88 E†X	139 GTO 94	199 RCL 23
37 FIX 1	89 .953226	140+LBL 03	•
38 "M?"	90 GTO 19	141 RCL 23	191 RCL 81
39 PROMPT	91+L8L 18	142 1 E6	192 * 193 STO 37
40 STO 07	92 .935264	143 *	194 LASTX
41 "N?"	93 *	144 RCL 92	195 RCL 24
42 PROMPT 43 STO 08	94 EtX	145 INT	196 *
44 X()Y	95 .861928	146 1 E2	197 STO 38
45 /	96+LBL 19	147 /	198 -
46 STO 96	97 *	148 *	199 STO 48
47 2	98 RCL 36	149+LBL 94	280+LBL 21
48 STO 09	99 1 E2	150 1 E6	201 RCL 35
49 /	199 /	151 /	202 RCL 36
50 RCL 39	191 *	152 STO 24	203 +
51 *	102 ENTERT	153 STO 44	204 RCL 06

Program Listing for AIRA (continued)

295 2	256 *	307 /	358 RCL 05
206 /	257 STO 29	308 -	359 *
297 *	258 FS? 03	389 4	360 RCL 34
208 1	259 GTO "Z"	310 *	361 /
209 +	260 RCL 37	311 /	362 RCL 16
219 STO 17	261 LASTX	312 STO 20	363 RCL 08
211 1	262 *	313 RCL 39	364 *
212 FC? 93	263 STO 38	314 *	365 RCL 97
213 GTO 12	264 RCL 38	315 1	366 /
214 RCL 23	265 LASTX	316 +	367 2
215 STO 30	266 *	317 STO 34	368 /
216 RCL 24	267 STO 31	318+LBL 22	369 -
217 STO 31	268+LBL "Z"	319 RCL 28	370 STO 33
218 -	269 2	320 .2098	371 RTH
219 +	270 RCL 28	321 *	372+LBL 05
229+LBL 12	271 -	322 RCL 06	373 RCL 26
221 RCL 25	272 2	323 4	374 RCL 91
222 2	273 RCL 07	324 /	375 /
223 *	274 /	325 -	376 RCL 18
224 RCL €7	275 RCL 98	326 RCL 05	377 /
225 /	276 RCL 97	327 *	378 RCL 11
226 -	277 /	328 RCL 34	379 *
227 RCL 10	278 2	329 /	380 t
228 *	279 /	330 RCL 28	381 +
229 RCL 09	289 -	331 2	382 ST* 22
230 +	281 RCL 25	332 / 333 -	383 RCL 22
231 STO 00	282 *	334 RCL 29	384 RCL 12
232 RCL 17	283 -	335 -	385 *
233 RCL 09	284 RCL 38	336 RCL 96	386 RCL 14 387 RCL 01
234 *	285 RCL 31	337 4	388 1
235 RCL 10	286 - 287 +	338 /	389 -
236 1	288 RCL 28	339 RCL 25	390 *
237 RCL 35 238 -	289 RCL 29	340 *	391 +
239 FS? 03	290 RCL 25	341 +	392 ST+ 21
249 GTO 13	291 +	342 RCL 38	393 RCL 22
241 RCL 48	292 +	343 RCL 31	394 RCL 13
242 +	293 STO 95	344 -	395 *
243+LBL 13	294 /	345 -	396 RCL 15
244 *	295 STO 19	346 RCL 31	397 FS? 03
245 -	296 2	347 2	398 GTC 87
246 RCL 99	297 *	348 /	399 GTO 08
247 X()Y	298 RCL 96	349 -	400+LBL 07
248 /	299 -	350 STO 26	401 RCL 33
249 STO 18	300 1	351 RCL 03	402 GTO 89
250 RCL 35	301 RCL 03	352 RCL 28	403+LBL 08
251 X<>Y	302 +	353 *	484 RCL 81
252 *	303 RCL 19	354 RCL 06	495 1
253 STO 28	304 RCL 39	355 2	486 -
254 RCL 36	395 *	356 /	407+LBL 09
255 LASTX	306 2	357 +	408 *

Program Listing for AIRA (concluded)

409 +	469 12911	511 20.948	562 RCL 27
418 1	461 RCL 06	512 -	563 X=8?
411 +	462 1998	513 CHS	564 GTO E
412 ST* 23	463 *	514 17.948	565 FIX 2
413 ST* 24	464 +	515 X<>Y	566 1 E3
414 RTN	465 RCL 25	516 /	567 /
415+LBL G	466 STO 16	517 RCL Y	568 STO Y
416 FIX 6	467 XEQ 81	518 *	569 "LBS CO ="
417 "K ="	468 "EI CH4 ="	519 FIX 1	570 XEQ 26
418 RCL 18	469 RCL 25	520 "NOX AT 3% 02 ="	571 *LBS CO2 =*
419 PROMPT	470 16043	521 PROHPT	572 XEQ 26
428 STOP	471 XEQ 01	522 STOP	573 "LBS NOX ="
421 °Z =°	472 "CO WET ="	523 RCL 33	574 XEQ 26
422 RCL 19	473 RCL 28	524 1 E2	575 "LBS CHY/X ="
423 PROMPT	474 1 E6	525 *	576 XEQ 26
424 STOP	475 *	526 FIX 2	577 *LBS CH4 =*
425 RCL 28	476 FIX 1	527 "% WATER ="	578 XEQ 26
426 "X/H ="	477 PROMPT	528 PROMPT	579 RCL 27
427 PROMPT	478 STOP	529 STOP	580 RCL 32
428 STOP	479 "CO2 HET ="	539 FIX 6	581 .92
429 GTO E	480 RCL 29	531 *F/A = *	582 *
430+LBL 06	481 1 E2	532 1	583 *
431 RCL 06	482 *	533 ENTERT	584 *LBS S02 =*
432 1.998	483 FIX 3	534 RCL 20	585 PROMPT
433 *	484 PROMPT	535 /	586 STOP
434 12.011	485 STOP	536 RCL 04	587 FIX 2
435 +	486 "HOX HET ="	537 *	588 GTO E
436 STO 84	487 RCL 31	538 28.965	589+LBL 01
437 RCL 30	488 1 E6	539 /	598 *
438 RCL 31	489 *	540 PROMPT	591 RCL 84
439 -	490 FIX 1	541 STOP	592 /
449 RCL 92	491 PROMPT	542 1	593 RCL 05
441 FRC	492 STOP	543 ENTERT	594 /
442 /	493 "CXHY WET ="	544 RCL 21	595 RCL 34
443 ST+ 31	494 RCL 16	545 18730	596 *
444 21	495 1 E6	546 /	597 PROMPT
445 STO 99	496 *	547 4.346	598 STOP
446 FIX 2	497 PROMPT	548 *	599 STO IND 80
447 *EI CO =*	498 STOP	549 -	600 ISG 00
448 RCL 28	499 *% OXYGEN, HET =*	550 RCL 24	601+LBL 00
449 28011	500 FIX 2	551 1000	602 RTN
450 XEQ 81	501 RCL 26	552 /	603+LBL 26
451 "EI CO2 ="	502 1 E2	553 -	684 RCL IND 89
452 RCL 29	503 *	554 1 E2	605 *
453 44009.8	504 PROMPT	555 *	686 PROMPT
454 XEQ 01	505 STOP	556 FIX 2	607 STOP
455 *EI HOX =*	596 RCL 31	557 *COMB. EFF. = *	608 X<>Y
456 RCL 31	507 1 E6	558 PROMPT	609 STO Y
457 46005.5	508 *	559 STOP	610 ISG 00
458 XEQ 01	509 FIX 1	569 21	611+LBL 89
459 "EI CHY/X ="	510 RCL Y	561 STO 00	612 RTN
7J7 E1 UNI/A -	JIS KUL I	JUL 310 00	613 .END.
			OIO ICHDI

A3. PROGRAM AIRB (HP-41C/41CV/41CX)

A3.1 Description of Program AIRB

Program AIRB calculates the emission indexes of carbon monoxide, carbon dioxide, oxides of nitrogen and hydrocarbons as mass units per 1000 mass units of fuel, for example, as pounds per 1000 pounds (or grams per kilogram) of fuel. This program makes no adjustments for the basis of measurement (wet, dry or semi-dry), the humidity, or the instrument interference coefficients. This program is much simpler than programs AIRAP and AIRA, makes fewer calculations and runs much faster. Manual entry of the program into the calculator memory is feasible. The best use of this program is for making quick estimates of emission indexes. Program AIRB does not require a printer.

A3.2 Definitions

Program AIRB uses the same definitions as Program AIRAP.

A3.3 Calculation of Emission Indexes

Program AIRB requires inputs of the concentrations of carbon monoxide, carbon dioxide, oxides of nitrogen and hydrocarbons. It does not require an input of the concentration of nitric oxide. The input uses the concentrations of the constituents as parts per million or as percent. The program converts each concentration to the mole fraction concentration. Program AIRB calculates the emission indexes using the equation

$$EI_{z} = \left(\frac{[z]}{[CO] + [CO_{2}] + [C_{x}H_{y}] - T}\right) \left(\frac{10^{3} M_{z}}{M_{C} + \alpha M_{H}}\right)$$

A3.4 Description of Labels Used in Program AIRB

LABEL USE

- A Initiates the input of data and sets the atomic hydrogen-tocarbon ratio at 2 to simulate JP-4 fuel.
- B Initiates the input of data and sets the atomic hydrogen-to-carbon ratio at 1.8 to simulate JP-5 fuel.
- C Initiates the input of data and sets the atomic hydrogen-tocarbon ratio at number specified by the user.
- J Initiates the input of data for a calculation which uses the atomic hydrogen-to-carbon ratio of the preceding calculation.

A3.5 Instructions for Using Program AIRB

KEYSTROKES DISPLAY

REMARKS

MINIMUM SIZE 007

XEQ AIRB	ENTER DATA	This command starts the program at Label A which makes calculations using a hydrogen-to-carbon ratio of 2 (JP-4). For other hydrogen-to-carbon ratios key in label B or label C. Label B sets the hydrogen-to-carbon ratio at 1.8 (JP-5). Label C uses a ratio specified by the user. If you wish to use either label B or C, key in now. This example uses the same emissions data as program AIRAP/AIRA (i.e., carbon monoxide, 500 ppm, carbon dioxide 2.00%, oxides of nitrogen 20 ppm and hydrocarbons 225 ppm) with adjustments for instrument interferences, converter efficiency and basis of measurement. The adjusted data entries are 483.3 ppm, 1.986%, 20.8 ppm, and 225 ppm. Key in the concentration of carbon monoxide as ppm.
483.3	483.3	Key in R/S to continue.
P/S	4.83 -04	The display shows the mole fraction concentration of carbon monoxide. Key in the concentration of carbon dioxide as %.
1.986	1.986	Key in R/S to continue.
R/S	.02	The display shows the mole fraction concentration of carbon dioxide. Key in the concentration of the oxides of nitrogen as ppm.
20.8	20.8	Key in R/S to continue.
R/S	2.08 -05	The display shows the mole fraction concentration of the oxides of nitrogen. Key in the concentration of hydrocarbons as ppm.
225	225	Key in R/S to continue.
R/S	EI CO =	Key in P/S to continue.
R/S	47.66	The display shows the emission index for carbon monoxide. Key in R/S to continue.

Instructions for Using Program AIRB (concluded)

KEYSTROKES	DISPLAY	REMARKS
R/S	EI CO2 =	Key in R/S to continue.
R/S	3077.34	The display shows the emission index for carbon dioxide. Key in R/S to continue.
R/S	EI NOX =	Key in R/S to continue.
R/S	3.37	The display shows the emission index for the oxides of nitrogen (calculated as nitrogen dioxide). Key in R/S to continue.
R/S	EI CXHY =	Key in R/S to continue.
R/S	12.71	The display shows the emission index for hydrocarbons (calculated as methane). Key in R/S to continue.
R/S Key A,	в, C or J	Labels A or B restart the program using hydrogen-to-carbon ratios of 2 or 1.8. Label C restarts the program using the hydrogen-to-carbon ratio selected by the user. Label J repeats the program using the hydrogen to carbon ratio of the previous calculation.

A or B	ENTER DATA	Repeat preceding steps.
С	H/C RATIO ?	Key in any hydrogen to carbon ratio.
1.83	1.83	Key in R/S to continue.
R/S	ENTER DATA	Key in the concentration of carbon monox- ide and continue using the procedure al- ready described.
J	ENTER DATA	Key in the concentration of carbon monox- ide and continue using the procedure already described.

A3.6 Program Listing for AIRB

91+LBL "AIRB"	46 +
82+LBL A	47 +
93 14.927	48 RCL 05
94 GTO 91	49 *
85+LBL 8	50 STO 06
96 13.825	51 28010
97 GTO 91	52 XEQ 02
08+LBL C	53 44809.8
99 "H/C RATIO"	54 XEQ 02
10 PROMPT	55 46005.5
11 1.003	56 XEQ 92
12 *	57 16043
13 12.911	58+LBL 92
14 +	59 RCL IND 00
15 GTO 91	60 *
16+LBL J	61 RCL 96
17 RCL 05	62 /
18+LBL 91	63 STO IHD 90
19 FIX 2	64 ISG 00
29 STO 95	65+LBL 00
21 1	66 4
22 STO 99	67 RCL 00
23 -ENTER DATA-	68 X<=Y?
24 PROMPT	69 RTN
25 1 E6	70 *EI CO =*
26 /	71 PROMPT .
27 STO 01	72 RCL 01
28 STOP	73 STOP
29 1 E2	74 "EI CO2"
30 /	75 PROMPT 76 RCL 82
31 STO 02	76 KGL 62 77 STOP
32 .00032	77 STOP 78 "EI NOX ="
33 -	78 EL NUA - 79 PROMPT
34 STOP	89 RCL 93
35 1 E6	81 STOP
36 /	82 "EI CXHY ="
37 STO 93	83 PROMPT
38 STOP	84 RCL 94
39 1 E6	85 STOP
49 /	86 TA, B, C OR J
41 STO 84	87 PROMPT
42 X<>Y	88 RTN
43 RCL 81	89 END
44 X<>Y	U/ CHD

45 RDH

A4. PROGRAM AIRNP (HP-41C/41CV/41CX)

A4.1 Description of Program AIRNP

Program AIRNP uses inputs of either (a) time of operation, thrust and fuel flow rate or (b) time of operation, fuel flow rate and emission index to calculate:

- (1) the amount of fuel used, and the amount of a constituent z produced, by the operation of a gas turbine engine at any power setting for a specified time;
- (2) the total amount of the constituent z produced by a group of power settings, such as those used in the testing of an engine;
- (3) the fuel used by the group of power settings; and
- (4) the amount of the constituent z produced for each pound of fuel used by the group of power settings.

This program uses a printer.

A4.2 Definitions

- W_z = the pounds (kilograms) of a constituent z produced by operation at a power setting for a specified time
- EIz = the emission index of the constituent z in the engine exhaust in units of mass per 1000 units of mass of the fuel, i.e., pounds (kilograms) per 1000 pounds (kilograms) of fuel used
- F = the amount of fuel used at the power setting in pounds (kilograms) per hour
- hr = the time in hours at the engine power setting
- z = a constituent of the engine exhaust, e.g., carbon monoxide, carbon dioxide, oxides of nitrogen or hydrocarbons

A4.3 Calculations

The emission index, the fuel flow rate and the length of time at an engine power setting determine the amount of a constituent in the engine exhaust. For any power setting,

$$W_z = EI_z \times F/1000 \times hr.$$

The addition of the amounts of the constituent from each power setting gives the total amount of the constituent produced by the operation of the engine at a group of power settings.

The calculations need an emission index for each power setting for each constituent. The emission indexes may be determined from (a) measured concentrations of the constituents, or (b) a plot of known emission indexes vs. thrusts. The plotting method allows the calculation of an emission index at a power setting for which there was no measurement of the concentration of the constituent.

The plotting method uses a group of emission indexes (calculated from the measured concentrations of the constituent in the exhaust) and the corresponding values of thrusts. To demonstrate this method, program AIRNP uses the following data*.

Power	Thrust	Emission
setting	pounds	index
15%	1597	3.95
20%	2069	4.56
26%	2728	5.15
3 7%	3845	6.42
46%	4883	8.37
63%	6662	11.78
76%	8031	14.80
Maximum cont.	9201	18.71
94%	9957	21.38
IRP	10548	25.16

Analysis of these data, using the program CFIT from the Hewlett-Packard Advantage Pac showed that they best fit the exponential equation

$$y = ae^{bx}$$
,

where y = emission index and x = thrust in pounds.

The print-out from program CFIT using these data appears in Paragraph A4.7.

To use this equation, the program must contain the constants 'a' and 'b'. Label C of program AIRNP contains these constants as steps 44 and 42. The program reserves labels A and B for user-determined constants for other engines and constituents. Labels A and B appear in the program listing with a space in place of the engine type indicator and by 'a' and 'b' in place of the constants. The user may wish to add other local labels such as D, E, G, I, a, d, and e for other engines and constituents.

^{*} A. F. Klarman and J. J. Zidzik, "F404-GE-400 Engine Exhaust Emission Test Results, Interim Report," Naval Air Propulsion Center, NAPC-LR-81-10, 30 November 1981.

To improve the fit of the data, the curve fitting procedure omits values of thrusts and emission indexes for the power settings of idle (EI = 1.16) and afterburner (EI = 9.22). These power settings use emission indexes determined by measurement of concentrations.

A4.4 Description of Labels Used in Program AIRNP

LABEL USE

- A Reserved for engine type and constants as specified by the user.
- B Reserved for engine type and constants as specified by the user.
- C Uses inputs of either (a) time, thrust and fuel flow rate, or (b) time, fuel flow rate and emission index to calculate the emissions from an engine. The demonstration in Paragraph A4.5 uses program steps which define the constants and print-out as emissions of the oxides of nitrogen from an F404-GE-400 engine.
- E Uses inputs of times, fuel flow rates and emission indexes to calculate emissions of any constituent. The print-out describes the constituent as 'z'.
- F May be used instead of 'XEQ AIRNP' to start the program, when the program is positioned in the main memory of the calculator.
- J After entry of data for any number of power settings, use label J to print-out the total amount of the constituent produced and the fuel used by these power settings. Label J also prints-out the amount of the constituent formed for each pound of fuel used.
- H cancels the last entry.
- Sets the print-out of the constituent at 'CO'.
- b Sets the print-out of the constituent at 'CXHY'.

A4.5 Instructions for Using Program AIRNP

KEYSTROKES

DISPLAY

REMARKS

MINIMUM SIZE 010

XEQ AIRNP KEY A/B/C/E

When using label C, the print-out always records 'NOX' unless changed by executing labels a or b at this time. Label a changes the print-out to 'CO', label b to 'CXHY'. Label C contains programmed entries for an F404 engine and constants for the plot (as an exponential equation) of the emission indexes of the oxides of nitrogen vs. thrust. See Paragraph A4.3 for details. Labels A and B contain dummy entries. The user can change data in labels A, B or C, add other local labels such as D, G, I, c, d or e, or number labels from 09 to 99. These labels use the same arrangement of program steps labels A, B or C.

The example in this demonstration uses a simulated engine test for an F404 engine with run times, thrusts, fuel flow rates and emission indexes, at power settings as follows:

	Minutes	Thrust	F	ΕI
Idle	5	•	996	1.16
89% rpm	5	5945	4850	_
IRP	10	10190	8514	-
Afterburner	- 3	-	29750	9.22

Key in C.

c	MINUTES?	The print-out shows that the emission calculations are for an F404 engine for the oxides of nitrogen. Key in the time of operation at idle.
5	5	Key in R/S to continue.
R/S	THRUST?	The data at this power setting does not include thrust. Key in R/S to skip to the input of fuel flow rate.
R/S	FUEL?	Key in the fuel flow rate.
996	996	Key in R/S to continue.

Instructions for Using Program AIRNP (continued)

KEYSTROKES	DISPLAY	REMARKS
R/S	EI?	The print-out shows the time of operation and fuel flow rate at idle. Key in the emission index.
1.16	1.16	Key in R/S to continue.
R/S	MINUTES?	The print-out continues with the emission index, the fuel used and the pounds of oxides of nitrogen (as nitrogen dioxide) formed. Key in the time at the next power setting (89% rpm).
5	5	Key in R/S to continue.
R/S	THRUST?	Key in thrust.
5945	5945	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
4850	4850	Key in R/S to continue.
R/S	MINUTES?	The first line of the print-out shows the time of operation, thrust and fuel flow rate at 89% rpm. The second line shows the emission index (as calculated from the plot of thrust vs. emission indexes), the fuel used, and the pounds of oxides of nitrogen produced. Key in the time at the next power setting (IRP).
10	10	Key in R/S to continue.
R/S	THRUST?	Key in thrust.
10190	10190	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
8514	8514	Key in R/S to continue.
R/S	MINUTES?	The print-out shows input-output data as previously described. Key in the time at the next power setting (afterburner).
3	3	Key in R/S to continue.

Instructions for Using Program AIRNP (continued)

KEYSTROKES	DISPLAY	REMARKS		
R/S	THRUST?	Key in R/S to use the emission index, in- stead of the thrust, for this calculation.		
R/S	FUEL?	Key in the fuel flow rate.		
29750	29750	Key in R/S to continue.		
R/S	EI?	Key in the emission index.		
9.22	9.22	Key in R/S to continue.		
R/S	MINUTES?	The print-out shows input-output data as previously described. There are no other power settings in this example. Key in J to continue.		
J	KEY A/B/C/E	The print-out shows the pounds of oxides of nitrogen produced by the sequence of power settings (50.60), the pounds of fuel used in the test (3394), and the pounds of the oxides of nitrogen produced for each pound of fuel used (0.01491). Key in E.		
E	MINUTES?	The program is ready to start a new calcu- ation. Label E makes calculations using time of operation, fuel flow rate and emission index. Label E does not print a header. Use for any constituent. Use the data of the preceding example and emission indexes of 9.85 for 89% rpm and 23.12 for IRP. Key in the time of operation at idle.		
5	5	Key in R/S to continue.		
R/S	FUEL?	Key in the fuel flow rate.		
996	996	Key in R/S to continue.		
R/S	EI?	The print-out shows the time of operation and fuel flow rate at idle. Key in the emission index.		
1.16	1.16	Key in R/S to continue.		
R/S	MINUTES?	The print-out continues with the emission index, the fuel used and the pounds of the constituent z formed. Key in the time at the next power setting (89% rpm).		

Instructions for Using Program AIRNP (continued)

KEYSTROKES	DISPLAY	REMARKS
5	5	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
4850	4850	Key in R/S to continue.
R/S	EI?	The print-out shows the time of operation and the fuel flow rate at 89% rpm. Key in the emission index.
9.85	9.85	Key in R/S to continue.
R/S	MINUTES?	The print-out continues with the emission index, the fuel used and the pounds of the constituent z formed. Key in the time at the next power setting (IRP).
10	10	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
8514	8514	Key in R/S to continue.
R/S	EI?	Key in the emission index for IRP.
23.12	23.12	Key in R/S to continue.
R/S	MINUTES?	The print-out shows input-output data as previously described. Key in the time at the next power setting (afterburner), making an intentional error.
35	35	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
29750	29750	Key in R/S to continue.
R/S	EI?	Key in the emission index.
9.22	9.22	Key in R/S to continue.
R/S	MINUTES?	The print-out shows input-output data as previously described. These data can be corrected after the print-out and before the next entry of time of operation. Key in H.

Instructions for Using Program AIRNP (concluded)

KEYSTROKES	DISPLAY	REMARKS		
ħ	MINUTES?	The print-out notes that the preceding entry has been deleted. Continue with the correct entries for this power setting. Key in 3.		
3	3	Key in R/S to continue.		
R/S	FUEL?	Key in the fuel flow rate at afterburner.		
29750	29750	Key in R/S to continue.		
R/S	EI?	Key in the emission index for afterburner.		
9.22	9.22	Key in R/S to continue.		
R/S	MINUTES?	The print-out shows the corrected calculation. There are no other power settings in this example. Key in J to continue.		
J	KEY A/B/C/E	The print-out shows the pounds of the constituent z produced by the sequence of power settings (50.60), the pounds of fuel used in the test (3394), and the pounds of the constituent z produced for each pound of fuel used (0.01491). The program is ready to start a new calculation.		

A4.6 Program Listing for AIRNP

91+LBL "AIRNP"	51 STO 95	101 "EI?"	151 ACA
02+LBL F	52+LBL 92	102 PROMPT	152 CLA
03 -NOX-	53 .	183 XC>Y	153 */LBS OF FUEL*
04 ASTO 0 6	54 STO 00	104+LBL 03	154 ACA
95 -CO-	55 STO 01	1 9 5 X<>Y	155 PRBUF
06 ASTO 07	56 FS? 01	106 FIX 2	156 *USED IN TEST =*
07 "CXHY"	57 GTO 03	107 ACX	157 ACA
	58 ACA	108 RCL 94	158 FIX 5
89 °Z"	59 • •	109 60	159 /
10 ASTO 89		119 /	160 ACX
	61 ARCL IND 05	111 STO Z	161 ADV
	62 ACA	112 RCL T	162 ADY
13 CF ^:	63 ADY	113 *	163 GTO F
14 CF 😅	64+LBL 03	114 FIX 1	164+LBL H
15 GTO 01	65 ADV	115 ACX	165 ST- 01
16 +LBL a	66 "MINUTES?"	116 ST+ 00	166 RDN
17-7	67 CF 29	117 STO Z	167 ST- 00
18 STO 05	68 FIX 1	118 FIX 2	168 94
19 GTO 01	69 PROMPT	119 X<>Y	169 ACCHR
29◆LBL b	79 STO 94	120 FIX 2	179 • •
21 8	71 ACX	121 1 E3	171 ACA
22 STO 95	72 FS? 01	122 /	172 "ENTRY DELETED"
23+LBL 01 .	73 GTO 05	123 *	173 FIX 0
24 CLA	74 .	123 * 124 ACX	174 RCA
25 "KEY A/B/C/E"	75 "THRUST?"	ICO ANA	175 ADV
26 PROMPT	76 PROMPT	126 FIX 1	176 GTO 83
27+LBL A	77 X=0?	127 ST+ 01	177 END
28 -p-	78 GTO 05	128 GTO 03	
29 STO 83	79 ACX	129+LBL J	
30 °a"	80 RCL 03	130 ADY	
31 STO 02	81 *	131 *LBS *	
	82 EtX	132 ARCL IND 05	
33 GTO 92	83 RCL 02	133 ACA	
34+LBL 3	84 *	134 CLR	
35 - 6-	85 GTO 06	135 */TEST =*	
36 STO 03	86+LBL 95	136 ACA	
37 °a°	87 SF 02	137 RCL 01	
38 STO 02	88 • •	138 FIX 2	
39	89 ACA	139 ACX	
40 GTO 02	90+LBL 06	140 ADY	
41+LBL C	91 "FUEL?"	141 ADV	
42 .00020093	92 PROMPT	142 "LBS FUEL/TEST ="	
43 STO 93	93 ACX	143 ACA	
44 2.98393	94 PRBUF	144 FIX 0	
45 STO 22	95 FS?C 82	145 RCL 00	
46 "F494"	96 GTO 87	146 ACX	
47 GTO 92	97 FO? 01	147 ADY	
48+LBL E	98 GTO 07	148 ADY	
49 SF 01	99 GTO 08	149 "LBS "	
50 9	100+LBL 07	150 ARC! IND 05	

A4.7 Example of Print-out from Program AIRNP

LABEL C	LABEL CFIT		
F484 NOX			
5,0 996.0	XROM -CFIT-		
1.16 83.0 0.10	Σ+ CLΣ FIT		
5.0 5945.0 4850.0	3.95 ENTER+		
9.85 404.2 3.98	1597.00 XEQ A		
	Σ+ CLΣ FIT		
10.0 10190.0 8514.0	4.56 ENTER† 2069.00 XEQ A		
23.12 1419.0 32.81	Σ+ CLΣ FIT		
7.0 20750.0	5.15 ENTERT		
3.9 29750.0 9.22 1487.5 13.71	2728.00 XEQ A		
7.22 1407.3 13.11	Σ+ CLΣ FIT		
	6.42 ENTERT		
LBS NOX/TEST = 50.60	3845.00 ΧΕΩ Α Σ+ CLΣ FIT		
	8.37 ENTERT		
LBS FUEL/TEST = 3394	4883.00 XEQ A		
1 P. 1101 1 P. OF FUEL	Σ+ CLΣ FIT		
LBS NOX/LBS OF FUEL USED IN TEST = 0.01491	11.78 ENTERT		
1350 IN 1531 - 8.81471	6662.00 XEQ A		
	Σ+ CLΣ FIT		
LABELS E AND H	14.80 ENTER† 8031.00 XEQ A		
LADEDO E AND II	Σ+ CLΣ FIT		
5.0 996.0	18.71 ENTERT		
1.16 83.0 9.10	9201.00 XEQ A		
	Σ+ CLΣ FIT		
5.0 4850.0	21.38 ENTER†		
9.85 404.2 3.98	9957.09 ΧΕΩ Α Σ+ CLΣ FIT		
10.0 8514.0	25.16 ENTERT		
23.12 1419.0 32.81	19548.09 XEQ A		
	Σ+ CLΣ FIT		
35.9 29750.9	XEQ E		
9.22 17354.2 160.01	L EX LOG P 8		
A FUTDU BELETER	XEQ E		
† ENTRY DELETED	EXP		
3.9 29750.9	a=2.98392688 b=0.00020093		
9.22 1487.5 13.71	R†2=0.99832741		

LBS Z/TEST = 50.60

LBS FUEL/TEST = 3394

USED IN TEST = 9.01491

LBS Z/LBS OF FUEL

A5. PROGRAM AIRN (HP-41C/41CV/41CX)

A5.1 Description of Program AIRN

Program AIRN makes the same calculations as program AIRNP. Program AIRN does not use a printer.

A5.2 Definitions

Program AIRN uses the same definitions as program AIRNP.

A5.3 Calculation of Emission Indexes

Program AIRN uses the same calculations as program AIRNP.

A5.4 Description of Labels Used in Program AIRN

LABEL USE

- C Uses inputs of either (a) time, thrust and fuel flow rate or (b) time, fuel flow rate and emission index to calculate the emissions of any constituent for a single power setting. When using option (a), the program must contain constants for an equation which defines the relation between thrust and emission index.
- E Uses inputs of times, fuel flow rates and emission indexes to calculate emissions of any constituent.
- F May be used instead of 'XEQ AIRN' to start the program, when the program is positioned in the main memory of the calculator.
- J After entry of data for any number of power settings, use label J to determine the total amount of the constituent produced and the fuel used by these power settings, and the amount of the constituent formed for each pound of fuel used.
- H Cancels the last entry.

A5.5 Instructions for Using Program AIRN

KEYSTROKES DISPLAY

R/S

FUEL?

REMARKS

MINIMUM SIZE 005

MINIMUM SIZE 00	5	
XEQ AIRN	KEY C or E	Label C needs, as program steps 08 and 10, constants which define the plot of thrust vs. the emission index of the constituent.
		The example in this demonstration uses a simulated engine test for an F404 engine with run times, thrusts, fuel flow rates and emission indexes, at power settings as follows:
		Minutes Thrust F EI
		Idle 5 - 996 1.16 89% rpm 5 5945 4850 - IRP 10 10190 8514 - Afterburner 3 - 29750 9.22
		Key in C.
С	MINUTES?	Key in the time of operation at idle.
5	5	Key in R/S to continue.
R/S	THRUST?	The data at this power setting does not include thrust. Key in R/S to skip to the input of fuel flow rate.
R/S	FUEL?	Key in the fuel flow rate.
996	996	Key in R/S to continue.
R/S	EI?	Key in the emission index.
1.16	1.16	Key in R/S to continue.
R/S	MINUTES?	Key in the time at the next power setting (89% rpm).
5	5	Key in R/S to continue.
R/S	THRUST?	Key in thrust.
5945	5945	Key in R/S to continue.

Key in the fuel flow rate.

Instructions for Using Program AIRN (continued)

KEYSTROKES	DISPLAY	REMARKS
4850	4850	Key in R/S to continue.
R/S	MINUTES?	Key in the time at the next power setting (IRP).
10	10	Key in R/S to continue.
R/S	THRUST?	Key in thrust.
10190	10190	Key in R/S to continue.
R/S	FUEL?	Key in the fuel flow rate.
8514	8514	Key in R/S to continue.
R/S	MINUTES?	Key in the time at the next power setting (afterburner).
3	3	Key in R/S to continue.
R/S	THRUST?	Key in R/S to use the emission index, in- stead of the thrust, for the calculation.
R/S	FUEL?	Key in the fuel flow rate.
29750	29750	Key in R/S to continue.
R/S	EI?	Key in the emission index.
9.22	9.22	Key in R/S to continue.
R/S	MINUTES?	There are no other power settings in this calculation. Key in J to continue.
J	Z/TEST =	Key in R/S to continue.
R/S	50.60	The display shows the pounds of the constituent produced by the sequence of power settings. Key in R/S to continue.
R/S	FUEL/TEST =	Key in R/S to continue.
R/S	3394	The display shows the pounds of fuel used in the test. Key in R/S to continue.
R/S	Z/LB FUEL =	Key in R/S to continue.

Instructions for Using Program AIRN (concluded)

KEYSTROKES	DISPLAY	REMARKS		
R/S	0.01491	The display shows pounds of the constituent produced for each pound of fuel used. Key in R/S to continue.		
R/S	KEY C OR E	The program is ready to start a new calculation from a group of power settings. Label E makes calculations using time of operation, fuel flow rate and emission index. Label H corrects an entry.		

APPENDIX B

Computer Programs

Appendix B contains four figures, the listings for the computer programs MATEI, SAMPFL and the listing for the file T56001M.

Figure B1 lists the 100 components of the comprehensive matrix using the data from the sample calculation of SAE AIR 1533. Figure B2 shows the matrix constant and the P vector. Figure B3 gives specific examples of some calculations using the P vector. Figure B4 shows the print-out from program MATEI using a Hewlett Packard LaserJet printer and the default font of the printer. The data in Figure B4 are the same as those in Figure 4-6 of Paragraph 4.5.1. However, the appearance differs because the printer used other fonts to prepare Figure 4-6. These figures are references for anyone installing the matrix program on a computer.

The instructions for using the computer programs appear as comment lines at the beginning of and throughout the program listings. Additional instructions appear on the computer monitor during the operation of the programs.

		MATRIX A		
0	1	0	0	0
1	9.5	0	0	00032
0	0	0	0	2
0	19	0	0	017686
0	2	0	2	1
1		2	1	428443
0	0	0	0	0
0		1	1	-1.5804
.0201214	-1	0	.0018	0201214
0	0	0	0	0
5.003035E-04	00013	0	0	-5.003035E-04
-1	0	0	0	0
.000225	0	0	0	0
0	-9.5	0	0	0
.00002	.0000028	0	0	.0000056
0	0	95	-1	0
9.000001E-06	1.26E-06	0	0	2.52E-06
0	0	0	-1	0
-1	1	0	1	1 0
1	1	1	1	

The size of matrix is 10×10 . Each row of the matrix uses two lines of print-out. Columns 1 to 5 of the matrix are on the first line of the print-out for the row. Columns 6 to 10 are on the second line.

Figure Bl. Components of matrix A for the solution of the ten sumiltaneous combustion equations using the data of the sample calculation of SAE AIR 1533 and program MATEI.

	MATRIX CONSTANT							
	9.5							
	19							
	0							
	0							
	0							
	0							
	0							
<u> </u>	0							
	0	,						
	0	·						
	P VECTOR							
Symbol	Program MATEI	Reported in SAE AIR 1533						
P _T	469.0321	469.03						
P ₁	9.314995	9.3150						
P ₂	363.601	363.60						
P ₃	82.40501	82.405						
P ₄	13.46352	13.464						
P ₅	0.2267105	0.2267						
P ₆	1.110885E-02	0.011109						
P ₇	5.489647E-03	0.005490						
P ₈	4.266954E-03	0.004267						
x	460.1441	460.14						

Figure B2. Matrix constant for the solution of the ten simultaneous combustion equations using the data for the sample calculation of SAE AIR 1533 and program MATEI, and the P vector from the matrix solution.

DATA

CALCULATION OF THE CONCENTRATION OF CARBON MONOXIDE [equations (A33), (30) and (A8) of SAE AIR 1533]

CO, ppm (dry) =
$$[P_5/(P_T - P_4)] \times 10^6$$

= $[0.226711/(469.0321 - 13.46352)] \times 10^6$
= 497.6
CO, ppm (semi-dry) = $([CO]_d/h_{sd}) \times 10^6$
= $(0.0004976/1.00607) \times 10^6$ = 494.6
CO, ppm (wet) = $(P_5/P_T)(10^6)$
= $(0.226711/469.0321) \times 10^6$ = 483.4

CALCULATION OF THE EMISSION INDEX OF CARBON MONOXIDE [equation (45) of SAE AIR 1533]

EI_{CO} =
$$(P_5/m)(10^3 M_{CO})/(M_C + (n/m)M_H)$$

= $(0.226711/9.5)(28.011 \times 10^3)/14.027$
= 47.65

Figure B3. Calculation of the dry, semi-dry and wet concentrations and the emission index of carbon monoxide using the P vector.

T56-A-16	MILITARY		F	ile T56001M
J = -0.07 L = -0.00010 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.86 in h = 0.0088 h _{sd} = 0.0060	84	m = 13.0 $n = 23.4$ $c/e = 0.95$	
CONSTITUENT	E Measure	XHAUST CONC d Ca dry	alculated	EMISSION INDEX
Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/ Hydrocarbons, meth Oxygen	ppm ppm x ppmC 2.9	sd 2.20	2.18 2.1 67.5 66.1 65.4 64.0 2.1 2.1 3.0 2.9	13 3229.31 1 10.45 0 10.12 1 0.33 9 0.14 0.16
Nitrogen Water, calc.	રુ રુ	79.79		58 77
Sulfur dioxide, ca Oxides of nitrogen Oxides of nitrogen	at 3% oxygen,	calc.(ppm meas.(ppm	wet) 345 wet) 318	0.40
<pre>K = 0.9723 F/A = 0.010231 Combustion efficie Shaft horsepower = Engine speed = 138 Engine exhaust tem</pre>	4090 20 rpm	0°F		
EMISSION RATE (pou for a fuel flow ra				
Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/ Hydrocarbons, meth Sulfur dioxide	x 0.31			

Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE
Measurement at NAVAIREWORKFAC ALAMEDA
Date of measurement 23 JUNE 1976
Engine S/N 102138
Test Cell 11, single point probe in test cell exhaust stack.
JP-5 fuel.

Figure B4. Print-out from program MATEI.

```
10 'Program Listing - MATEI
20 '
30 'AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE. SEPTEMBER 1987 (jak)
40 '
50 'This program uses measured concentrations of carbon monoxide, carbon
60 'dioxide, oxides of nitrogen and hydrocarbons; and fuel flow rates to
70 'calculate emission indexes, emission rates and other emission parameters.
80 '
90 'The program uses the comprehensive matrix solution of ten combustion
100 'equations as described in Aerospace Information Report, AIR 1533.
110 '(Reference 1, of AESO 1-87).
120 '
130 'The program uses either an IBM Proprinter or a Hewlett Packard LaserJet
140 'printer. If some other printer is used, it may be necessary to modify the
150 'program to get the proper value field for the degree symbol. The LaserJet
160 'printer adds horizontal and vertical rules, and bold letters to the print-
170 'out if the printer has the HP 92286T font cartridge. For an example of
180 'a ruled print-out see Figure 4-3 of paragraph 4.5.1.
                                                           Without the
190 '92286T cartridge, the LaserJet printer uses the default font (courier)
200 'resident in the printer. For an example of this print-out see Figure B4
210 'of Appendix B.
220 '
230 'To print double strike on the IBM Proprinter, delete 3350.
240 'To print the matrix and the matrix constant, delete 4210.
250 'To print the P vector, delete 4310.
260 '
270 'To use this program your computer needs a basic compiler. This program
280 'was written using the IBM Personal Computer Basic Version D3.10.
290 '
300 'To run this program, load the program and key in run. Then, respond to
310 'queries as they appear on the monitor.
320 '
330 'The query "which file" has optional responses.
340 '
350 '(1) Key in the code of a file which you have established using the program
360 'SAMPFL. Key return to continue.
370
380 '(2) Key in 0 (zero) then return to permit entry of each variable in
390 'response to a series of queries. If you respond to a query by keying
400 'return, the program makes no entry or for some variables assigns a default
410 'value. Return sends the program to the next variable or continues the
420 'program if there are no other variables to be entered. The variables
430 'assigned default values are PRI=2, SULF = 0.02\%, m = 13, n = 23.4,
440 'hsd = 0.00607 and converter efficiency = 0.95.
450 '
460 'The variable h must have a value. If it is assigned zero, the program
470 'next asks for inputs of relative humidity, temperature and barometric
480 'pressure. After entry of the engine exhaust temperature (EGT), the pro-
490 'gram continues with the matrix calculation without further prompting.
500 '
510 '(3) Key in 9, then return to use the basic matrix of Reference 1, page 9.
520 'The basic matrix solution makes no adjustments for the basis of measure-
530 'ment, (wet, dry or semi-dry), humidity, instrument interferences or
540 'efficiency of the oxides of nitrogen converter. This option uses the
```

```
550 'm and n values of JP-5 fuel. If you want to use other values you
560 'must make changes in the program.
570 '
580 'The inputs using option (3) are the concentrations of carbon monoxide,
590 'carbon dioxide, oxides of nitrogen and hydrocarbons; and the fuel flow
600 'rate. The calculations appear on the monitor as a table of emission
610 'indexes and emission rates. This option is suitable for approximate
620 'calculations.
630 '
640 'For color monitors set foreground (FG) and background (BG) (line 680)
650 'to whatever color you wish. FG must not be zero. For monochrome
660 'monitors, BG must be zero.
670 '
680 FG=14:PG=1
690 '
700 OPTION BASE 1:COLOR FG,0:CLS
710 DIM A(10,10), E(10), F(10), G(10,10), P(10)
720 J$="####.#":K$="######.##":L$="####.###":N$="####.##"
730 '
740 FOR I = 1 TO 10:READ F(I):NEXT I
750 FOR I=1 TO 10:FOR J=1 TO 10:READBA((I,J):NEXT J:NEXT I
760 DATA 13,23.4,0,0,0,0,0,0,0,0
770 DATA 0,1,0,0,0,1,13,0,0,-0.00032
780 DATA 0,0,0,0,2,0,23.4,0,0,-.02
790 DATA 0,2,0,2,1,1,0,2,1,-0.4296
800 DATA 0,0,2,0,0,0,0,1,1,-1.5804
810 DATA 0, -1,0,0,0,0,0,0,0,0
820 DATA 0,0,0,0,0,-1,0,0,0,0
830 DATA 0,0,0,0,0,0,-13,0,0,0
840 DATA 0,0,0,0,0,0,0,-1,-1,0
850 DATA 0,0,0,0,0,0,0,0,-1,0
860 DATA -1,1,1,1,1,1,1,1,0
870 PRINT "KEY 1 FOR IBM PROPRINTER"
880 PRINT "KEY ENTER FOR HP LASERJET PRINTER"
890 PRINT
900 COLOR FG, BG: INPUT "WHICH PRINTER"; PRI
910 IF PRI=0 THEN PRI=2
920 IF PRI=1 THEN 960 ELSE 930
930 LPRINT CHR$(27); "&aOR"
           CHR$(27);"&a8L"
940 LPRINT
950 LPRINT CHR$(27); "&k12H"
960 COLOR FG, 0: CLS: COLOR FG, BG: INPUT "WHICH FILE"; X$
970 IF X$="0" THEN 1020 ELSE 980
980 IF X$="9" THEN 990 ELSE 1900
990 C(1)=13:C(2)=23.4:C(3)=0:C(4)=0:C(5)=1:C(6)=2
1000 COLOR FG.O:CLS
1010 GOTO 1720
1020 PRINT: COLOR FG. 0
1030 PRINT "FOR MEASUREMENTS BY AESO KEY IN 1"
1040 PRINT "FOR MEASUREMENTS BY NAPC KEY IN 2"
1050 PRINT "FOR MEASUREMENTS BY OTHERS KEY NAME"
1060 PRINT: COLOR FG, BG
1070 INPUT " MEASURED BY
                              ":M$
1080 IF M$="1" THEN 1110
'090 IF M$="2" THEN 1130
```

```
1100 GOTO 1140
1110 MS-"AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE"
1120 GOTO 1140
1130 M$="NAVAL AIR PROPULSION CENTER"
1140 COLOR 12,0:PRINT TAB(15)M$
1150 COLOR FG, BG
1160 INPUT " PLACE OF MEASUREMENT"; P$: PRINT
1170 INPUT " DATE OF MEASUREMENT"; D$: PRINT
1180 INPUT " ENGINE SERIAL NUMBER": SNS: PRINT
1190 INPUT " ADDITIONAL REMARKS (LINE 1)"; R$: PRINT
1200 INPUT " ADDITIONAL REMARKS (LINE 2)"; RR$: PRINT
1210 INPUT " ENGINE TYPE, NUMERAL, MANF., MODEL (EX. J79-GE-8)"; A$: PRINT
1220 INPUT " POWER SETTING"; B$: PRINT
1230 COLOR FG, 0: PRINT
1240 PRINT "1 STARTS WITH INPUT OF INSTRUMENT COEFFICIENTS"
1250 PRINT "2 STARTS WITH INPUT OF x, y, h"
1260 PRINT: COLOR FG, BG
1270 INPUT " KEY IN 1, 2."; R: COLOR 14,0
1280 CLS:PRINT
1290 IF R-1 THEN 1350
1300 IF R-2 THEN 1410
1310 COLOR 2,0
1320 CLS: PRINT "YOU MUST KEY IN 1 OR 2 TO USE THE MATRIX": PRINT : PRINT
1330 GOTO 1230
1340 X-5:GOTO 1500
1350 COLOR FG, BG
1360 INPUT "J"; B(1):PRINT
1370 INPUT "L"; B(2):PRINT
1380 INPUT "L'"; B(3):PRINT
1390 INPUT "M"; B(4):PRINT
1400 INPUT "M'"; B(5):PRINT
1410 COLOR FG, 0: PRINT
1420 PRINT "3 CONTINUES WITH INPUT OF x, y, h"
1430 PRINT "5 CONTINUES WITH INPUT OF x, y, h, hsd, converter efficiency"
1440 PRINT: COLOR FG. BG
1450 INPUT " 3, or 5"; X:COLOR FG,0
1460 CLS: PRINT
1470 PRINT
1480 IF X=3 THEN 1490
1490 COLOR FG, BG
1500 INPUT "x"; C(1): PRINT
1510 IF C(1)=0 THEN C(1)=13
1520 INPUT "y";C(2):PRINT
1530 IF C(2)=0 THEN C(2)=23.4
1540 INPUT "h"; C(3):C(4)=.00607:C(5)=.95:PRINT
1550 IF C(3)=0 THEN 1560 ELSE 1590
1560 INPUT "RELATIVE HUMIDITY"; C(7): PRINT
1570 INPUT "TEMPERATURE"; C(8): PRINT
1580 INPUT "BAROMETRIC PRESSURE"; C(9): PRINT
1590 IF X-5 THEN 1600 ELSE 1640
1600 INPUT "hsd"; C(4): PRINT
1610 IF C(4)=0 THEN C(4)=.00607
1620 INPUT "CONVERTER EFFICIENCY"; C(5): PRINT
1630 IF C(5)=0 THEN C(5)=.95
1640 COLOR FG, 0
```

```
1650 INPUT "SULFUR CONTENT OF FUEL, %"; SULF: PRINT
1660 IF SULF-0 THEN SULF-.02: '%
1670 PRINT "KEY 1 FOR NOx MEASURED WET"
1680 PRINT "KEY 2 FOR NOx MEASURED SEMI-DRY"
1690 PRINT : COLOR FG, BG
1700 INPUT " NOX MEASUREMENT"; C(6): PRINT
1710 PRINT: COLOR FG, 0: CLS: COLOR FG, BG
1720 IF X$="9" THEN 1730 ELSE 1740
1730 INPUT " ENGINE TYPE, NUMERAL, MANF., MODEL (EX. J79-GE-8)"; A$:PRINT
1740 INPUT " POWER SETTING"; B$: PRINT
1750 INPUT " CO":D(1):PRINT
1760 INPUT " CO2"; D(2): PRINT
1770 INPUT " NOx":D(3):PRINT
1780 IF X$="9" THEN 1800 ELSE 1790
1790 INPUT " NO"; D(4): PRINT
1800 INPUT "CxHy"; D(5): PRINT
1810 IF X$="9" THEN 1830 ELSE 1820
1820 INPUT "O2"; D(6): PRINT
1830 INPUT "FUEL FLOW"; FF: PRINT
1840 IF X$="9" THEN 1960 ELSE 1850
1850 INPUT "THRUST"; TH: PRINT
1860 INPUT "HORSEPOWER"; HP: PRINT
1870 INPUT "RPM"; RPM: PRINT
1880 INPUT "EGT"; EGT: PRINT
1890 GOTO 1960
1900 X$="A:"+X$
1910 OPEN "I", #1, X$
1920 INPUT #1,A$,B$,F$,M$,P$,D$,SN$,R$,RR$,FF,TH,RPM,HP,EGT,SULF
1930 INPUT \#1,B(1),B(2),B(3),B(4),B(5)
1940 INPUT \#1,C(1),C(2),C(3),C(4),C(5),C(6),C(7),C(8),C(9)
1950 INPUT #1,D(1),D(2),D(3),D(4),D(5),D(6)
1960 PRINT: COLOR 2,0: PRINT "WAIT"
1970 IF C(7)=0 THEN 1980
1980 IF C(8)=0 THEN 2120 ELSE 1990
1990 IF C(8)<51 THEN 2040 ELSE 2000
2000 IF C(8)<76 THEN 2070 ELSE 2010
2010 X = .031767 * C(8)
2020 VP-EXP(X)*.080455
2030 GOTO 2100
2040 X-.038251*C(8)
2050 VP-EXP(X)*.053226
2060 GOTO 2100
2070 X-.035264*C(8)
2080 VP = EXP(X) * .061928
2090 GOTO 2100
2100 AVP=C(7)/100*VP
2110 C(3) = AVP/(C(9) - AVP)
2120 F(1)=C(1):F(2)=C(2)
2130 IF X$="9" THEN 2170
2140 IF D(4)=0 THEN 2150 ELSE 2170
2150 D(4)=D(3)*.97
2160 FLAG-1
2170 A(1,7)=C(1):A(2,7)=C(2)
2180 A(2,10)=(-2)*C(3):A(3,10)=-.41896-.00064-C(3)
2190 E-D(2)/100*(1+C(4))
```

```
2200 A(5,1)=E:A(5,4)=D(2)/100*B(1):A(5,5)=-E
2210 E-D(1)/10^6*(1+C(4))
2220 A(6,1)=E+C(4)*B(4):A(6,5)=-E-C(4)*B(4):A(6,2)=B(2)
2230 A(7,1)=D(5)/10^6:A(7,7)=-C(1)
2240 A(8,1)=D(3)/10^6:A(8,2)=D(3)/10^6*B(3)
2250 A(8,5)=D(3)/10^6*B(5):A(8,8)=-C(5)
2260 A(9,1)=D(4)/10^6:A(9,2)=D(4)/10^6*B(3)
2270 A(9,5)=D(4)/10^6*B(5)
2280 IF C(6)-1 THEN 2340
2290 Q-1+C(4)*(1+B(5))
2300 A(8,1)=D(3)/10^6*Q:A(8,5)=-A(8,1)
2310 A(9,1)=D(4)/10^6*Q:A(9,5)=-A(9,1)
2320 IF X$="9" THEN 2330 ELSE 2340
2330 A(6,5)=0: A(8,5)=0:A(5,5)=0
2340 FOR I=1 TO 10
2350 FOR J-1 TO 10
2360 G(I,J)=A(I,J)
2370 NEXT J:NEXT I
2380 FOR I-1 TO 10
2390 E(I) = F(I)
2400 NEXT I
2410 FOR J1-1 TO 10
2420 \text{ TEMP} = 0
2430 FOR J2 - J1 TO 10
2440 IF ABS(A(J2,J1)) < TEMP THEN GOTO 2470
2450 \text{ TEMP} = ABS(A(J2,J1))
2460 IBIG - J2
2470 NEXT J2
2480 IF IBIG - J1 THEN GOTO 2570
2490 FOR J2 -J1 TO 10
2500 TEMP - A(J1,J2)
2510 A(J1,J2) = A(IBIG,J2)
2520 A(IBIG,J2)-TEMP
2530 NEXT J2
2540 \text{ TEMP} = E(J1)
2550 E(J1)=E(IBIG)
2560 E(IBIG)-TEMP
2570 IF J1-10 THEN GOTO 2670
2580 N1 - J1+1
2590 FOR J2-N1 TO 10
2600 A(J2,J1)-A(J2,J1)/A(J1,J1)
2610 FOR J3-N1 TO 10
2620 A(J2,J3)=A(J2,J3)-A(J2,J1)*A(J1,J3)
2630 NEXT J3
2640 E(J2)=E(J2)-A(J2,J1)*E(J1)
2650 NEXT J2
2660 NEXT J1
2670 E(10)-E(10)/A(10,10)
2680 N1-10
2690 FOR J2=N1 TO 10
2700 E(N1-1) \sim E(N1-1) - E(J2) *A(N1-1,J2)
2710 NEXT J2
2720 E(N1-1)=E(N1-1)/A(N1-1,N1-1)
2730 N1-N1-1
2740 IF N1<1 THEN GOTO 2690
```

```
2750 FOR I-1 TO 10
2760 P(I)-E(I)
2770 NEXT I
2780 FOR I-1 TO 10
2790 FOR J-1 TO 10
2800 A(I,J)=G(I,J)
2810 NEXT J:NEXT I
2820 C=12.011:0=15.9994:H=1.008:N=14.0067
2830 MWCO-C+0:MWCO2-C+0*2:MWNO2-N+0*2
2840 MWCHX=C+H*F(2)/F(1):MWCH4=C+H*4
2850 M=F(1)*C+F(2)*H
2860 EICO-P(6)*1000*MWCO/M
2870 EICO2-P(2)*1000*MWCO2/M
2880 EINOX=(P(9)+P(8))*1000*MWN02/M
2890 EINO-P(9)*1000*MWN02/M
2900 EINO2-P(8)*1000*MWNO2/M
2910 EICHX-P(7)*F(1)*1000*MWCHX/M
2920 EICH4-P(7)*F(1)*1000*MWCH4/M
2930 HHSD=1+C(4)
2940 COW=P(6)/P(1)*10^6
2950 COD=P(6)/(P(1)-P(5))*10^6
2960 COSD-COD/HHSD
2970 CO2W=P(2)/P(1)*100
2980 CO2D=P(2)/(P(1)-P(5))*100
2990 CO2SD-CO2D/HHSD
3000 NOXW=(P(8)+P(9))/P(1)*10^6
3010 NOXD=(P(8)+P(9))/(P(1)-P(5))*10^6
3020 NOXSD-NOXD/HHSD
3030 NOW=P(9)/P(1)*10^6
3040 NOD=P(9)/(P(1)-P(5))*10^6
3050 NOSD-NOD/HHSD
3060 \text{ NO2W-P(8)/P(1)*10^6}
3070 NO2D=P(8)/(P(1)-P(5))*10^6
3080 NO2SD-NO2D/HHSD
3090 CXHYW=F(1)*P(7)/P(1)*10^6
3100 CXHYD=F(1)*P(7)/(P(1)-P(5))*10^6
3110 CXHYSD=CXHYD/HHSD
3120 O2D=P(4)/(P(1)-P(5))*100
3130 O2SD-O2D/HHSD
3140 O2W=P(4)/P(1)*100
3150 N2D=P(3)/(P(1)-P(5))*100
3160 N2SD-N2D/HHSD
3170 N2W-P(3)/P(1)*100
3180 K=(P(1)-P(5))/P(1)
3190 O2DM-1.00607*D(6)
3200 O2WM-O2DM*K
3210 H20=P(5)/P(1)*100
3220 FA=(C(1)*C+C(2)*H)/28.965/P(10)
3230 N=(1-4.346*EICO/18730-EICHX/1000)*100
3240 F=NOXW*17.948/(20.948-02W)
3250 G-NOXW*17.948/(20.948-02WM)
3260 T-FF/1000
3270 WCO-T*EICO:WCO2-T*EICO2:WNOX-T*EINOX
3280 WCHX=T*EICHX:WCH4=T*EICH4:WSO2=T*SULF*20
3290 CLS:COLOR FG, 0
```

```
3300 IF C(6)=1 THEN 3310 ELSE 3330
3310 H$="w"
3320 GOTO 3340
3330 H$-"sd"
3340 'Delete the next step to print double strike on the IBM Proprinter.
3350 GOTO 3380
3360 LPRINT
3370 LPRINT CHR$(27); CHR$(71);
3380 IF X$="9" THEN 3390 ELSE 3680
3390 CLS:COLOR 15,0
3400 PRINT "Approximate emission indexes and emission rates for"
3410 PRINT "a ";
3420 COLOR 10,0:PRINT A$;
3430 COLOR 15,0:PRINT " engine at ";
3440 COLOR 10,0:PRINT B$;
3450 COLOR FG,0
3460 PRINT : PRINT : PRINT
3470 PRINT "CONSTITUENT
                                        EMISSION INDEX
                                                                POUNDS PER HOUR"
3480 PRINT : PRINT
3490 PRINT TAB(1) "CARBON MONOXIDE";
3500 PRINT TAB(30)USING K$; EICO;
3510 PRINT TAB(55)USING K$; WCO: PRINT
3520 PRINT TAB(1) "CARBON DIOXIDE";
3530 PRINT TAB(30)USING K$; EICO2;
3540 PRINT TAB(55)USING K$; WCO2: PRINT
3550 PRINT TAB(1) "OXIDES OF NITROGEN (AS NO2)";
3560 PRINT TAB(30)USING K$; EINOX;
3570 PRINT TAB(55)USING K$; WNOX: PRINT
3580 PRINT TAB(1)"HYDROCARBONS (AS CHY/X)";
3590 PRINT TAB(30)USING K$; EICHX;
3600 PRINT TAB(55)USING K$; WCHX: PRINT
3610 PRINT TAB(1) "HYDROCARBONS (AS CH4)";
3620 PRINT TAB(30)USING K$; EICH4;
3630 PRINT TAB(55)USING K$; WCH4: PRINT
3640 PRINT TAB(1) "SULFUR (AS SO2)";
3650 PRINT TAB(30)USING K$; SULF*20;
3660 PRINT TAB(55)USING K$; WSO2: PRINT
3670 GOTO 6290
3680 IF KK=2 THEN 3690 ELSE 3700
3690 LPRINT: LPRINT
3700 LPRINT TAB(3)A$ TAB(23)B$ TAB(56)F$:COLOR FG,0
3710 LPRINT
3720 IF B(1)=0 THEN 3730 ELSE 3750
3730 LPRINT TAB(3)"J";
3740 GOTO 3760
3750 LPRINT TAB(3)"J = "USING "##.##"; B(1);
3760 IF C(7)=100 THEN 3770 ELSE 3790
3770 LPRINT TAB(21) "DEW = "USING "###." : C(8);
3780 GOTO 3820
3790 IF C(8)=0 THEN 3860
3800 IF C(7)=100 THEN 3850
                       - "USING "##.";C(8);
3810 LPRINT TAB(21)"T
3820 IF PRI=1 THEN 3830 ELSE 3850
3830 LPRINT CHR$(248);"F";
3840 GOTO 3860
```

```
3850 LPRINT CHR$(179);"F";
3860 LPRINT TAB(48) "m - "USING "##.#"; C(1)
3870 IF B(2)=0 THEN 3880 ELSE 3900
3880 LPRINT TAB(3)"L";
3890 GOTO 3910
3900 LPRINT TAB(3)"L = "USING "##.#####"; B(2);
3910 IF C(7)=0 THEN 3940
3920 IF C(7)=100 THEN 3940
3930 LPRINT TAB(21)"RH - "USING "##%"; C(7);
3940 LPRINT TAB(48)"n = "USING "##.#"; C(2)
3950 IF B(3)=0 THEN 3960 ELSE 3980
3960 LPRINT TAB(3)"L'";
3970 GOTO 4000
3980 LPRINT TAB(3)"L' = "USING "##.##";B(3);
3990 IF C(9)=0 THEN 4020
                         ="USING "###.##";C(9);
4000 LPRINT TAB(21)"B
4010 LPRINT " in. Hg";
4020 LPRINT TAB(42) NOx c/e = "USING "##.##"; C(5)
4030 IF B(4)=0 THEN 4040 ELSE 4060
4040 LPRINT TAB(3)"M";
4050 GOTO 4070
4060 LPRINT TAB(3)"M - "USING "##.#####";B(4);
4070 LPRINT TAB(21)"h - "USING "## .######"; C(3)
4080 IF B(5)=0 THEN 4090 ELSE 4110
4090 LPRINT TAB(3)"M'";
4100 GOTO 4120
4110 LPRINT TAB(3)"M' = "USING "##.##"; B(5);
 4120 IF PRI-1 THEN 4130 ELSE 4150
4130 LPRINT TAB(21)"h";
 4140 GOTO 4170
 4150 LPRINT TAB(21) "h"; CHR$(27); "&a+.5R";
 4160 GOTO 4190
 4170 LPRINT "sd = ";USING "排. #排排排";C(4)
 4180 GOTO 4300
 4190 LPRINT "sd"; CHR$(27); "&a-.5R"; " = "; USING "##.#####"; C(4)
 4200 'Delete the next step to print the matrix and the matrix constant.
 4210 GOTO 4300
 4220 LPRINT: FOR I=1 TO 10
 4230 LPRINT TAB(2)A(I,1) TAB(18)A(I,2) TAB(32)A(1,3);
 4240 LPRINT TAB(46)A(I,4) TAB(60)A(I,5)
 4250 LPRINT TAB(2)A(I,6) TAB(18)A(I,7) TAB(32)A(I,8);
 4260 LPRINT TAB(46)A(I,9) TAB(60)A(I,10):LPRINT
 4270 NEXT I
 4280 FOR I=1 TO 10
 4290 LPRINT F(I):NEXT I
 4300 'Delete the next step to print the P vector.
 4310 GOTO 4340
 4320 LPRINT: LPRINT "P VECTOR"
 4330 FOR I=1 TO 10:LPRINT E(I):NEXT I
 4340 LPRINT
 4350 LPRINT TAB(6) "CONSTITUENT" TAB(33) "EXHAUST CONCENTRATION";
 4360 LPRINT TAB(60) "EMISSION"
 4370 LPRINT TAB(27) "Measured TAB(44) "Calculated TAB(62) "INDEX"
 4380 LPRINT TAB(41) "dry "TAB(47) "semi-"TAB(54) "wet"
 4390 LPRINT TAB(48) "dry": LPRINT
```

```
4400 LPRINT TAB(2) "Carbon monoxide" TAB(23) "ppm";
4410 LPRINT TAB(27)USING J$; D(1);
4420 LPRINT " sd":
4430 LPRINT TAB(38)USING J$; COD;
4440 LPRINT TAB(45)USING J$; COSD;
4450 LPRINT TAB(52)USING J$; COW;
4460 LPRINT TAB(59)USING K$; EICO
4470 LPRINT TAB(2) "Carbon dioxide" TAB(24) "%";
4480 LPRINT TAB(29)USING "##.##";D(2);
4490 LPRINT " sd";
4500 LPRINT TAB(38)USING N$; CO2D;
4510 LPRINT TAB(45)USING N$; CO2SD;
4520 LPRINT TAB(52)USING N$; CO2W;
4530 LPRINT TAB(59)USING K$; EICO2
4540 LPRINT TAB(2) "Oxides of nitrogen" TAB(23) "ppm";
4550 LPRINT TAB(27)USING J$; D(3);
4560 LPRINT " ";H$;
4570 LPRINT TAB(38)USING J$; NOXD;
4580 LPRINT TAB(45)USING J$; NOXSD;
4590 LPRINT TAB(52) USING J$; NOXW;
4600 LPRINT TAB(59) USING K$; EINOX
4610 LPRINT TAB(2) "Nitric oxide" TAB(23) "ppm";
4620 IF FLAG-1 THEN 4650
4630 LPRINT TAB(27)USING J$; D(4);
4640 LPRINT " ";H$;
4650 LPRINT TAB(38)USING J$; NOD;
4660 LPRINT TAB(45)USING J$; NOSD;
4670 LPRINT TAB(52)USING J$; NOW;
4680 LPRINT TAB(59)USING K$; EINO
4690 LPRINT TAB(2) "Nitrogen dioxide" TAB(23) "ppm";
4700 LPRINT TAB(38)USING J$; NO2D;
4710 LPRINT TAB(45)USING J$; NO2SD;
4720 LPRINT TAB(52)USING J$; NO2W;
4730 LPRINT TAB(59)USING K$; EINO2
4740 LPRINT TAB(2) "Hydrocarbons, CHy/x"TAB(23) "ppmC";
4750 LPRINT TAB(27)USING J$;D(5);
4760 LPRINT " w":
4770 LPRINT TAB(38)USING J$;CXHYD;
4780 LPRINT TAB(45)USING J$; CXHYSD;
4790 LPRINT TAB(52)USING J$; CXHYW;
4800 LPRINT TAB(59)USING K$; EICHX
4810 LPRINT TAB(2) "Hydrocarbons, methane";
4820 LPRINT TAB(59)USING K$; EICH4
4830 LPRINT TAB(2) "Oxygen" TAB(24) "%";
4840 IF D(6)=0 THEN 4870
4850 LPRINT TAB(29)USING "##.#";D(6);
4860 LPRINT " sd";
4870 LPRINT TAB(38)USING N$;02D;
4880 LPRINT TAB(45)USING N$; O2SD;
4890 LPRINT TAB(52)USING N$;02W
4900 LPRINT TAB(2)"Nitrogen"TAB(24)"%"TAB(38)USING N$;N2D;
4910 LPRINT TAB(45)USING N$; N2SD;
4920 LPRINT TAB(52)USING N$; N2W
4930 LPRINT TAB(2) "Water, calc. "TAB(24) "%" TAB(52) USING N$; H20
4940 LPRINT
```

```
4950 LPRINT TAB(2) "Sulfur dioxide, calc. "TAB(59) USING K$; SULF*20
4960 LPRINT
4970 LPRINT TAB(2) "Oxides of nitrogen at 3% oxygen, calc.(ppm wet)";
4980 LPRINT TAB(52)USING "####";F
4990 LPRINT TAB(2) "Oxides of nitrogen at 3% oxygen, meas.(ppm wet)";
5000 IF D(6)=0 THEN 5010 ELSE 5020
5010 LPRINT :GOTO 5030
5020 LPRINT TAB(52)USING "####";G
5030 LPRINT
5040 LPRINT TAB(2)"K - "USING "#.####";K
5050 LPRINT TAB(2)"F/A = "USING "#.######"; FA
5060 LPRINT TAB(2) "Combustion efficiency = "USING "排.排排%";N
5070 IF TH-0 THEN 5090
5080 LPRINT TAB(2) "Thrust ="; TH; "pounds"
5090 IF HP-0 THEN 5110
5100 LPRINT TAB(2)"Shaft horsepower =";HP
5110 IF RPM-0 THEN LPRINT:GOTO 5130
5120 LPRINT TAB(2) "Engine speed =";RPM; "rpm"
5130 IF EGT=0 THEN LPRINT:GOTO 5200
5140 LPRINT TAB(2) "Engine exhaust temperature =";USING "#####";EGT;
5150 IF PRI-1 THEN 5180 ELSE 5160
5160 LPRINT CHR$(179); "F"
5170 GOTO 5190
5180 LPRINT CHR$(248):"F"
5190 CLS:COLOR FG:CLS
5200 CLS:COLOR FG
5210 IF TH=0 THEN 5220 ELSE 5230
5220 IF HP-O THEN LPRINT ELSE 5230
5230 IF FF-0 THEN 5240 ELSE 5280
5240 FOR I-1 TO 10
5250 LPRINT
5260 NEXT I
5270 GOTO 5380
5280 LPRINT
5290 LPRINT TAB(2) "EMISSION RATE (pounds of constituent per hour)"
5300 LPRINT TAB(2) "for a fuel flow rate of"; FF;
5310 LPRINT "pounds per hour": LPRINT
5320 LPRINT TAB(2) "Carbon monoxide" TAB(24) USING K$; WCO
5330 LPRINT TAB(2) "Carbon dioxide" TAB(24) USING K$; WCO2
5340 LPRINT TAB(2) "Oxides of nitrogen" TAB(24) USING K$; WNOX
5350 LPRINT TAB(2)"Hydrocarbons, CHy/x"TAB(24)USING K$; WCHX
5360 LPRINT TAB(2) "Hydrocarbons, methane"; TAB(24) USING KS; WCH4
5370 LPRINT TAB(2) "Sulfur dioxide" TAB(24) USING K$; WSO2
5380 LPRINT
5390 LPRINT TAB(2) "Measurement by ";M$
5400 LPRINT TAB(2) "Measurement at ": P$
5410 LPRINT TAB(2) "Date of measurement "; D$
5420 LPRINT TAB(2) "Engine S/N "; SN$
5430 LPRINT TAB(2)R$
5440 LPRINT TAB(2)RR$
5450 COLOR FG, 0:CLS
5460 IF PRI-1 THEN 5470 ELSE 5530
5470 PRINT "1 MOVES OPERATION TO THE END OF THE PROGRAM."
5480 PRINT "2 PRINTS ANOTHER COPY"
5490 PRINT "3 CONTINUES CALCULATION WITH NEXT POWER SETTING"
```

```
5500 PRINT: COLOR FG, BG
5510 INPUT "SELECT NUMBER"; KK
5520 ON KK GOTO 6280,3700,1710
5530 COLOR FG.O:CLS
5540 PRINT "1 MOVES OPERATION TO THE END OF THE PROGRAM AND FEEDS DATA SHEET."
5550 PRINT "2 CONTINUES CALCULATION WITH NEXT POWER SETTING"
5560 PRINT "3 ADDS RULES AND BOLD LETTERS TO THE DATA SHEET IF THE"
5570 PRINT " PRINTER HAS THE HP92286 FONT CARTRIDGE (LASERJET ONLY)."
5580 PRINT: COLOR FG. BG
5590 INPUT "SELECT NUMBER": KK
5600 ON KK GOTO 6260,5630,5650
5610 LPRINT CHR$(12)
5620 GOTO 6280
5630 LPRINT CHR$(12)
5640 GOTO 1710
5650 LPRINT CHR$(27);"(0B";
5660 LPRINT CHR$(27)+"&a5L";
5670 LPRINT CHR$(27)+"&a1R";
,,,,T";
5690 LPRINT ".
5700 LPRINT CHR$(27)"+&a2R":
5720 FOR I - 1 TO 5
5730 LPRINT ". .
  . " :
5740 NEXT I
5750 LPRINT CHR$(27) "&a9R";
5770 FOR I = 1 TO 15
5780 LPRINT ". .
  . " ;
5790 NEXT I
5800 LPRINT CHR$(27) "&a25R":
,,,,6";
5820 LPRINT ". .
5830 LPRINT CHR$(27) "&a27R";
...,6";
5850 LPRINT ".
  . " ;
5860 LPRINT ".
5870 LPRINT CHR$(27) "&a30R";
,,,,6";
5890 FOR I - 1 TO 6
5900 LPRINT ". .
  . " ;
5910 NEXT I
```

```
5920 LPRINT CHR$(27) "&a37R";
,,,,6";
5940 FOR I - 1 TO 9
5950 LPRINT ". .
5960 NEXT I
5970 LPRINT CHR$(27) "&a47R";
,,,,6":
5990 FOR I - 1 TO 6
6000 LPRINT ". .
  . " :
6010 NEXT I
6020 LPRINT CHR$(27) "&a54R";
,,,,G":
6040 LPRINT CHR$(27)+"(OU": CHR$(27)+"(slp8v":
6050 LPRINT CHR$(27)+"&a3r20C";
6060 LPRINT "A"
6070 LPRINT CHR$(27)+"&a7r20C";
6080 LPRINT "B"
6090 LPRINT CHR$(27)+"&a18.0r20C";
6100 LPRINT "C"
6110 LPRINT CHR$(27)+"&a27.0r20C";
6120 LPRINT "D"
6130 LPRINT CHR$(27)+"&a29.5r20C";
6140 LPRINT "E"
6150 LPRINT CHR$(27)+"&a34.5r20C";
6160 LPRINT "F"
6170 LPRINT CHR$(27)+"&a42.5r20C";
6180 LPRINT "G"
6190 LPRINT CHR$(27)+"&a51.5r20C";
6200 LPRINT "H"
6210 LPRINT CHR$(27); "E";
6220 LPRINT CHR$(27); "&aOR";
6230 IF PRI-1 THEN 6240 ELSE 6280
6240 LPRINT CHR$(27); CHR$(72);
6250 GOTO 6280
6260 LPRINT CHR$(12)
6270 IF KK-2 THEN 3680 ELSE 6280
6280 COLOR 7,0:CLS
6290 STOP
```

```
1 'Program listing - SAMPFL
2 'AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE, SEPTEMBER 1987 (jak)
3 '
4 'This program describes the use of a file to load data into program MATEI
5 'or MATEIE The lines numbered 10 or multiples of 10, and line 71, are the
6 'program. All other lines are instructions. Load File T56001M (stored as a
7 'BASIC program) and RUN to place it on a formatted disk in drive 'a'.
8 'instructions show which variables need to be (continued on line 12)
9 1
10 'OPEN "a:T56001M" FOR OUTPUT AS #1:F$="File T56001M"
12 'changed for each power setting of the engine. Figure 4-3 of paragraph
13 '4.5.1 shows the print-out obtained by using file T56001M in program
14 'MATEIE.
15 '
16 'Enter the name of the file in line 10.
17 '
18 'In line 20, specify the engine and the power setting.
19 '
20 'A$="T56-A-16":B$="MILITARY"
21 '
22 'In line 30, tell who made the measurement.
30 'M$-"AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE"
31 '
32 'In line 40, give the place of the measurement
33 '
40 'P$="NAVAIREWORKFAC ALAMEDA"
41 '
42 'In line 50, enter the date of the measurement.
43 '
50 'D$-23 "JUNE 1976"
52 'In line 60, enter the engine serial number. Make no entry between
53 'the quotation marks if the serial number is not known.
54 '
60 'SN$-"102138"
61 '
62 'In lines 70 and 71, write whatever you wish between the quotation marks,
63 'for two lines (up to 80 characters per line) of remarks.
64 '
70 'R$-" "
71 'RR$=" "
72 '
73 'In line 80, enter the fuel flow rate in pounds per hour.
74 '
80 'FF-2219
81 '
82 'In line 90, enter the engine speed as rpm.
83 '
90 'RPM-13820
91 '
92 'In line 100, for engines rated in thrust, enter the thrust in pounds.
93 'Enter zero in line 100 if the engine is rated in horsepower.
```

```
94 '
100 'TH-3890
101 '
102 'In line 110, for engines rated in horsepower, enter the horsepower.
103 'Enter zero in line 110 if the engine is rated in pounds thrust.
104 '
110 'HP-0
111 '
112 'In line 120, enter the engine exhaust temperature. The calculation
113 'of emission indexes, from the measured concentration of the constituents.
114 'does not use rpm, thrust or engine exhaust temperature. These variables
115 'may be useful in other studies.
116 '
120 'EGT-1970
121 '
122 'In line 130, enter the sulfur content of the fuel. In this example the
123 'sulfur content of the fuel is 0.02%.
124 '
130 'SULF-0.02:'%
131 '
132 'In line 140 enter the instrument interference coefficients
133 'in the following order: J, L, L',M, M'.
134 '
140 'DATA -.07, -.0001, .14, -.00033, .28
141 '
142 'In line 150, enter (1),(2) the molecular constants (m and n) of the fuel,
143 '(3) h, (4) hsd, (5) efficiency of the NOx converter, (6) 1 (if NOx meas-
144 'urement was wet), or 2 (if NOx measurement was semi-dry), (7) relative
145 'humidity (%) (for dew point measurements let the relative humidity equal
146 '100%), (8) dry bulb temperature in degrees F, and (9) barometric
147 'pressure (in. Hg). If (7), (8), and (9) are zeros, program MATEI uses
148 'the value of h as entered, otherwise it calculates a value for h.
149 '
150 'DATA 13,23.4,0,.00607,.95,2,15,97,29.97
151 '
152 ' In line 160 enter the measured concentrations of (1) carbon monoxide
153 '(ppm), (2) carbon dioxide (%), (3) oxides of nitrogen (ppm), (4) nitric
154 'oxide (ppm), if measured (or zero in not measured), (5) hydrocarbons (ppm)
155 'and (6) oxygen (%).
156 '
160 'DATA 11.1,2.21,67.1,0,2.9,17.6
161 '
162 'Program steps 170 to 250 are the same for all files.
163 '
170 'WRITE #1,A$,B$,F$,M$,SN$,R$,RR$,FF,TH,RPM,HP,EGT,SULF
180 'FOR I=I to 5: READ B(I): NEXT I
190 'FOR I=1 TO 9: READ C(I): NEXT I
200 'FOR I=1 TO 6: READ D(I): NEXT I
210 'PRINT #1,B(1);B(2);B(3);B(4);B(5)
220 'PRINT #1,C(1);C(2);C(3);C(4);C(5);C(6);C(7);C(8);C(9)
230 'PRINT #1,D(1);D(2);D(3);D(4);D(5);D(6)
240 CLOSE #1
250 END
251 '
252 'Page B-19 gives the program listing for T56001M.
```

```
10 OPEN "a:T56001M" FOR OUTPUT AS #1:F$-"File T56001M"
20 A$="T56-A-16":B$="MILITARY"
30 M$="AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE"
40 P$-"NAVAIREWORKFAC ALAMEDA"
50 D$="23 JUNE 1976"
60 SN$-"102138"
70 R$="Test Cell 11, single point probe in test cell exhaust stack."
71 RR$="JP-5 fuel."
80 FF-2219
90 RPM-13820
100 TH-0
110 HP-4090
120 EGT-1970
130 SULF-.02:'%
140 DATA -.07,-0.00010,.14,-0.00033,.28
150 DATA 13,23.4,.0067,.00607,.95,2,15,97,29.86
160 DATA 11.1,2.21,67.1,0,2.9,17.6
170 WRITE #1,A$,B$,F$,M$,P$,D$,SN$,R$,RR$,FF,TH,RPM,HP,EGT,SULF
180 FOR I=1 TO 5: READ B(I): NEXT I
190 FOR I=1 TO 9: READ C(I): NEXT I
200 FOR I=1 TO 6:READ D(I):NEXT I
210 PRINT#1,B(1);B(2);B(3);B(4);B(5)
220 PRINT#1,C(1);C(2);C(3);C(4);C(5);C(6);C(7);C(8);C(9)
230 PRINT#1,D(1);D(2);D(3);D(4);D(5);D(6)
240 CLOSE #1
250 END
```

APPENDIX C

Data Sheets

INDEX OF DATA SHEETS IN APPENDIX C

ENGINE	POWER SETTING	FILE
TF30-P-6C	Idle 30% Thrust 75% Thrust Normal rated Military	TF30020I TF30020B TF30020C TF30020N TF30020M
TF30-P-412A	Idle 75% Thrust Normal rated Military Afterburner zone 5	TF30021I TF30021B TF30021N TF30021M TF30021A
TF34-GE-400	Idle 75% rpm Military	TF34001I TF34001B TF34001M
TF41-A-2	Idle 8000 rpm 9000 rpm 10000 rpm 75% Maximum continuous 90% Maximum continuous Intermediate	TF41001I TF41001B TF41001C TF41001D TF41001E TF41001N TF41003M
J52-P-6B	Idle 3000 lbs Thrust 75% Thrust Normal rated Military	J52001I J52001B J52001C J52001N J52001M
J52-P-8B	Idle Manual idle 3000 lbs Thrust 75% Thrust Normal rated Military	J52010I J52010MI J52010B J52010C J52010N J52010M
J57-P-10	Idle 75% Thrust Normal rated Military	J57001I J57001B J57001N J57001M
J57-P-420	Idle 30% Thrust 75% Thrust 96% rpm Normal rated Intermediate Afterburner	J57021I J57021B J57021C J57021D J57021N J57021M J57021A

INDEX OF DATA SHEETS IN APPENDIX C (continued)

ENGINE	POWER SETTING	FILE
J65-W-5F	Idle 7450 rpm 8000 rpm 8300 rpm Military	J65001I J65001B J65001C J65001D J65001M
J79-GE-8D	Idle 75% rpm 87% rpm 90% Normal rated Military Afterburner	J79001I J79001B J79001C J79001D J79001M J79020A
J79-GE-10B	Idle 30% Thrust 85% rpm 75% Thrust Intermediate Afterburner	J79BB01I J79BB01B J79BB01C J79BB01D J79BB01M J79BB01A
J79-GE-8B	Idle 75% rpm 87% rpm 90% rpm 95% rpm Military	J79002I J79002B J79002C J79002D J79002E J79002M
J79-GE-8B	Idle 75% rpm 87% rpm 90% rpm 95% rpm Military	J79F02I J79F02B J79F02C J79F02D J79F02E J79F02M
7LM1500-PB-104A	Idle 75% Thrust Normal rated Intermediate	LM1501I LM1501B LM1501N LM1501M
LM2500	Idle 7235 rpm 7708 rpm 7814 rpm 7949 rpm 8046 rpm 8190 rpm 8210 rpm 8297 rpin 8415 rpm	LM2501I LM2501B LM2501C LM2501D LM2501E LM2501F LM2501G LM2501H LM2501J LM2501K

INDEX OF DATA SHEETS IN APPENDIX C (continued)

ENGINE	POWER SETTING	FILE
LM2500	8643 rpm 8752 rpm	LM2501L LM2501N
T53-L-11D	Ground idle Flight idle Normal rated Military Takeoff	T53001I T53001B T53001N T53001M T53001T
T56-A-16	Low speed ground idle High speed ground idle Flight idle 75% 100% Military	T56001I T56001B T56001C T56001D T56001E T56001M
T58-GE-8F	Idle High idle Approach Cruise Maximum continuous Takeoff	T58A65I T58A55B T58A56C T58A31D T58A58N T58A76M
T64-GE-6B	Idle 75% hp Normal rated Military Maximum continuous	T64001I T64001B T64001N T64001M
T64-GE-413	Idle 75% hp Normal rated Intermediate Maximum	T64031I T64031B T64031N T64031M
T64-GE-415	Idle 75% hp Normal rated Military Maximum rated power	T64051I T64051B T64051N T64051M
T64-GE-7	Idle 75% hp Normal rated Intermediate Maximum	T64002I T64002B T64002N T64002M

INDEX OF DATA SHEETS IN APPENDIX C (concluded)

ENGINE	POWER SETTING	FILE
T64-GE-7	Idle 75% Horsepower Normal rated Intermediate Maximum	T64003I T64003B T64003N T64003M T64003X
T76-G-12A	Ground start High idle Military	T76001I T76001B T76001M
T400-CP-400	Ground idle Flight idle Cruise Military	T40001I T40001B T40001C T40001M
GTC85-72	No load Load	GT8501I GT8501M
GTPC95-2	Idle 100%	GT9501I GT9501M
GTCP100-54	Idle 100%	GT1001I GT1001M
T-62T-27	Idle 100%	T6201I T6201M
WR27-1	Low flow 38 cam High flow 90 cam	WR2701B WR2701C

Α	TF30-P-6C	IDLE		File TF	300201	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T RH B H h	= 29.98 in. = 0.009949 = 0.00607		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	Measure	EXHAUST CONCE d dry	NTRATION Calculated semi- dry	wet	MISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 116.9 % 0.35 ppm 2.0 ppm ppm ppmc 42.2	sd 0.35 sd 2.0 2.0 0.1	114.6 0.35 2.0 1.9 0.1 42.5 20.39 78.65	113.8 0.34 2.0 1.9 0.1 42.2 20.25 78.12 1.27	70.58 3339.56 2.03 1.97 0.06 12.92 14.99
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at Oxides of nitrogen at				51	
F	<pre>K = 0.9873 F/A = 0.001577 Combustion efficiency Thrust = 645 pounds Engine speed Engine exhaust tempera</pre>					
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 652061 Test Cell 15, single p JP-5 fuel.	EWORKFAC ALAMED JULY 1976)A			

А	TF30-P-6C		30% THRU	ST		File	TF30020B	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RH B H h	=	71°F 39% 29.98 in. 0.009949 0.00607	Нg	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		Measure	EXH	AUST CONCE dry	NTRATION Calculated semi- dry	d wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppmC % % %	35.9 0.49 6.5 8.3	sd sd	33.6 0.49 6.6 6.4 0.2 8.4 20.33 79.18	33.4 0.48 6.5 6.3 0.2 8.4 20.21 78.70	33.2 0.48 6.5 6.3 0.2 8.3 20.05 78.08 1.39	14.87 3376.83 4.77 4.62 0.15 1.84 2.13
D	Sulfur dioxide, calc.		<u>,,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,</u>					0.40
E	Oxides of nitrogen at Oxides of nitrogen at						129	
F	<pre>K = 0.9861 F/A = 0.002182 Combustion efficiency Thrust = 3400 pounds Engine speed Engine exhaust tempera</pre>							
	EMISSION RATE pounds for a fuel flow rate o							
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	6854 9 3 4	. 19 . 97 . 68 . 73 . 33					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 652061 Test Cell 15, single pJP-5 fuel.	EWORKFA JULY	AC ALAMEI 1976	A				

А	TF30-P-6C		75% THRUST		File 1	ΓF30020C	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		RH = B = H =	= 71°F = 39% = 29.98 in. I = 0.009949 = 0.00607	Hg	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		EX Measured	HAUST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	17.2 sd 0.66 sd 13.7 sd 3.3 w	0.65	14.6 0.65 13.8 13.3 0.4 3.3	14.4 0.64 13.6 13.2 0.4 3.3 19.79 78.02 1.54	4.75 3337.67 7.38 7.14 0.23 0.54 0.62
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at Oxides of nitrogen at					212	
F	<pre>K = 0.9846 F/A = 0.002972 Combustion efficiency Thrust = 6275 pounds Engine speed Engine exhaust temper</pre>						
G	EMISSION RATE (pounds for a fuel flow rate Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	of 3560 16 11882 26 1 2	pounds per				
Н	Measurement by AIRCR Measurement at NAVAI Date of measurement Engine S/N 652061 Test Cell 15, single JP-5 fuel.	REWORKF 1 JULY	AC ALAMEDA 1976				

A	TF30-P-6C		NORMAL	RATI	ED	File	F30020N	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RI B H	i = = =	71°F 39% 29.98 in. 0.009949 0.00607	Нд	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		Measur	EXH	AUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, Chy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	11.2 0.78 21.8	sd sd	8.5 0.77 22.0 21.3 0.7 5.2 19.94 79.28	8.4 0.77 21.9 21.2 0.7 5.2 19.82 78.80	8.4 0.76 21.7 21.0 0.7 5.1 19.61 77.98 1.64	2.31 3314.95 9.86 9.55 0.31 0.70 0.81
D	Sulfur dioxide, calc.	_						0.40
E	Oxides of nitrogen at Oxides of nitrogen at						291	
F	<pre>K = 0.9836 F/A = 0.003535 Combustion efficiency Thrust = 8395 pounds Engine speed Engine exhaust tempera</pre>							
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	11. 16011. 47. 3.	pounds 18 20					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 652061 Test Cell 15, single p JP-5 fuel.	EWORKFA JULY 1	C ALAME .976	AC				

Α	TF30-P-6C	MILITARY		File TF30020M	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T RH B H h	= 29.98 in. Hg = 0.009949	$m = 13.$ $n = 23.$ $\eta = 0.$.4
	CONSTITUENT		EXHAUST CONCENTR d Cal	ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 10.1 s % 0.97 s ppm 36.8 s ppm ppm ppm ppm ppmC 8.3 v % % %	30 0.96 37.2 36.0 1.2 8.5	7.2 7.1 0.96 0.95 37.0 36.5 35.8 35.4 1.2 1.2 8.4 8.3 19.57 19.33 78.87 77.92 1.80	1.56 3287.67 13.28 12.86 0.42 0.91 1.05
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at Oxides of nitrogen at			405	
F	<pre>K = 0.9820 F/A = 0.004430 Combustion efficiency Thrust = 11025 pounds Engine speed Engine exhaust tempera</pre>				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 652061 Test Cell 15, single p JP-5 fuel.	EWORKFAC ALAMEDA JULY 1976	A		

Α	TF30-P-412A	IC	DLE	File TF30021I			
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		RH = B = H =	= 93°F = 22% = 29.95 in. Hg = 0.011470 = 0.00607	77	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT			HAUST CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	64.7 sd 0.25 sd 2.2 sd 71.1 w	0.25	62.5 0.25 2.2 2.1 0.1 71.6 20.52 78.62	62.0 0.24 2.2 2.1 0.1 71.1 20.37 78.04 1.33	55.51 3440.59 3.22 3.12 0.10 31.42 36.46
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at Oxides of nitrogen at					69	
F	K = 0.9867 F/A = 0.001094 Combustion efficiency Thrust = 595 pounds Engine speed = 10278 Turbine inlet tempera	rpm					-
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		ounds per 1 97 84 96 90 94				
н	Measurement by AIRCRA Measurement at NAVAIA Date of measurement 2 Engine S/N 679326 Test Cell 16, single p JP-5 fuel.	REWORKFAC 24 JUNE 1	ALAMEDA 976				

A	TF30-P-412A	75% THRUST	File	TF30021B		
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 93°F RH = 22% B = 29.95 in h = 0.01147 h _{sd} = 0.00607	$ \begin{array}{c c} n = \\ \eta = \\ 0 \end{array} $	13.0 23.4 0.95		
	CONSTITUENT		T CONCENTRATION Calculate dry semi- dry	d wet	EMISSION INDEX	
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 9.6 sd % 0.46 sd ppm 13.6 sd ppm ppm ppm ppmC 6.2 w	7.2	7.1 0.45 13.5 13.1 0.4 6.2 20.06 77.98 1.51	3.43 3413.00 10.74 10.40 0.34 1.48 1.72	
D	Sulfur dioxide, calc. 0.40					
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 275 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	<pre>K = 0.9849 F/A = 0.002027 Combustion efficiency = 99.77% Thrust = 7070 pounds Engine speed = 13441 rpm Turbine inlet temperature = 1570°F</pre>					
	EMISSION RATE (pounds of for a fuel flow rate of					
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	46.19				
Н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC ALAMEDA Date of measurement 24 JUNE 1976 Engine S/N 679326 Test Cell 16, single point probe, 85 feet behind engine. JP-5 fuel.					

A	TF30-P-412A	NORMAL RATED		File TF30021N	, , , , , , , , , , , , , , , , , , , 	
8	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 93°F RH = 22% B = 29.95 in. h = 0.011470 h _{sd} = 0.00607		$m = 13.0 n = 23.4 \eta = 0.95$		
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX	
С	Oxides of nitrogen pr Nitric oxide pr Nitrogen dioxide pr	0.56 sd m 25.0 sd m m mC 6.2 w	0.56 25.3 24.5 0.8 6.3	4.2 4.1 0.55 0.55 25.1 24.9 24.3 24.1 0.8 0.8 6.3 6.2 20.11 19.91 78.73 77.94 1.60	162 3371.58 16.02 15.52 0.51 1.20 1.39	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			431		
F	<pre>K = 0.9840 F/A = 0.002497 Combustion efficiency = 99.84% Thrust = 9550 pounds Engine speed = 14105 rpm Turbine inlet temperature = 1806°F</pre>					
G	Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄	•				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 24 of Engine S/N 679326 Test Cell 16, single poin JP-5 fuel.	RKFAC ALAMEDA UNE 1976		ne .		

A	TF30-P-412A	YRATILIM	File	TF30021M		
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 93°F RH = 22% B = 29.95 i h = 0.0114 h _{sd} = 0.0060	n. Hg	13.0 23.4 0.95		
	CONSTITUENT	EXHAU Measured	ST CONCENTRATION Calculated dry semi- dry	d wet	EMISSION INDEX	
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	opm 6.7 sd 7 sd 7 sd 7 sd 9 sd 9 sd 9 sd 9 sd	4.1 4.1 0.63 0.63 35.6 35.3 34.4 34.2 1.1 1.1 4.7 4.6 20.13 20.01 79.23 78.75	4.0 0.62 35.0 33.9 1.1 4.6	1.38 3347.82 19.60 18.98 0.62 0.77 0.90	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 544 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	<pre>K = 0.9834 F/A = 0.002874 Combustion efficiency = 99.89% Thrust = 10900 pounds Engine speed = 14505 rpm Turbine inlet temperature = 1958°F</pre>					
	EMISSION RATE (pounds of for a fuel flow rate of	-				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	9.71 23602.14 138.20 5.46 6.34 2.82				
н	Measurement by AIRCRAFT Measurement at NAVAIREM Date of measurement 24 Engine S/N 679326 Test Cell 16, single poi JP-5 fuel.	JORKFAC ALAMEDA JUNE 1976				

Α	TF30-P-412A	AFTERBURNER ZONE 5	File TF30021A			
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 93°F RH = 22% B = 29.95 in. H = 0.011470 h _{sd} = 0.00607	m = 13.0 n = 23.4 η = 0.95			
	CONSTITUENT	EXHAUST CONCEN	TRATION EMISSIC INDEX semi- wet dry			
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	4.57 sd 4.55 64.4 sd 65.4 63.4 2.1	240.1 229.5 4.52 4.32 3188.5 65.0 62.1 4.7 63.0 60.2 4.6 2.1 2.0 0.1 9.2 8.8 0.2 14.71 14.06 80.14 76.59 5.00	56 79 54 _5 20		
D	Sulfur dioxide, calc.		0.4	•0		
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or		162			
F	<pre>K = 0.9500 F/A = 0.021252 Combustion efficiency = 99.73% Thrust = 18850 pounds Engine speed = 14460 rpm Turbine inlet temperature = 1970°F</pre>					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 47800 pounds per hour Carbon monoxide 514.91 Carbon dioxide 152413.20 Oxides of nitrogen 229.04 Hydrocarbons, CHy/x 9.75 Hydrocarbons, CH ₄ 11.31 Sulfur dioxide 19.12					
Н	Measurement by AIRCRAFT EMMeasurement at NAVAIREWORD Date of measurement 24 JUMEngine S/N 679326 Test Cell 16, single point JP-5 fuel.	KFAC ALAMEDA NE 1976				

A	TF34-GE-400	IDLE		File	TF34001I	
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00504$ $M' = 0.28$	T = 59°F RH = 64% B = 29.92 i h = 0.0107 h = 0.0060	23	n =	13.0 23.4 0.95	
	CONSTITUENT		ST CONCEN' C	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	pm 211.9 sd % 0.41 sd pm 2.0 sd pm pm pm % % % %	178.9 0.41 2.0 2.0 0.1 59.7 20.42 79.15	177.9 0.40 2.0 1.9 0.1 59.4 20.30 78.67	176.4 0.40 2.0 1.9 0.1 58.9 20.14 78.04 1.41	90.98 3248.66 1.69 1.63 0.05 14.99 17.40
D	Sulfur dioxide, calc. 0.40					
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				44	
F	K = 0.9859 F/A = 0.001899 Combustion efficiency = 96.39% Thrust = 950 pounds Engine speed = 11600 rpm					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 485 pounds per hour Carbon monoxide 44.13 Carbon dioxide 1575.60 Oxides of nitrogen 0.82 Hydrocarbons, CHy/x 7.27 Hydrocarbons, CH ₄ 8.44 Sulfur dioxide 0.19					
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAL AIR STATION, NORTH ISLAND Date of measurement 13,14 NOVEMBER 1975 Engine S/N 202110 TF34 Test Cell, single point probe in test cell exhaust. JP-5 fuel. The thrust was not measured. The listed value is typical for this engine.					

A	TF34-GE-400	75% rpm		File TF340011	3	
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00504$ $M' = 0.28$	T = 59°F RH = 64% B = 29.92 in h = 0.01072 h _{sd} = 0.00607	3	$m = 13.0$ $n = 23.4$ $\eta = 0.95$;	
	CONSTITUENT		T CONCENTE Cal	RATION lculated semi- wet dry	EMISSION INDEX	
С	Carbon monoxide ppor Carbon dioxide % Oxides of nitrogen ppor Nitric oxide ppor Nitrogen dioxide ppor Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen % Nitrogen % Water %	0.44 sd n 4.2 sd n	68.3 0.44 4.2 4.1 0.1 10.9 20.39 79.16	67.9 67.3 0.43 4.2 4.2 4.1 4.0 0.1 10.8 10.7 20.27 20.10 78.69 78.04 1.42	3.42 3.32 0.11 2.63 3.06	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			89		
F	<pre>K = 0.9858 F/A = 0.001964 Combustion efficiency = 98.96% Thrust = 960 pounds Engine speed = 12000 rpm</pre>					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 460 pounds per hour Carbon monoxide 15.44 Carbon dioxide 1550.06 Oxides of nitrogen 1.58 Hydrocarbons, CHy/x 1.21 Hydrocarbons, CH ₄ 1.41 Sulfur dioxide 0.18					
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAL AIR STATION, NORTH ISLAND Date of measurement 13,14 NOVEMBER 1975 Engine S/N 202110 TF34 Test Cell, single point probe in test cell exhaust. JP-5 fuel. The thrust was not measured. The listed value is typical for this engine.					

A	TF34-GE-400	MILITARY	1	File TF34001M		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00504$ $M' = 0.28$	RH = 6 B = 2 h =	9°F 64% 29.92 in. Hg 0.010723 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$		
	CONSTITUENT	Measur	EXHAUST CON- ed dry	Calculated	EMISSION INDEX	
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 60.2 % 0.81 ppm 17.3 ppm ppm ppmc 3.0	sd 0.80 sd 17.5 16.9 0.6	0 0.80 0.79 17.4 17.2 16.8 16.6 0.5 0.5 3.0 3.0	5.95 3304.70 7.51 7.28 0.24 0.39 0.46	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	K = 0.9826 F/A = 0.003682 Combustion efficiency = 99.82% Thrust = 9275 pounds Engine speed = 16500 rpm					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 3800 pounds per hour Carbon monoxide 22.62 Carbon dioxide 12557.87 Oxides of nitrogen 28.56 Hydrocarbons, CHy/x 1.50 Hydrocarbons, CH ₄ 1.74 Sulfur dioxide 1.52					
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAL AIR STATION, NORTH ISLAND Date of measurement 13,14 NOVEMBER 1975 Engine S/N 202110 TF34 Test Cell, single point probe in test cell exhaust. JP-5 fuel. The thrust was not measured. The listed value is typical for this engine.					

А	TF41-A-2	IDLE		File TF410011	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	RH = B = H =	93°F 22% 29.90 in. Hg 0.011490 0.00607	$m = 13.$ $n = 23.$ $\eta = 0.$. 4
	CONSTITUENT	EXH Measured	dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.55 sd 2.9 sd	0.55 2.9 2.8 0.1 291.8 29	4.8 262.1 0.54 0.54 2.9 2.9 2.8 2.8 0.1 0.1 0.0 287.1 0.10 19.90 8.72 77.92 1.61	94.80 3050.49 1.71 1.66 0.05 51.26 59.48
D	Sulfur dioxide, calc.			-	0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			49	
F	<pre>K = 0.9839 F/A = 0.002711 Combustion efficiency = 92 Thrust = 595 pounds Engine speed = 7100 rpm Engine exhaust temperature</pre>				
G					
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 24 JU Engine S/N 141917 Test Cell 15, single point JP-5 fuel.	KFAC ALAMEDA INE 1976		exhaust plane	

Α	TF41-A-2		8000 RPM		File	TF41001B	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		RH = B = H =	= 93°F = 22% = 29.90 in. = 0.011490 = 0.00607		$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT	•		HAUST CONCE	NTRATION Calculated semi- dry	l wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppmC % % %	236.5 sd 0.53 sd 3.6 sd 201.8 w	0.53	234.0 0.52 3.6 3.5 0.1 203.8 20.13 78.72	231.7 0.52 3.6 3.5 0.1 201.8 19.93 77.93 1.59	88.70 3112.35 2.25 2.18 0.07 38.14 44.26
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 1 Oxides of nitrogen at 1					63	
F	<pre>K = 0.9841 F/A = 0.002561 Combustion efficiency = Thrust = 820 pounds Engine speed = 8000 rpr Engine exhaust temperate</pre>	n					
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	109 3828 2 46 54	pounds per .10 .19 .77				
Н	Measurement by AZRCRAN Measurement at NAVAIRN Date of measurement 24 Engine S/N 141917 Test Cell 15, single po JP-5 fuel.	EWORKFA JUNE	AC ALAMEDA 1976			ıst plane	

Α	TF41-A-2	9000 RPM		File T	F41001C	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	RH B H	= 93°F = 22% = 29.90 in. = 0.011490 = 0.00607	Нд	$m = 13.6$ $n = 23.6$ $\eta = 0.6$	4
	CONSTITUENT	EX Measured	HAUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen	om 166.3 sd 0.56 sd om 4.7 sd om om omC 124.5 w	0.56	163.8 0.55 4.7 4.6 0.1 125.8 20.10 78.73	162.1 0.55 4.7 4.5 0.1 124.5 19.90 77.93 1.61	60.41 3200.23 2.86 2.77 0.09 22.90 26.58
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				80	
F	<pre>K = 0.9839 F/A = 0.002631 Combustion efficiency = 9 Thrust = 1210 pounds Engine speed = 9020 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide					
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 24 C Engine S/N 141917 Test Cell 15, single poin JP-5 fuel.	ORKFAC ALAMEDA JUNE 1976			st plane.	

Α	TF41-A-2	10000 RPM		File	TF41001D	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	RH B	RH = 22% B = 29.90 in. Hg H = 0.011490) 4 95
	CONSTITUENT		KHAUST CONCE dry	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 121.4 sc % 0.59 sc ppm 6.2 sc ppm ppm ppm ppmC 73.0 w	0.59	118.8 0.58 6.2 6.0 0.2 73.8 20.06 78.74	117.6 0.58 6.2 6.0 0.2 73.0 19.86 77.92 1.63	42.30 3253.88 3.64 3.53 0.11 12.95 15.04
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3				101	
F	<pre>K = 0.9837 F/A = 0.002726 Combustion efficiency = Thrust = 1800 pounds Engine speed = 10029 rp Engine exhaust temperat</pre>	m	· · · · · · · · · · · · · · · · · · ·		·	
G	Oxides of nitrogen Hydrocarbons, CH _{Y/X}	79.53 6117.30 6.84				
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 24 Engine S/N 141917 Test Cell 15, single po JP-5 fuel.	WORKFAC ALAMEDA JUNE 1976			ist plane.	

Α	TF41-A-2	75% MAX	IMUN	CONTINUOUS	S File	TF41001E	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	В	H = = =	93°F 22% 29.90 in. H 0.011490 0.00607	g	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT	Measur	EXH	AUST CONCENT Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp	om om omC 6.4	sd sd	9.6 0.92 45.2 43.8 1.4 6.5	9.5 0.92 44.9 43.5 1.4 6.5	9.4 0.91 44.3 42.9 1.4 6.4 19.36 77.81 1.92	2.17 3292.14 16.85 16.32 0.53 0.73 0.85
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%					500	
F	<pre>K = 0.9808 F/A = 0.004242 Combustion efficiency = 9 Thrust = 9550 pounds Engine speed = 12056 rpm Engine exhaust temperature</pre>						
	EMISSION RATE (pounds of for a fuel flow rate of 6						 .
G	Carbon monoxide Carbon dioxide 19 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide						
Н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 24 3 Engine S/N 141917 Test Cell 15, single poin JP-5 fuel.	ORKFAC ALAME TUNE 1976	DA			st plane	

А	TF41-A-2	90% MAXIMUM CONTINUOUS	File TF41001N	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 93°F RH = 22% B = 29.90 in. Hg h = 0.011490 h _{sd} = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONCENT Measured Ca dry	RATION lculated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	11.0 sd 8.0 1.04 sd 1.03 67.5 sd 68.2 66.1 2.2 8.2 w 8.4 19.59 79.37	8.0 7.9 1.03 1.01 67.8 66.9 65.7 64.7 2.1 2.1 8.3 8.2 19.47 19.19 78.89 77.77 2.01	1.62 3280.21 22.67 21.95 0.71 0.84 0.97
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% ox Oxides of nitrogen at 3% ox	ygen, calc.(ppm wet) ygen, meas.(ppm wet)	684	
F	<pre>K = 0.9799 F/A = 0.004759 Combustion efficiency = 99. Thrust = 11500 pounds Engine speed = 12460 rpm Engine exhaust temperature</pre>			
	EMISSION RATE (pounds of co for a fuel flow rate of 748			
G	Carbon dioxide 2453 Oxides of nitrogen 16 Hydrocarbons, $CH_{y/x}$			
Н	Measurement by AIRCRAFT EN Measurement at NAVAIREWORK Date of measurement 24 JUN Engine S/N 141917 Test Cell 15, single point JP-5 fuel.	FAC ALAMEDA E 1976		

А	TF41-A-2	INTERMEDIATE	File TF41003M					
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 69°F RH = 59% B = 29.93 H = 0.014 h _{sd} = 0.006	107	. 4				
	CONSTITUENT		NCENTRATION Calculated y semi- wet dry	EMISSION INDEX				
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen	1.19 sd 1. om 76.8 sd 77. om 75. om 2. omC 7.2 w 7. d 19.0 sd 19.	2 74.7 73.4 4 2.4 2.4	1.64 3267.64 22.46 21.75 0.71 0.64 0.74				
D	Sulfur dioxide, calc.			0.40				
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 671 Oxides of nitrogen at 3% oxygen, meas.(ppm wet) 594							
F	<pre>K = 0.9761 F/A = 0.005464 Combustion efficiency = Thrust = 14000 pounds Engine speed Engine exhaust temperatu</pre>							
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 8940 pounds per hour Carbon monoxide 14.63 Carbon dioxide 29212.69 Oxides of nitrogen 200.76 Hydrocarbons, CHy/x 5.73 Hydrocarbons, CH ₄ 6.65 Sulfur dioxide 3.58							
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 8 J Engine S/N 141369 Test Cell 15, single poi JP-5 fuel.	DRKFAC ALAMEDA JLY 1976						

Α	J52-P-6B		DLE			Fi	le J52001I	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RI B H h	=	0.012130		$m = 13.6$ $n = 23.6$ $\eta = 0.6$	4
	CONSTITUENT		Measure	EXH	AUST CONCE	NTRATION Calculat semi- dry	ced	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % % %	195.0 0.46 2.8 106.8 20.3	sd sd w	193.7 0.46 2.8 2.7 0.1 108.5 20.35 79.17	192.6 0.45 2.8 2.7 0.1 107.9 20.23 78.69	0.45 2.8 2.7 0.1 106.8 3 20.03	86.37 3196.13 2.07 2.01 0.07 23.88 27.71
D	Sulfur dioxide, calc.			·				0.40
E	Oxides of nitrogen at Oxides of nitrogen at						54 59	
F	<pre>K = 0.9841 F/A = 0.002165 Combustion efficiency Thrust = 512 pounds Engine speed = 6926 rp Engine exhaust tempera</pre>	m						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	f 714 p 61. 2282. 1. 17. 19.	67 03 48 05					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 649773 Test Cell 15, single p JP-5 fuel.	EWORKFA 7 JUNE	C ALAMEI 1976	DA			naust plane.	

А	J52-P-6B	3000 LBS TH	RUST	File J52001B	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	RH :	= 70°F = 49% = 29.84 in. H = 0.012150 = 0.00607	$m = 13$ $n = 23$ $\eta = 0$	3.4
	CONSTITUENT		HAUST CONCENT Ca dry	RATION lculated semi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH4 Oxygen	pm 52.9 sd % 0.65 sd pm 7.2 sd pm pm pm pm % 20.1 sd %	0.64 7.3 7.0 0.2 5.1	50.3 49.7 0.64 0.63 7.2 7.1 7.0 6.9 0.2 0.2 5.1 5.0 19.99 19.76 78.76 77.86	3.91 3.79 0.12 0.82 0.96
_	Water	%		1.74	
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			108 119	
F	<pre>K = 0.9826 F/A = 0.002943 Combustion efficiency = Thrust = 3034 pounds Engine speed = 9770 rpm Engine exhaust temperatu</pre>				
	EMISSION RATE (pounds of for a fuel flow rate of				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	38.13 7638.86 9.01 1.89 2.20 0.92			
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 17 Engine S/N 649773 Test Cell 15, single poi JP-5 fuel.	ORKFAC ALAMEDA JUNE 1976			e .

Α	J52-P-6B	7	'5% THRU	JST		File J	152001C	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RF B H h	= = =	70°F 49% 29.84 in. H 0.012150 0.00607	Ig	$m = 13.0$ $n = 23.0$ $\eta = 0.0$	4
	CONSTITUENT		Measure	EXH	AUST CONCENT Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppmC % % %	28.3 0.90 15.0 5.5 19.9	sd sd	25.6 0.89 15.2 14.7 0.5 5.6 19.78 79.33	25.4 0.89 15.1 14.6 0.5 5.6 19.66 78.85	25.1 0.88 14.9 14.4 0.5 5.5	6.00 3290.12 5.84 5.65 0.18 0.65 0.75
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3						171 202	
F	<pre>K = 0.9804 F/A = 0.004108 Combustion efficiency = Thrust = 5446 pounds Engine speed = 10641 rg Engine exhaust temperate</pre>	pm						
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		pounds 1 85 82 22 58 00	-				
н	Measurement by AIRCRAI Measurement at NAVAIRI Date of measurement 1 Engine S/N 649773 Test Cell 15, single po JP-5 fuel.	EWORKFA 7 JUNE	C ALAMEI 1976	AC			st plane.	

A	J52-P-6B	NORMAL RATED	File J52001N					
В	J =0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 70°F RH = 49% B = 29.84 in H = 0.012150 h _{sd} = 0.00607		. 4				
	CONSTITUENT	EXHAUST CONC Measured dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX				
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.04 sd 1.03 22.3 sd 22.5 21.8 0.7	1.03 1.01 22.4 22.1 21.7 21.4 0.7 0.7 5.6 5.5 19.47 19.18	4.53 3276.40 7.48 7.24 0.24 0.56 0.65				
D	Sulfur dioxide, calc.			0.40				
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 224 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)							
F	<pre>K = 0.9792 F/A = 0.004765 Combustion efficiency = 99 Thrust = 7202 pounds Engine speed = 11177 rpm Engine exhaust temperature</pre>							
G								
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 17 JU Engine S/N 649773 Test Cell 15, single point JP-5 fuel.	KFAC ALAMEDA NE 1976						

A	J52-P-6B		MILITARY			File	J52001M	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RF B H h	= = =	70°F 49% 29.84 in. 0.012150 0.00607		$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUEN'1		Measure	EXH	AUST CONCE	NTRATION Calculated semi- dry	l wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	19.2 1.13 29.2 3.5	sd sd	16.2 1.12 29.5 28.6 0.9 3.6 19.47	16.1 1.11 29.3 28.4 0.9 3.6 19.35 78.93	15.8 1.10 28.9 28.0 0.9 3.5 19.05 77.69 2.16	3.01 3271.29 9.00 8.72 0.28 0.33 0.33
D	Sulfur dioxide, calc.							0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at						273 333	
F	<pre>K = 0.9784 F/A = 0.005183 Combustion efficiency Thrust = 8275 pounds Engine speed = 11500 Engine exhaust temper</pre>	rpm						
G	EMISSION RATE (pounds for a fuel flow rate Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	0f 6328 19 20700 56 2 2	pounds p					
н	Measurement by AIRCR Measurement at NAVAI Date of measurement Engine S/N 649773 Test Cell 15, single JP-5 fuel.	REWORKFA 17 JUNE	AC ALAMEI 1976	DΑ			st plane	

A	J52-P-8B	IDLE	File J52010I	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 73°F RH = 44% B = 29.93 in. 1 h = 0.012091 h = 0.00607		
	CONSTITUENT	Measured	CONCENTRATION Calculated dry semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.47 sd 2.5 sd 2.194.6 w 19 20.2 sd 2	7.5 146.6 145.2 0.47 0.46 0.46 2.5 2.5 2.5 2.4 2.4 2.4 0.1 0.1 0.1 7.7 196.6 194.6 0.34 20.22 20.02 9.17 78.69 77.91 1.59	63.78 3166.50 1.79 1.74 0.06 42.20 48.96
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or			
F	<pre>K = 0.9841 F/A = 0.002233 Combustion efficiency = 94 Thrust = 475 pounds Engine speed = 6625 rpm Engine exhaust temperature</pre>			
G	Carbon dioxide 219 Oxides of nitrogen Hydrocarbons, $CH_{y/x}$)	
Н	Measurement by AIRCRAFT EN Measurement at NAVAIREWORK Date of measurement 29 JUN Engine S/N 661421 Test Cell 15, single point JP-5 fuel.	KFAC ALAMEDA NE 1976		

A	J52-P-8B	MANUAL IDLE	·	File J52010MI	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 73°F RH = 44% B = 29.93 i h = 0.0120 h _{sd} = 0.0060	91	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		IST CONCENT Ca dry	TRATION alculated semi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 139.1 sd 0.40 sd ppm 2.2 sd ppm ppm ppm 221.7 w	137.5 0.40 2.2 2.2 0.1 225.1 20.44 79.15	136.7 135.4 0.39 0.39 2.2 2.2 2.1 2.1 0.1 0.1 223.8 221.7 20.32 20.13 78.67 77.94 1.53	1.84 1.79 0.06 56.16 65.16
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3 Oxides of nitrogen at 3			48	
F	<pre>K = 0.9847 F/A = 0.001911 Combustion efficiency = Engine speed = 6350 rpm</pre>				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 29 Engine S/N 661421 Test Cell 15, single po JP-5 fuel.	WORKFAC ALAMEDA JUNE 1976			e.

Α	J52-P-8B		3000 LB	S THRU	ST	File	J52010B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28		RH = B =	73°F 44% 29.93 0.0120	091	m = η = η = η = η = η = η = η = η = η =		
	CONSTITUENT		Measu		JST CONCEN C. dry	IRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC		8 sd sd w	33.6 0.67 12.3 11.9 0.4 11.1 20.07 79.25	33.4 0.67 12.3 11.9 0.4 11.0 19.95 78.77	33.0 0.66 12.1 11.7 0.4 10.9 19.72 77.85 1.76	10.54 3319.15 6.34 6.14 0.20 1.72 1.99
D	Sulfur dioxide, calc.				······································			0.40
E	Oxides of nitrogen at Oxides of nitrogen at						177 170	
F	K = 0.9824 F/A = 0.003079 Combustion efficiency Thrust = 3005 pounds Engine speed = 9866 rg Engine exhaust tempera	pm						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide	of 2300 24 7634	pounds 23 04					
	Oxides of nitrogen Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	3 4	.58 .94 .58					
н	Measurement by AIRCRA Measurement at NAVAII Date of measurement 2 Engine S/N 661421 Test Cell 15, single p JP-5 fuel.	REWORKF 29 JUNE	AC ALAM 1976	EDA			st plane	

A	J52-P-8B	75% THRU	ST	File J52010C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		EXHAUST CONC d dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	pm 17.0 % 0.99 pm 28.6 pm pm pmC 5.4 % 19.5 %	sd 0.98 sd 28.9 28.0 0.9 w 5.5	0.98 0.96 28.7 28.3 27.8 27.4 0.9 0.9 5.5 5.4 19.54 19.26	10.10 9.78 0.32 0.58 0.67
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			301 294	
F	K = 0.9797 F/A = 0.004526 Combustion efficiency = Thrust = 5900 pounds Engine speed = 10869 rpm Engine exhaust temperatu				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide 1 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4	4320 pounds p 12.98 4187.45 43.64 2.50 2.90			
н	Sulfur dioxide Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 29 Engine S/N 661421 Test Cell 15, single poi JP-5 fuel.	ORKFAC ALAMED JUNE 1976	A		e .

A	J52-P-8B	NORMAL RATED		File J52010N			
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	T = 73°F RH = 44% B = 29.93 in h = 0.012093 h _{sd} = 0.00607		$m = 13.0$ $n = 23.4$ $\eta = 0.95$			
	CONSTITUENT		CONCE dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX		
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.23 sd 42.9 sd	5.1 1.22 43.4 42.0 1.4 7.1 19.33 79.44	1.21 1.19 43.1 42.4 41.8 41.1 1.4 1.3 7.0 6.9	0.87 3266.06 12.13 11.75 0.38 0.59 0.69		
D	Sulfur dioxide, calc.				0.40		
Ε	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 372 Oxides of nitrogen at 3% oxygen, meas.(ppm wet) 408						
F	<pre>K = 0.9777 F/A = 0.005649 Combustion efficiency = 99 Thrust = 8030 pounds Engine speed = 11478 rpm Engine exhaust temperature</pre>						
G	EMISSION RATE (pounds of c for a fuel flow rate of 61 Carbon monoxide Carbon dioxide 200 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	30 pounds per hour 5.35 20.96 74.36					
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 29 JU Engine S/N 661421 Test Cell 15, single point JP-5 fuel.	KFAC ALAMEDA NE 1976					

A	J52-P-8B	MILIT	ARY		File J	52010M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T RH B h	= 73°F = 44% = 29.93 i = 0.0120 = 0.0060	91	$ \begin{array}{r} m = 1 \\ n = 2 \\ \eta = 3 \end{array} $	23.4	
	CONSTITUENT	Mea	EXHAU asured	ST CONCENT Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	% 1 ppm 52 ppm ppm ppm ppm ppmC 12	3.1 sd 1.40 sd 2.7 sd 2.3 w	4.8 1.39 53.3 51.6 1.7 12.6 19.10 79.50	4.7 1.38 53.0 51.3 1.7 12.5 18.99 79.02	4.6 1.25 52.0 50.4 1.6 12.3 18.65 77.61 2.38	0.71 3254.59 13.05 12.64 0.41 0.93 1.08
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 3					406 426	
F	K = 0.9762 F/A = 0.006449 Combustion efficiency = Thrust = 9200 pounds Engine speed = 11906 rp Engine exhaust temperat	om	₊° F				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	5.22 23986.31 96.16					
н	Measurement by AIRCRAI Measurement at NAVAIRI Date of measurement 29 Engine S/N 661421 Test Cell 15, single po JP-5 fuel.	EWORKFAC AI JUNE 1976	AMEDA			st plane.	AFSO 00-20-1007

A	J57-P-10	IDLE		File	J57001i	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 63°F RH = 67% B = 29.97 in h = 0.01290 h = 0.00600	33	m - η - η - η		
	CONSTITUENT		ST CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
U	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH4	pm 237.4 sd % 0.55 sd pm 3.3 sd pm pm pm % % % %	0.55 3.3 3.2 0.1	234.9 0.54 3.3 3.2 0.1 570.9 20.11 78.72	232.2 0.54 3.3 3.2 0.1 564.3 19.87 77.81 1.75	80.52 2920.94 1.87 1.81 0.06 96.60 112.10
D	Sulfur dioxide, calc.					0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				55	
F	K = 0.9825 F/A = 0.002831 Combustion efficiency = Thrust = 555 pounds Engine speed = 6009 rpm Engine exhaust temperatu					
	EMISSION RATE (pounds of for a fuel flow rate of					
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	88.57 3213.04 2.05 106.26 123.31 0.44				
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 9 J Engine S/N 606306 Test Cell 15, single poi JP-5 fuel.	ORKFAC ALAMEDA ULY 1976			st plane	

A	J57-P-10	75% THE	RUST		File J	57001B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	RH = B =	29.97 in 0.01293		m = 1 n = 2 η =		
	CONSTITUENT	Measu		CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water			15.4 1.00 21.6 20.9 0.7 7.4 19.63 79.36	15.3 1.00 21.5 20.8 0.7 7.3 19.51 78.88	15.1 0.98 21.2 20.5 0.7 7.2 19.21 77.68 2.13	3.21 3281.02 7.40 7.17 0.23 0.76 0.88
D	Sulfur dioxide, calc.		*				0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at					219	
F	K = 0.9787 F/A = 0.004621 Combustion efficiency Thrust = 7040 pounds Engine speed = 8958 rp Engine exhaust tempera	n					
	EMISSION RATE (pounds for a fuel flow rate o						
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	41.97					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 9 Engine S/N 606306 Test Cell 15, single polyp-5 fuel.	EWORKFAC ALAM JULY 1976	EDA			st plane	

A	J57-P-10	NORMAL RATED		File J57001N	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 63°F RH = 67% B = 29.97 in h = 0.01293 h _{sd} = 0.00607	. Нg	m = 13.0 m = 23.4 m = 0.95	
	CONSTITUENT		T CONCENTRATION Calculory sem	ated i- wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 13.0 sd 1.16 sd 20pm 30.0 sd 20pm 20pm 20pm 20pm 20pm 20pm 20pm 20pm	9.9 9.1 1.15 1.3 30.3 30.3 29.4 29.3 1.0 1.0 11.3 11.3 19.43 19.7 79.42 78.5	14 1.13 1 29.6 2 28.7 0 0.9 2 11.0	1.79 3268.55 9.00 8.72 0.28 1.00 1.16
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			272 235	
F	K = 0.9774 F/A = 0.005325 Combustion efficiency = Thrust = 9050 pounds Engine speed = 9267 rpm Engine exhaust temperatu				
G	Oxides of nitrogen Hydrocarbons, CH _{Y/X}				
	Hydrocarbons, CH₄ Sulfur dioxide	8.44 2.90			
н	Measurement by AIRCRAFT Measurement at NAVAIREM Date of measurement 9 J Engine S/N 606306 Test Cell 15, single poi JP-5 fuel.	ORKFAC ALAMEDA ULLY 1976		xhaust plane.	

Α	J57-P-10	MI	LITARY	<u>, </u>		File J	57001M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	B h	H = 6 = 2	3°F 7% 9.97 in 0.01293 0.00607	3	m = 1 n = 2 η =		
	CONSTITUENT	î	1 easur		T CONCEN' C. dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	10.2 1.26 37.6 10.3 19.0	sd sd w	7.0 1.25 38.0 36.8 1.2 10.5	7.0 1.24 37.8 36.6 1.2 10.5	6.8 1.22 37.1 36.0 1.2 10.3 18.84 77.59 2.34	1.16 3262.61 10.37 10.04 0.33 0.86 1.00
0	Sulfur dioxide, calc.							0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at						316 292	
F	K = 0.9766 F/A = 0.005792 Combustion efficiency Thrust = 10310 pounds Engine speed = 9468 rp Engine exhaust tempera	om	043°F					
	EMISSION RATE (pounds for a fuel flow rate of						<u> </u>	
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	9.74 27308.0 86.73 7.23 8.44 3.33	7 8 3 0					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 9 Engine S/N 606306 Test Cell 15, single p JP-5 fuel.	EWORKFAC JULY 19	ALAME 76	DA			st plane.	

Α	J57-P-420	IDLE			File	J57021I		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	T RH B H h	=	58°F 90% 30.02 in. 0.014564 0.00607	Нд	$m = 13.$ $n = 23.$ $\eta = 0.$	4	
	CONSTITUENT	Measure	EXH	AUST CONCE	NTRATION Calculated semi- dry	d wet	EMISSION INDEX	
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x pp Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.56 n 2.7 n	sd	236.0 0.56 2.7 2.6 0.1 452.9 20.21 79.20	234.6 0.55 2.7 2.6 0.1 450.1 20.09 78.72	231.5 0.54 2.7 2.6 0.1 444.2 19.83 77.69 1.91	80.74 2985.39 1.53 1.48 0.05 76.46 88.73	
D	Sulfur dioxide, calc.						0.40	
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 43 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)							
F	<pre>K = 0.9809 F/A = 0.002821 Combustion efficiency = 9 Thrust = 393 pounds Engine speed = 6794 rpm Engine exhaust temperatur</pre>							
	EMISSION RATE (pounds of for a fuel flow rate of l							
G	Carbon dioxide 3 Oxides of nitrogen Hydrocarbons, CH _{Y/X}	106.74 946.69 2.03 101.08 117.29 0.53						
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 16 J Engine S/N 634012 Test Cell 20, single poin JP-5 fuel.	RKFAC NORTH ANUARY 1974	ISL	AND		ust plane		

Α	J57-P-420	30% THRUST		File J57021B	
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	RH =		$m = 13.0$ $n = 23.0$ $\eta = 0.0$	4
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen	om om omC 27.6 w	0.64 8.3 8.0 0.3 28.2 2	5.1 44.5 0.64 0.63 8.2 8.1 8.0 7.9 0.3 0.3 8.0 27.6 9.99 19.72 8.76 77.67 1.98	14.83 3310.23 4.45 4.31 0.14 4.54 5.27
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			118	
F	<pre>K = 0.9802 F/A = 0.002952 Combustion efficiency = 9 Thrust = 3577 pounds Engine speed = 8407 rpm Engine exhaust temperature</pre>				
G	EMISSION RATE (pounds of for a fuel flow rate of flow	-			
Н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 16 . Engine S/N 634012 Test Cell 20, single poin JP-5 fuel.	ORKFAC NORTH ISI JANUARY 1974	AND	exhaust plane.	

A	J57-P-420	75% THRUST		File J57021C		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	RH =	58°F 90% 30.02 in. Hg 0.014564 0.00607	$m = 13.$ $n = 23.$ $\eta = 0.$	4	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX	
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	pm 36.5 sd % 0.82 sd pm 16.3 sd pm pm pm pmC 8.4 w	0.81 16.5 1 16.0 1 0.5 8.6	6.6 16.4 0.81 0.80 6.4 16.1 5.9 15.6 0.5 0.5 8.5 8.4 9.77 19.46 8.82 77.62 2.12	4.32 3303.38 6.99 6.77 0.22 1.09 1.27	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	<pre>K = 0.9788 F/A = 0.003729 Combustion efficiency = Thrust = 6946 pounds Engine speed = 9090 rpm Engine exhaust temperatu</pre>					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 5767 pounds per hour Carbon monoxide 24.91 Carbon dioxide 19050.60 Oxides of nitrogen 40.32					
	Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	6.31 7.33 2.31				
Н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC NORTH ISLAND Date of measurement 16 JANUARY 1974 Engine S/N 634012 Test Cell 20, single point probe 95 feet behind engine exhaust plane. JP-5 fuel.					

А	J57-P-420	96% RPM		File J57021D		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	RH =	0.02,50.	$m = 13$ $n = 23$ $\eta = 0$. 4	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX	
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.00 sd 27.4 sd	0.99 27.7 26.8 0.9 10.4 19.64	5.5 5.4 0.99 0.97 7.5 27.1 6.7 26.2 0.9 0.9 0.4 10.2 9.53 19.20 8.88 77.56 2.27	1.17 3284.34 9.58 9.28 0.30 1.09 1.26	
D	Sulfur dioxide, calc.				0.40	
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 277 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	<pre>K = 0.9773 F/A = 0.004571 Combustion efficiency = 99 Thrust = 9139 pounds Engine speed = 9569 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 7667 pounds per hour Carbon monoxide 8.96 Carbon dioxide 25181.04 Oxides of nitrogen 73.46 Hydrocarbons, CHy/x 8.32 Hydrocarbons, CH ₄ 9.65 Sulfur dioxide 3.07					
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC NORTH ISLAND Date of measurement 16 JANUARY 1974 Engine S/N 634012 Test Cell 20, single point probe 95 feet behind engine exhaust plane. JP-5 fuel.					

Α	J57-P-420	NORMAL RATED	File J57021N				
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	T = 58°F RH = 90% B = 30.02 in. H = 0.014564 h _{sd} = 0.00607	<u> </u>	4			
	CONSTITUENT	EXHAUST CONCE	NTRATION Calculated semi- wet dry	EMISSION INDEX			
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.98 sd 0.97 25.7 sd 26.0 25.2 0.8	5.7 5.6 0.97 0.95 25.8 25.4 25.0 24.6 0.8 0.8 6.6 6.5 19.55 19.23 78.87 77.56 2.26	1.23 3287.72 9.18 8.89 0.29 0.71 0.82			
D	Sulfur dioxide, calc.			0.40			
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 265 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)						
F	<pre>K = 0.9774 F/A = 0.004475 Combustion efficiency = 99 Thrust = 9241 pounds Engine speed = 9508 rpm Engine exhaust temperature</pre>						
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 7701 pounds per hour Carbon monoxide 9.49 Carbon dioxide 25318.72 Oxides of nitrogen 70.70 Hydrocarbons, CHy/x 5.44 Hydrocarbons, CH ₄ 6.31 Sulfur dioxide 3.08						
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC NORTH ISLAND Date of measurement 16 JANUARY 1974 Engine S/N 634012 Test Cell 20, single point probe 95 feet behind engine exhaust plane. JP-5 fuel.						

Α	J57-P-420	ı	NTERME	DIAT	E	File	J57021M	
В	J = -0.07 $L = -0.0008$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$		T RI- B H h _s	= = =	58°F 90% 30.02 in. 0.014564 0.00607		$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		Measure		AUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Cxygen Nitrogen Water	ppm % ppm ppm ppm ppmC	24.1 1.21 45.1 5.6	sd sd	2.0 1.20 45.6 44.2 1.4 5.7 19.36 79.43	43.9 1.4 5.7	1.9 1.17 44.5 43.1 1.4 5.6 18.89 77.48 2.45	0.34 3268.72 12.97 12.56 0.41 0.49 0.57
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 387 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)							
F	<pre>K = 0.9755 F/A = 0.005553 Combustion efficiency Thrust = 12007 pounds Engine speed = 10090 r Engine exhaust tempera</pre>	:pm						
	EMISSION RATE (pounds for a fuel flow rate o							
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	34550. 137. 5. 6.						
Н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 634012 Test Cell 20, single p JP-5 fuel.	REWORKFA .6 JANUA	C NORTH	ISL	AND		st plane	

A	J57-P-420	AFTERBURNER	J., J	File J57021A	-
В	J = -0.07 $L = -0.0006$ $L' = 0.14$ $M = -0.00209$ $M' = 0.28$	H =		$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p	pm 336.1 sd 4.29 sd pm 65.4 sd pm pm pm pmC 103.0 w	4.27 66.4 64.3 2.1 108.5 10	8.0 284.7 4.24 4.05 6.0 63.0 3.9 61.1 2.1 2.0 7.8 103.0 5.08 14.40 0.04 76.45 5.06	14.20 3177.14 5.16 5.00 0.16 2.54 2.94
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			173	-
F	K = 0.9494 F/A = 0.020041 Combustion efficiency = Thrust = 18240 pounds Engine speed = 10085 rpm Engine exhaust temperatu				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide 12 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
Н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 16 Engine S/N 634012 Test Cell 20, single poi JP-5 fuel.	ORKFAC NORTH ISLAN JANUARY 1974	TD.	exhaust plane	

А	J65-W-5F	IDLE		File J65	50011
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$	В Н	4 = 45% = 30.04 i	n. Hg 72	a = 13.0 a = 23.4 a = 0.95
	CONSTITUENT	Measur	EXHAUST CON ed dry	Calculated	EMISSION INDEX wet
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	pm 201.7 % 0.87 pm 6.3 pm pm pm pmC 82.5 % 20.0	sd 0.8 sd 6.4 6.2 0.2	36 0.86 6.3 2 6.1 9 0.2 83.5	96.4 0.85 6.2 6.1 0.2 82.5 9.78 11.35 1.84
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				74 94
F	<pre>K = 0.9816 F/A = 0.004087 Combustion efficiency = Thrust = 450 pounds Engine speed = 4020 rpm Engine exhaust temperatu</pre>				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 22 Engine S/N 603118 Test Cell 1, single poin JP-5 fuel.	ORKFAC ALAME JUNE 1976	DA		

А	J65-W-5F	7450 rpm	File J650	001B		
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		n 4 in. Hg	= 13.0 = 23.4 = 0.95		
	CONSTITUENT	EXHAUST (CONCENTRATION Calculated dry semi- dry	EMISSION INDEX wet		
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.89 sd 00 nn 18.6 sd 18 nn 18.6 sd 18 nn	0.88 0.88 8.8 18.7 1 8.2 18.1 1 0.6 0.6 8.2 8.1 9.79 19.67 1 9.32 78.84 7	2.4 0.87 3279.73 8.4 7.30 7.9 0.6 0.23 8.0 0.95 1.10 9.42 7.86 1.85		
D	Sulfur dioxide, calc.			0.40		
E	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 217 Oxides of nitrogen at 3% oxygen, meas.(ppm wet) 139					
F	<pre>K = 0.9815 F/A = 0.004075 Combustion efficiency = 9 Thrust = 4710 pounds Engine speed = 7450 rpm Engine exhaust temperatur</pre>					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 4370 pounds per hour Carbon monoxide 55.11 Carbon dioxide 14332.42 Oxides of nitrogen 31.89 Hydrocarbons, CHy/x 4.16 Hydrocarbons, CH ₄ 4.82 Sulfur dioxide 1.75					
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC ALAMEDA Date of measurement 22 JUNE 1976 Engine S/N 603118 Test Cell 1, single point probe in test cell exhaust stack. JP-5 fuel.					

Α	J65-W-5F	8	3000 rpm			File	J65001C	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RH B H h _s	= = =	70°F 45% 30.04 in. 0.011072 0.00607	Hg	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		Measure	EXH	AUST CONCEI dry	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	41.3 1.09 17.9	sd sd	38.5 1.08 18.1 17.5 0.6 7.6 19.52 79.39	38.2 1.08 18.0 17.4 0.6 7.5	37.7 1.06 17.7 17.2 0.6 7.4 19.13 77.79 2.02	7.39 3266.45 5.71 5.53 0.18 0.72 0.83
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at Oxides of nitrogen at						175	
F	<pre>K = 0.9798 F/A = 0.005008 Combustion efficiency Thrust = 6380 pounds Engine speed = 8000 rp Engine exhaust tempera</pre>	om						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	9f 5970 44. 19500. 34. 4.	pounds 13 71 10 28					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N 603118 Test Cell 1, single po JP-5 fuel.	REWORKFA 22 JUNE	C ALAMEI 1976	DA				

А	J65-W-5F	8	300 rpm		·	File	J65001D	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RH B H	l = = =	70°F 45% 30.04 in. 0.011072 0.00607	Нg	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT	•	Measure	EXH	dry	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	29.7 1.22 18.1 3.8	sd	26.7 1.21 18.3 17.7 0.6 3.9 19.35 79.44	26.5 1.20 18.2 17.6 0.6 3.9 19.23 78.96	26.1 1.19 17.9 17.3 0.6 3.8 18.93 77.75 2.13	4.57 3261.68 5.15 4.99 0.16 0.33 0.38
D	Sulfur dioxide, calc.						-	0.40
E	Oxides of nitrogen at Oxides of nitrogen at						160	
F	<pre>K = 0.9787 F/A = 0.005611 Combustion efficiency Thrust = 7330 pounds Engine speed = 8300 rp Engine exhaust tempera</pre>	m						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	of cons f 7040 32. 22962. 36. 2. 2.	pounds 19 25 28 31 68	per per	hour) hour			
Н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N 603118 Test Cell 1, single po	FT ENVII EWORKFA	RONMENTA C ALAME 1976	DA				

A	J65-W-5F	MILITARY	·	File	J65001M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 70°F RH = 45% B = 30.04 in h = 0.01107 h _{sd} = 0.00607	'2	m = n = η =		
	CONSTITUENT		T CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.28 sd 19.3 sd	32.5 1.27 19.5 18.9 0.6 7.6 19.27 79.46	32.3 1.26 19.4 18.8 0.6 7.5	31.8 1.24 19.1 18.5 0.6 7.4 18.84 77.73 2.18	5.31 3255.43 5.23 5.06 0.16 0.61 0.71
D	Sulfur dioxide, calc.	——————————————————————————————————————		<u> </u>		0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				163	
F	<pre>K = 0.9782 F/A = 0.005897 Combustion efficiency = 99 Thrust = 7250 pounds Engine speed = 8311 rpm Engine exhaust temperature</pre>					
G	Carbon dioxide 226	46 pounds per hou 36.86 12.21 36.31				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 22 JU Engine S/N 603118 Test Cell 1, single point JP-5 fuel.	KFAC ALAMEDA NE 1976				

A	J79-GE-8D	IDLE		File J7900)11
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0.0100 h = 0.0060		$m = 13.0$ $n = 23.4$ $\eta = 0.9$	•
	CONSTITUENT		JST CONCEN C	alculated	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.62 sd 4.3 sd	167.7 0.62 4.3 4.2 0.1 103.3 20.14 79.23	4.3 4 4.2 4 0.1 0 102.6 101 20.02 19 78.75 78	3209.27 2.3 2.37 2.1 2.29 0.1
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			69)
F	<pre>K = 0.9848 F/A = 0.002904 Combustion efficiency = 97 Thrust = 259 pounds Engine speed = 5012 rpm Engine exhaust temperature</pre>				
G	Carbon dioxide 38 Oxides of nitrogen Hydrocarbons, $CH_{y/x}$	05 pounds per ho 67.12 67.17 2.86			
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 10 MA Engine S/N 401917 Test Cell 20, single point JP-5 fuel.	KFAC NORTH ISLAN Y 1977	ID		lane.

Α	J79-GE-8D	75% RPM		File	J79001B		
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0.010 h = 0.006		m - n - η -			
	CONSTITUENT		UST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX	
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen	72.0 sd 0.49 sd 0.41 sd 0m 0m 0m 0m 0m 0m 0m 0m 0m	69.9 0.49 4.1 4.0 0.1 20.4 20.33 79.18		69.0 0.48 4.1 4.0 0.1 20.1 20.04 78.07 1.40	30.61 3341.62 2.98 2.88 0.09 4.40 5.11	
D	Sulfur dioxide, calc.					0.40	
Ε		Oxides of nitrogen at 3% oxygen, calc.(ppm wet) 81 Oxides of nitrogen at 3% oxygen, meas.(ppm wet)					
F	K = 0.9860 F/A = 0.002205 Combustion efficiency = 9 Thrust = 1022 pounds Engine speed = 5763 rpm Engine exhaust temperature						
G	i e	46.53 5079.26 4.52					
	Sulfur dioxide Measurement by AIRCRAFT	0.61	PPORT OFFI	CE.			
н	Measurement at NAVAIREWO Date of measurement 10 M Engine S/N 401917 Test Cell 20, single poir JP-5 fuel.	ORKFAC NORTH ISLA MAY 1977	ND		st plane		

A	J79-GE-8D	87% RPM		File J	79001C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0.01000 h = 0.00607		$m = 1$ $n = 2$ $\eta = 2$		
	CONSTITUENT		T CONCENT Ca dry	CRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen	om 24.3 sd 0.72 sd 11.4 sd om 0m om 2.0 w	21.7 0.71 11.5 11.2 0.4 2.0 20.02 79.26	21.6 0.71 11.4 11.1 0.4 2.0 19.90 78.78	21.4 0.70 11.3 11.0 0.4 2.0 19.70 78.00 1.59	6.43 3321.46 5.60 5.42 0.18 0.30 0.34
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				163	
F	<pre>K = 0.9841 F/A = 0.003257 Combustion efficiency = 9 Thrust = 5933 pounds Engine speed = 6662 rpm Engine exhaust temperature</pre>					
	EMISSION RATE (pounds of for a fuel flow rate of 4					
G	Oxides of nitrogen	29.23 5096.06 25.45 1.35 1.57				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 10 N Engine S/N 401917 Test Cell 20, single poir JP-5 fuel.	ORKFAC NORTH ISLAND 1AY 1977			st plane.	

A	J79-GE-8D		90% NORM	AL RATE	D	File	79001D	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28			0.010000 0.00607	-	m = η = η =		
	CONSTITUENT-		Measure		CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppm % % % %	0.96 23.2	sd sd w	13.9 0.95 23.4 22.7 0.7 1.0 19.70 79.35	13.9 0.95 23.3 22.6 0.7 1.0 19.58 78.87	13.7 0.94 23.0 22.3 0.7 1.0 19.34 77.92 1.80	3.06 3289.04 8.46 8.20 0.27 0.11 0.13
D	Sulfur dioxide, calc.							0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at						257	
F	K = 0.9820 F/A = 0.004382 Combustion efficiency Thrust = 9700 pounds Engine speed = 7155 rp Engine exhaust tempera	m						
	EMISSION RATE (pounds for a fuel flow rate of						<u> </u>	
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	2698 6	9.45					
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 401917 Test Cell 20, single p JP-5 fuel.	REWORK .0 MAY	FAC NORTH	ISLAND			st plane	

A	J79-GE-8D	MILITARY		File J79001M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0.01000 h _{sd} = 0.00607		$m = 13.0 n = 23.4 \eta = 0.95$	
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppr Carbon dioxide % Oxides of nitrogen ppr Nitric oxide ppr Nitrogen dioxide ppr Hydrocarbons, CHy/x ppr Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.07 sd n 32.0 sd n	1.06 32.3 31.3 1.0 1.4	10.5 10.3 1.06 1.04 32.2 31.7 31.1 30.7 1.0 1.0 1.4 1.4 19.43 19.18 78.91 77.88 1.90	2.07 3278.84 10.44 10.11 0.33 0.14 0.16
D	Sulfur dioxide, calc.			•	0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			322	
F	K = 0.9810 F/A = 0.004898 Combustion efficiency = 99 Thrust = 10838 pounds Engine speed = 7690 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of of for a fuel flow rate of 94) Carbon monoxide Carbon dioxide 309 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	19.54 994.88 98.70	,		
н	Measurement by AIRCRAFT I Measurement at NAVAIREWOR Date of measurement 10 MA Engine S/N 401917 Test Cell 20, single point JP-5 fuel.	RKFAC NORTH ISLAND NY 1977			· .

A	J79-GE-10	AFTERBURNER	File J79020A
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00209 M' = 0.28	T = 63°F RH = 72% B = 29.92 in. H h = 0.013935 h = 0.00607	
	CONSTITUENT	EXHAUST (Measured	CONCENTRATION EMISSION Calculated INDEX dry semi- wet dry
c	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	% 3.81 sd 3.81 sd 5.2 pm 52.9 sd 5.2 pm 52.7 w 34 % 15.7 sd 15	7.6 246.1 236.2 13.25 3.79 3.77 3.62 3186.92 3.7 53.4 51.2 4.72 2.0 51.7 49.6 4.57 1.7 1.6 0.15 4.3 34.1 32.7 0.91 1.05 5.83 15.73 15.10 0.35 79.87 76.66 4.60
D	Sulfur dioxide, calc.		0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%		
F	<pre>K = 0.9540 F/A = 0.017773 Combustion efficiency = Thrust = 17222 pounds Engine speed = 7464 rpm Engine exhaust temperature</pre>		
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide 10 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		
н	Measurement by AIRCRAFT Measurement at NAVAIREV Date of measurement 12 Engine S/N 433996 Test Cell 20, single poi JP-5 fuel.	ORKFAC NORTH ISLAND JUNE 1974	

Α	J79-GE-10B		IDLE			File	J79BB01I		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00161$ $M' = 0.28$		В Н	= h	61°F 72% 29.88 in. 0.012991 0.00607		$m = 13.$ $n = 23.$ $\eta = 0.$	4	
	CONSTITUENT		Measur	EXH	AUST CONCE	NTRATION Calculate semi- dry	d wet	EMISSION INDEX	
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % % %	415.6 0.70 2.9 281.1 20.0	sd sd	402.1 0.69 2.9 2.8 0.1 286.5 20.01 79.25	399.7 0.69 2.9 2.8 0.1 284.8 19.89 78.77	394.5 0.68 2.9 2.8 0.1 281.1 19.63 77.75 1.90	111.41 3023.18 1.33 1.29 0.04 39.19 45.47	
D	Sulfur dioxide, calc.					,		0.40	
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3						39 44		
F	<pre>K = 0.9810 F/A = 0.003480 Combustion efficiency = Thrust = 265 pounds Engine speed = 5077 rpr Engine exhaust temperate</pre>	n							
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 1250 pounds per hour Carbon monoxide 139.26 Carbon dioxide 3778.97 Oxides of nitrogen 1.67 Hydrocarbons, CHy/x 48.98 Hydrocarbons, CH ₄ 56.84 Sulfur dioxide 0.50								
Н	Measurement by AIRCRAI Measurement at NAVAIRI Date of measurement 12 Engine S/N 433421 Test Cell 19, single po JP-5 fuel.	EWORKFA 2 June	AC NORTH 1974	ISL	AND		ust plane		

Α	J79-GE-10B		30% THRU	JST		File	J79BB01B			
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00161$ $M' = 0.28$		T RI B H h	 - -	61°F 72% 29.88 in. 0.012991 0.00607		$m = 13.$ $n = 23.$ $\eta = 0.$	4		
	CONSTITUENT		Measur	EXH	AUST CONCE	NTRATION Calculated semi- dry	i wet	EMISSION INDEX		
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % %	67.9 0.57 6.8 15.6 20.2	sd	53.5 0.57 6.9 6.7 0.2 15.9 20.22 79.21	0.56 6.8 6.6 0.2 15.8	52.5 0.56 6.7 6.5 0.2 15.6 19.86 77.82 1.76	20.04 3331.43 4.23 4.10 0.13 2.94 3.41		
D	Sulfur dioxide, calc.							0.40		
E	Oxides of nitrogen at Oxides of nitrogen at						112 121			
F	K = 0.9824 F/A = 0.002573 Combustion efficiency Thrust = 3381 pounds Engine speed = 6340 rp Engine exhaust tempera	oin								
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 3422 pounds per hour Carbon monoxide 68.59									
н	Measurement by AIRCRAFT ENVIRONMENTAL SUPPORT OFFICE Measurement at NAVAIREWORKFAC NORTH ISLAND Date of measurement 12 June 1974 Engine S/N 433421 Test Cell 19, single point probe 95 feet behind engine exhaust plane. JP-5 fuel.									

А	J79-GE-10B	85% RPM		· · ·	File .	J79BB01C	
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00161$ $M' = 0.28$	T RI B H h	d = = =	29.88 in. 0.012991	Нg	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT	Measur	EXH.	AUST CONCE (dry	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄	pm 57.6 % 0.66 pm 8.6 pm pm pmC 14.3 % 20.1 %	sd sd w	42.3 0.65 8.7 8.4 0.3 14.6 20.10 79.24	42.0 0.65 8.6 8.4 0.3 14.5	41.5 0.64 8.5 8.3 0.3 14.3 19.73 77.79 1.83	13.63 3317.03 4.60 4.46 0.15 2.32 2.69
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%					126 142	
F	<pre>K = 0.9817 F/A = 0.002991 Combustion efficiency = Thrust = 4243 pounds Engine speed = 6496 rpm Engine exhaust temperature</pre>						
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide l Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide						
Н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 12 Engine S/N 433421 Test Cell 19, single poi JP-5 fuel.	ORKFAC NORTH June 1974	ISL	AND		st plane.	

A	J79-GE-10B	75% THRUST		File J79BB01D	
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00161$ $M' = 0.28$	RH =		$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen % Nitrogen % Water %	0.99 sd 23.4 sd	0.98 23.7 22.9 0.7 15.2 19.66	2.8 12.6 0.98 0.96 3.5 23.2 2.8 22.4 0.7 0.7 5.1 14.9 9.54 19.24 8.88 77.68 2.12	2.74 3281.22 8.26 8.00 0.26 1.60 1.85
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			243 270	33333
F	<pre>K = 0.9788 F/A = 0.004530 Combustion efficiency = 99 Thrust = 9000 pounds Engine speed = 7171 rpm Engine exhaust temperature</pre>				
G	Oxides of nitrogen Hydrocarbons, CH _{Y/x}				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 12 Ju Engine S/N 433421 Test Cell 19, single point JP-5 fuel.	KFAC NORTH ISL ne 1974	AND	exhaust plane	

А	J79-GE-10B	IN	TERME	DIATE	:	File	J79BB01M		
В	J = -0.07 $L = -0.0009$ $L' = 0.14$ $M = -0.00161$ $M' = 0.28$		T RH B H	= = =	61°F 72% 29.88 in. 0.012991 0.00607	Нд	$m = 13.0$ $n = 23.0$ $\eta = 0.0$	4	
	CONSTITUENT	M	leasure	EXH	AUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX	
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm % ppm ppm ppm ppm % % % % %	29.3 1.19 35.1 13.6 19.4		9.1 1.18 35.5 34.4 1.1 13.9 19.39 79.43	9.0 1.17 35.3 34.2 1.1 13.8 19.27 78.95	8.9 1.15 34.7 33.6 1.1 13.6 18.94 77.61 2.29	1.60 3265.84 10.26 9.93 0.32 1.21 1.40	
D	Sulfur dioxide, calc.					 .		0.40	
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%						311 333		
F	<pre>K = 0.9771 F/A = 0.005467 Combustion efficiency = Thrust = 11248 pounds Engine speed = 7475 rpm Engine exhaust temperature</pre>		286°F						
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 10000 pounds per hour Carbon monoxide 15.97 Carbon dioxide 32658.38 Oxides of nitrogen 102.58 Hydrocarbons, CHy/x 12.09 Hydrocarbons, CH ₄ 14.03 Sulfur dioxide 4.00								
н	Measurement by AIRCRAFT Measurement at NAVAIREM Date of measurement 12 Engine S/N 433421 Test Cell 19, single poi JP-5 fuel.	VORKFAC June 19	NORTH 974	ISL	AND		ust plane.		

A	J79-GE-10B	AFTER	BUR	NEF	₹		File	J79BB01A	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00161 M' = 0.28		T RH B H	=	61°F 72% 29.88 in. 0.012991 0.00607			$m = 13.$ $n = 23.$ $\eta = 0.$. 4
	CONSTITUENT	Meas	I sured		AUST CONCE	Calcu se	CION lated emi- dry	wet	EMISSION INDEX
C	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	% 3. pm 49. pm pm pm pm pm 18.	.3 v	sd sd	264.2 3.68 49.8 48.2 1.6 19.1 15.97 80.31	3 49 48 1 19	2.6 3.66 3.5 3.0 3.6 3.0 3.8 3.8 3.83	252.5 3.52 47.6 46.1 1.5 18.3 15.27 76.76 4.42	14.56 3186.88 4.51 4.37 0.14 0.52 0.60
D	Sulfur dioxide, calc.								0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%							150 145	
F	<pre>K = 0.9558 F/A = 0.017267 Combustion efficiency = Thrust = 17500 pounds Engine speed = 7475 rpm Engine exhaust temperature</pre>								
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide 11 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide								
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 12 Engine S/N 433421 Test Cell 19, single poils JP-5 fuel.	ORKFAC NOB June 1974	RTH]	[SL	AND		exhau	st plane	

Α	J79-GE-8B	IC	LE				File	J79002I	
В	J = -0.07 $L = -0.0001$ $L' = 0.14$ $M = -0.00033$ $M' = 0.28$		T RH B H h	= I = =				$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		Measure	EXH	AUST CONCE	Calcu se	ION lated mi- try	wet	EMISSION INDEX
C	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	% ppm ppm	166.9 0.62 4.1 100.6	sd sd	165.3 0.62 4.1 4.0 0.1 102.6 20.14 79.23	0 4 4 0 101	3 61 1 0 1 9	162.1 0.60 4.1 3.9 0.1 100.6 19.76 77.71 1.91	54.92 3210.91 2.26 2.19 0.07 16.82 19.52
D	Sulfur dioxide, calc.						· .		0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at							61	
F	<pre>K = 0.9809 F/A = 0.002903 Combustion efficiency Thrust = 233 pounds Engine speed = 5016 rp Engine exhaust tempera</pre>	om							
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		oounds 1 5 7 9 8 9						
Ħ	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 401394 Test Cell 20, single p JP-5 fuel.	REWORKFAC .3 MAY 19	NORTH 177	ISL	AND		exhau	st plane	

A	J79-GE-8B	75% RPM		File J79002B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.01404 h _{sd} = 0.00607	0	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUS Measured		ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppr Carbon dioxide % Oxides of nitrogen ppr Nitric oxide ppr Nitrogen dioxide ppr Hydrocarbons, CHy/x ppr Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.49 sd n 4.2 sd n	0.49 4.2 4.1 0.1 17.6	66.7 65.9 0.48 0.48 4.2 4.2 4.1 4.0 0.1 0.1 17.5 17.3 20.20 19.96 78.70 77.76 1.79	29.41 3345.65 3.05 2.96 0.10 3.81 4.42
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			76	
F	K = 0.9821 F/A = 0.002203 Combustion efficiency = 98 Thrust = 863 pounds Engine speed = 5768 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of for a fuel flow rate of 1st Carbon monoxide Carbon dioxide 5st Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide				
н	Measurement by AIRCRAFT Measurement at NAVAIREWOOD Date of measurement 13 Marce Engine S/N 401394 Test Cell 20, single point JP-5 fuel.	ENVIRONMENTAL SUPP RKFAC NORTH ISLAND AY 1977			

A	J79-GE-8B	87%	RPM		File J	79002C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T RH B h	= 29.91 in = 0.014040		m = 1 n = 2 η =	23.4	
	CONSTITUENT			CONCENCE C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	% ppm 1 ppm ppm	3.4 sd 0.73 sd 1.5 sd 2.2 w	20.8 0.72 11.6 11.3 0.4 2.2 20.01 79.27	20.7 0.72 11.5 11.2 0.4 2.2 19.89 78.79	20.4 0.71 11.4 11.0 0.4 2.2 19.61 77.69 1.99	6.07 3319.84 5.57 5.39 0.18 0.32 0.38
D	Sulfur dioxide, calc.						0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at					153	
F	K = 0.9801 F/A = 0.003304 Combustion efficiency Thrust = 6015 pounds Engine speed = 6600 r Engine exhaust temper	pm	/2°F				
G	EMISSION RATE (pounds for a fuel flow rate Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	of 4689 pot 28.48 15566.75 26.11					
н	Measurement by AIRCR Measurement at NAVAI Date of measurement Engine S/N 401394 Test Cell 20, single JP-5 fuel.	REWORKFAC N 13 MAY 1977	ORTH ISLAND			st plane	

A	J79-GE-8B	90% RPM		File J7	79002D	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 h = 0.014 h _{sd} = 0.006	040	m = 1 n = 2 n =	3,4	
	CONSTITUENT	EXHA Measured	UST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
C	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	20m 18.5 sd 0.97 sd 22.3 sd 20m 22.3 sd 20m 22.7 w	15.6 0.96 22.5 21.8 0.7 2.8 19.68 79.35	0.7 2.7 19.57	15.3 0.94 22.0 21.3 0.7 2.7 19.25 77.60 2.20	3.40 3286.69 8.05 7.79 0.25 0.30 0.34
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				233	
F	<pre>K = 0.9780 F/A = 0.004431 Combustion efficiency = Thrust = 9659 pounds Engine speed = 7126 rpm Engine exhaust temperatu</pre>					
G						
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 13 Engine S/N 401394 Test Cell 20, single poi JP-5 fuel.	ORKFAC NORTH ISLA MAY 1977	ND		t plane	AFSO 00-20-1997

A	J79-GE-8B	95% RPM		File J7900	2E
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.01404 h = 0.00601	40	$ \begin{array}{r} m = 13.0 \\ n = 23.4 \\ \eta = 0.9 \end{array} $	
	CONSTITUENT		ST CONCENT Ca dry	lculated	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.01 sd m 25.4 sd m m m mC 1.1 w	12.9 1.00 25.7 24.9 0.8 1.1 19.63 79.36	25.5 25 24.7 24 0.8 0 1.1 1 19.51 19 78.88 77	.98 3283.97 .1 8.79
О	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			257	
F	K = 0.9777 F/A = 0.004617 Combustion efficiency = 9 Thrust = 10291 pounds Engine speed = 7280 rpm Engine exhaust temperatur				
	EMISSION RATE (pounds of for a fuel flow rate of 8				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	'624 . 79 73 . 97			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 13 M Engine S/N 401394 Test Cell 20, single poin JP-5 fuel.	ORKFAC NORTH ISLANI IAY 1977)		lane.

Α	J79-GE-8B	9	MILITARY			File	J79002M	
8	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28		h = ()%		n =	13.0 23.4 0.95	
	CONSTITUENT		Measure		UST CONCENT Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppmC % %	16.3 1.08 32.9	sd sd	13.3 1.07 33.3 32.2 1.0 1.6	13.2 1.07 33.1 32.0 1.0 1.6 19.42 78.91	13.0 1.05 32.5 31.5 1.0 1.6	2.59 3276.97 10.63 10.29 0.34 0.16
D	Sulfur dioxide, calc.							0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at						313	
F	K = 0.9771 F/A = 0.004946 Combustion efficiency Thrust = 10939 pounds Engine speed = 7686 rg Engine exhaust tempera	om						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	23. 30230. 98. 1.	pounds 1 92 07 06 45					
Н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 401394 Test Cell 20, single p JP-5 fuel.	REWORKFA 13 MAY 1	C NORTH 977	ISLAN	ID		st plane	

A	J79-GE-8B	75% RPM		File J79F02B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.014040 h _{sd} = 0.00607		m = 13.0 n = 23.4 η = 0.95	
	CONSTITUENT	EXHAUS Measured	dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 88.9 sd % 0.49 sd ppm 3.2 sd ppm ppm ppm ppmC 25.7 w	0.49 3.2 3.1 0.1 26.2 2	6.4 85.4 0.48 0.48 3.2 3.2 3.1 3.1 0.1 0.1 6.0 25.7 0.20 19.96 8.70 77.76 1.79	37.86 3325.27 2.31 2.24 0.07 5.62 6.53
٥	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at Oxides of nitrogen at			58	
F	K = 0.9821 F/A = 0.002216 Combustion efficiency Thrust = 863 pounds Engine speed = 5768 rp Engine exhaust tempera	om			
	EMISSION RATE (pounds for a fuel flow rate of				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	59.33 5210.70 3.62 8.81 10.23 0.63			
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 401394 Test Cell 20, single p JP-5 fuel with ferroce	EWORKFAC NORTH ISLAND 3 MAY 1977 oint probe 85 feet bel		exhaust plane	

Α	J79-GE-8B	87% RPM		File J	79F02C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h - 0.0	l in. Hg	m = 1 n = 2 η =	3.4	
	CONSTITUENT		HAUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 31.5 sd % 0.73 sd ppm 10.0 sd ppm ppm ppm ppmC 2.2 w	0.72	28.8 0.72 10.0 9.7 0.3 2.2 19.89 78.79	28.4 0.71 9.9 9.6 0.3 2.2 19.61 77.69 1.99	8.44 3315.94 4.84 4.68 0.15 0.32 0.37
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at Oxides of nitrogen at				133	
F	K = 0.9801 F/A = 0.003308 Combustion efficiency Thrust = 6015 pounds Engine speed = 6600 rp Engine exhaust tempera	m				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	f 4689 pounds per 39.58 15548.46 22.68 1.51				
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 401394 Test Cell 20, single po JP-5 fuel with ferroce	EWORKFAC NORTH IS 3 MAY 1977 Dint probe 85 fee	LAND		t plane	

A	J79-GE-8B	90% RPM		File J79F02D	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.014044 h = 0.00607	r . Hg η	1 = 13.0 1 = 23.4 2 = 0.95	
	CONSTITUENT	EXHAUS Measured	CONCENTRATIO Calcula dry semi dry	ted wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 25.9 sd % 0.97 sd ppm 20.8 sd ppm ppm ppm ppm 2.7 w	23.1 23.0 0.96 0.9 21.0 20.4 20.2 0.7 2.8 2.7 19.68 19.5 79.35 78.8	06 0.94 0 20.6 19.9 0 0.6 2 2.7 16 19.25	5.01 3284.08 7.50 7.26 0.24 0.30 0.34
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3			217	
F	<pre>K = 0.9780 F/A = 0.004435 Combustion efficiency = Thrust = 9659 pounds Engine speed = 7126 rpm Engine exhaust temperat</pre>	ı			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 13 Engine S/N 401394 Test Cell 20, single po JP-5 fuel with ferrocer	WORKFAC NORTH ISLAND MAY 1977 int probe 85 feet be		khaust plane	

Α	J79-GE-8B	95% RPM		File J	79F02E	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.01404 h = 0.00607	0	m = 1 n = 2 η =	23.4	
	CONSTITUENT			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.01 sd 23.9 sd	16.5 1.00 24.2 23.4 0.8 1.1 19.63 79.36	16.4 1.00 24.0 23.3 0.8 1.1 19.51 78.88	16.1 0.98 23.6 22.9 0.7 1.1 19.19 77.59 2.23	3.44 3282.76 8.27 8.01 0.26 0.12 0.13
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				241	
F	K = 0.9777 F/A = 0.004619 Combustion efficiency = 99 Thrust = 10939 pounds Engine speed = 7686 rpm Engine exhaust temperature					
	EMISSION RATE (pounds of c for a fuel flow rate of 84					
G	Carbon dioxide 276 Oxides of nitrogen Hydrocarbons, CHy/x	69.58				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 13 MA Engine S/N 401394 Test Cell 20, single point JP-5 fuel with ferrocene.	KFAC NORTH ISLAND Y 1977			st plane	

A	J79-GE-8B	MILITARY	·	File J79F02M	
8	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 64°F RH = 70% B = 29.91 in h = 0.01404 h = 0.00607		m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT		dry se	TION lated emi- wet	EMISSION INDEX
С	Carbon monoxide ppor Carbon dioxide % Oxides of nitrogen ppor Nitric oxide ppor Nitrogen dioxide ppor Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.08 sd n 30.7 sd n	1.07 1 31.0 30 30.1 29 1.0 1 1.6 1	7.8 17.5 1.07 1.05 0.8 30.3 0.9 29.4 1.0 1.0 1.6 1.6 0.42 19.09 3.91 77.57 2.29	3.49 3275.52 9.91 9.60 0.31 0.16 0.18
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			292	
F	K = 0.9771 F/A = 0.004949 Combustion efficiency = 9 Thrust = 10939 pounds Engine speed = 7686 rpm Engine exhaust temperatur				
G	EMISSION RATE (pounds of for a fuel flow rate of 9 Carbon monoxide Carbon dioxide 30 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	32.21 32.70 216.70 91.46			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 13 M Engine S/N 401394 Test Cell 20, single poin JP-5 fuel with ferrocene.	RKFAC NORTH ISLAND AY 1977		exhaust plane	

A	7LM1500-PB-104A	IDLE		File LM1501I	
В	J = -0.07 L = -0.0009 L' = 0.14 M = -0.00642 M' = 0.28	T = 59°F RH = 73% B = 30.08 in h = 0.012186 h _{sd} = 0.00607		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT			ATION . culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.43 sd 1.6 sd	0.43 1.6 1.6 0.1 42.2	81.6 80.8 0.42 0.42 1.6 1.6 1.6 1.5 0.1 0.1 41.9 41.5 20.28 20.09 77.93 1.56	40.86 3336.90 1.32 1.28 0.04 10.36 12.02
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% o Oxides of nitrogen at 3% o			33	
F	<pre>K = 0.9844 F/A = 0.001938 Combustion efficiency = 98 Thrust = 565 pounds Engine speed = 5026 rpm Engine exhaust temperature</pre>				
G	Carbon dioxide 41 Oxides of nitrogen Hydrocarbons, $CH_{y/x}$ Hydrocarbons, CH_{4}	37 pounds per hou: 50.54 27.74 1.63			
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 10 FE Engine S/N 417214 Test Cell 13, single point JP-5 fuel, 346 square inch	NVIRONMENTAL SUPPO KFAC NORTH ISLAND BRUARY 1975 probe 50 feet bel		e exhaust plane	

A	7LM1500-PB-104A	75% THRUST		File l	LM1501B	
В	J = -0.07 L = -0.0009 L' = 0.14 M = -0.00642 M' = 0.28	T = 59°F RH = 73% B = 30.08 in h = 0.01218 h = 0.00607	4	m = n = η =		
	CONSTITUENT	EXHAUS Measured		NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.63 sd 6.7 sd	12.1 0.62 6.8 6.6 0.2 8.1 20.14 79.23		11.9 0.61 6.7 6.4 0.2 8.0 19.80 77.86 1.73	4.14 3344.09 3.79 3.67 0.12 1.37 1.59
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% o Oxides of nitrogen at 3% o				104	
F	<pre>K = 0.9827 F/A = 0.002832 Combustion efficiency = 99 Thrust = 6041 pounds Engine speed = 6957 rpm Engine exhaust temperature</pre>					
G	Carbon dioxide 153	97 pounds per hou 19.02 72.79 17.40				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 10 FE Engine S/N 417214 Test Cell 13, single point JP-5 fuel, 346 square inch	KFAC NORTH ISLAND BRUARY 1975 probe 50 feet be			st plane	

Α	7LM1500-PB-104A	NORMAL RATED	File	LM1501N	
В	J = -0.07 L = -0.0009 L' - 0.14 M = -0.00642 M' = 0.28	T = 59°F RH = 73% B = 30.08 in. 1 h = 0.012184 h _{sd} = 0.00607	n =	13.0 23.4 0.95	
	CONSTITUENT	Measured	CONCENTRATION Calculate dry semi- dry	d wet	EMISSION INDEX
c	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.82 sd 14 13:9 sd 14 1 2 7.6 w	8.7 8.7 0.81 0.81 4.0 14.0 3.6 13.5 0.4 0.4 7.7 7.7 9.89 19.77 9.30 78.82	8.6 0.80 13.8 13.3 0.4 7.6 19.51 77.80 1.89	2.26 3307.09 5.97 5.78 0.19 0.99 1.15
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or			172	
F	K = 0.9811 F/A = 0.003725 Combustion efficiency = 99 Thrust = 10024 pounds Engine speed = 7453 rpm Engine exhaust temperature				
G	Carbon dioxide 2613 Oxides of nitrogen 4 Hydrocarbons, $CH_{y/x}$	03 pounds per hour 17.87 35.91 47.17)	,	
н	Measurement by AIRCRAFT EN Measurement at NAVAIREWORN Date of measurement 10 FEN Engine S/N 417214 Test Cell 13, single point JP-5 fuel, 346 square inch	KFAC NORTH ISLAND BRUARY 1975 probe 50 feet behi		ust plane.	

А	7LM1500-PB-104A		INTERMEDIATE		File L	.M1501M		
8	J = -0.07 L = -0.0009 L' = 0.14 M = -0.00642 M' = 0.28		T = 59°F RH = 73% B = 30.08 in h = 0.01218 h = 0.00607	4	m - 1 n = 2 n -			
	CONSTITUENT			T CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX	
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC	53.2 sd 0.83 sd 15.2 sd 8.0 w	7.1 0.82 15.4 14.9 0.5 8.2 19.87 79.30	7.1 0.82 15.3 14.8 0.5 8.1 19.75 78.82	7.0 0.81 15.1 14.6 0.5 8.0 19.50 77.79 1.90	1.82 3306.05 6.45 6.24 0.20 1.03 1.19	
D	Sulfur dioxide, calc.						0.40	
Ε	Oxides of nitrogen at Oxides of nitrogen at					186		
F	K = 0.9810 F/A = 0.003771 Combustion efficiency Thrust = 10509 pounds Engine speed = 7564 rg Engine exhaust tempers	p m						
	for a fuel flow rate of	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 8356 pounds per hour						
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	27625 53 8 9	3.86					
Н	Measurement by AIRCRA Measurement at NAVAIA Date of measurement Engine S/N 417214 Test Cell 13, single p JP-5 fuel, 346 square	REWORKF 10 FEBR point p	FAC NORTH ISLAND RUARY 1975 Probe 50 feet be)		st plane		

Α	LM2500	IDLE		File LM2501I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT .		EXHAUST CONCE d dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 259.1 % 0.65 ppm 2.3 ppm ppm ppmC 334.8	sd 0.64 sd 2.3 2.3 0.1	2.3 2.3 2.2 2.2 0.1 0.1 338.3 334.8	77.73 3051.92 1.15 1.11 0.04 50.60 58.72
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3			35	
F	K = 0.9838 F/A = 0.003201 Combustion efficiency = Engine speed = 5000 rpm Engine exhaust temperat	1			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 19 Engine S/N GG018 Test Cell 20, single po JP-5 fuel.	WORKFAC NORTH MAY 1977	ISLAND		

Α	LM2500	7235 RPM		File LM2501B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	h = 0		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		EXHAUST CONC ed dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 124.7 % 0.70 ppm 5.3 ppm ppm ppmC 64.2	sd 0.69 sd 5.4 5.2 0.2	0.69 0.68 5.3 5.3 5.2 5.1 0.2 0.2 64.9 64.2	36.51 3245.36 2.62 2.53 0.08 9.58 11.12
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3 Oxides of nitrogen at 3			76	
F	K = 0.9835 F/A = 0.003242 Combustion efficiency = Engine speed = 7235 rpm Engine exhaust temperat				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide				
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 19 Engine S/N GG018 Test Cell 20, single po JP-5 fuel.	ORKFAC NORTH MAY 1977	ISLAND		

А	LM2500	7708 RPM		File LM2501C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 in h = 0.01070 h = 0.00607	1	$ \begin{array}{r} m = 13.0 \\ n = 23.4 \\ \eta = 0.95 \end{array} $	
	- CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen	om 64.6 sd 6 0.82 sd om 10.3 sd om om omC 16.7 w	0.81 10.4 1 10.1 1 0.3 17.0 1	1.8 61.1 0.81 0.80 0.3 10.2 0.0 9.9 0.3 0.3 6.9 16.7 9.76 19.53 8.82 77.91 1.75	15.96 3280.82 4.39 4.25 0.14 2.15 2.50
D	Sulfur dioxide, calc.				0.40
٤	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			130	
F	K = 0.9825 F/A = 0.003755 Combustion efficiency = 9 Engine speed = 7708 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of for a fuel flow rate of a fuel flow rate				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 19 M Engine S/N GG018 Test Cell 20, single poin JP-5 fuel.	ORKFAC NORTH ISLAND MAY 1977	1	exhaust plane	

А	LM2500	781	4 RPM			File L	.M2501D	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T RH B h	= 29			$m = 1$ $n = 2$ $\eta = 2$	23.4	
	CONSTITUENT		easure			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	* %	47.6 0.89 12.6 9.9	sd sd	45.0 0.88 12.7 12.3 0.4 10.1 19.79 79.32	44.7 0.88 12.7 12.3 0.4 10.0 19.67 78.84	44.2 0.87 12.5 12.1 0.4 9.9 19.43 77.89 1.81	10.65 3282.17 4.95 4.79 0.16 1.18 1.37
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at Oxides of nitrogen at						148	
F	K = 0.9819 F/A = 0.004072 Combustion efficiency Engine speed = 7814 rpt Engine exhaust tempera	n	55°F					
G		36.52 11261.14 16.97						
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N GG018 Test Cell 20, single po JP-5 fuel.	EWORKFAC 1 9 MAY 1971	NORTH 7	ISLAND			st plane	

Α	LM2500	79	49 RPM	l		File L	.M2501E	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T RI B h	_ (m = 3 n = 3 η =		
	CONSTITUENT		leasur			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % % %	26.9 0.97 17.3	sd sd	24.1 0.96 17.5 16.9 0.6 5.3 19.68 79.35	24.0 0.96 17.4 16.8 0.5 5.3 19.56 78.87	23.6 0.94 17.2 16.6 0.5 5.2 19.31 77.86 1.88	5.23 3282.84 6.23 6.04 0.20 0.57 0.66
נ	Sulfur dioxide, calc.							0.40
Ε	Oxides of nitrogen at 3% oxygen, calc.(ppm wet) Oxides of nitrogen at 3% oxygen, meas.(ppm wet)							
F	K = 0.9812 F/A = 0.004436 Combustion efficiency Engine speed = 7949 rp Engine exhaust tempera	m	959°F					
G	EMISSION RATE (pounds of constituent per hour) for a fuel flow rate of 4097 pounds per hour Carbon monoxide 21.43 Carbon dioxide 13449.79 Oxides of nitrogen 25.54 Hydrocarbons, CHy/x 2.33 Hydrocarbons, CH ₄ 2.70 Sulfur dioxide 1.64							
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N GG018 Test Cell 20, single p JP-5 fuel.	EWORKFAC 9 MAY 191	NORTH 77	ISLAND			st plane	

A	LM2500	8046 RPM		File I	_M2501F	
В	J = -0.07 L = -0.0001 L = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 ir h = 0.01070 h _{sd} = 0.00607	1	m = n = η =		
	CONSTITUENT		T CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppr Carbon dioxide % Oxides of nitrogen ppr Nitric oxide ppr Nitrogen dioxide ppr Hydrocarbons, CHy/x ppr Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.03 sd n 20.8 sd n	15.4 1.02 21.0 20.4 0.7 4.3 19.60 79.37	15.3 1.02 20.9 20.2 0.7 4.3 19.49 78.89	15.1 1.00 20.6 20.0 0.7 4.2 19.23 77.84 1.93	3.14 3280.10 7.05 6.83 0.22 0.43 0.50
D	Sulfur dioxide, calc.			· · · · · · · · · · · · · · · · · · ·		0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			-	215	
F	<pre>K = 0.9807 F/A = 0.004714 Combustion efficiency = 99 Engine speed = 8046 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of of for a fuel flow rate of 46 Carbon monoxide Carbon dioxide 150 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	521 pounds per hou 14.52 .57.32 32.59				
н	Measurement by AIRCRAFT I Measurement at NAVAIREWOR Date of measurement 19 MA Engine S/N GG018 Test Cell 20, single point JP-5 fuel.	RKFAC NORTH ISLAND NY 1977)		st plane	

A	LM2500	8190 RPM	 	File LM2501G	
8	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T - 66°F RH - 50% B - 29.98 in h - 0.010700 h _{sd} - 0.00607		m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.16 sd n 29.1 sd n	28.5 0.9 4.6 19.43	6.8 6.7 1.14 1.13 29.2 28.8 28.3 27.9 0.9 0.9 4.6 4.5 19.31 19.03 78.94 77.80 2.04	1.23 3271.41 8.74 8.46 0.28 0.41 0.48
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			270	
F	<pre>K = 0.9796 F/A = 0.005320 Combustion efficiency = 99 Engine speed = 8190 rpm Engine exhaust temperature</pre>				
G	EMISSION RATE (pounds of of for a fuel flow rate of 50 Carbon monoxide Carbon dioxide 184 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	6.95 473.62 49.35			
н	Measurement by AIRCRAFT I Measurement at NAVAIREWON Date of measurement 19 MA Engine S/N GG018 Test Cell 20, single point JP-5 fuel.	RKFAC NORTH ISLAND AY 1977			

A	LM2500	8210 RPM	File LM2501H	
В	J0.07 L0.0001 L' - 0.14 M0.00033 M' - 0.28	T = 66°F RH = 50% B = 29.98 in. Hg h = 0.010701 h = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		NCENTRATION Calculated y semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.17 sd 1.1 29.8 sd 30.1 29.2 0.9 C 4.1 w 4.2	16 1.15 1.14 29.9 29.5 2 29.0 28.6 9 0.9 0.9 2 4.2 4.1 42 19.30 19.02	1.11 3270.93 8.87 8.59 0.28 0.37 0.43
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of		274	
F	<pre>K = 0.9795 F/A = 0.005367 Combustion efficiency = 99 Engine speed = 8210 rpm Engine exhaust temperature</pre>			
G	EMISSION RATE (pounds of c for a fuel flow rate of 57 Carbon monoxide Carbon dioxide 186 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	10 pounds per hour 6.34 77.01 50.66		
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 19 MA Engine S/N GG018 Test Cell 20, single point JP-5 fuel.	KFAC NORTH ISLAND Y 1977		

Α	LM2500	8297 RPM	······································	File LM2501	J
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 in h = 0.01070 h = 0.00607	1	m = 13.0 n = 23.4 η = 0.95	
	CONSTITUENT		T CONCENTE Cal	RATION lculated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppor Carbon dioxide % Oxides of nitrogen ppor Nitric oxide ppor Nitrogen dioxide ppor Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.25 sd n 35.6 sd n	3.6 1.24 36.0 34.9 1.1 4.6	3.6 3.5 1.23 1.2 35.8 35.2 34.6 34.1 1.1 1.1 4.6 4.5 19.19 18.9 78.97 77.7 2.1	1 3265.79 9.90 9.59 0.31 0.38 0.44
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% oxides of nitrogen at 3% oxides			309	
F	K = 0.9788 F/A = 0.005741 Combustion efficiency = 96 Engine speed = 8297 rpm Engine exhaust temperature				
G	Oxides of nitrogen				
н	Measurement by AIRCRAFT Measurement at NAVAIREWOLD Date of measurement 19 Marce Engine S/N GG018 Test Cell 20, single point JP-5 fuel.	RKFAC NORTH ISLAND AY 1977			ne .

A	LM2500	8415 RPM		File LM2501K	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 in h = 0.01070 h _{sd} = 0.00607		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CH ₄ Oxygen % Nitrogen % Water %	1.33 sd m 45.4 sd m m mC 5.6 w	44.5 1.4 5.7 19.20	1.8 1.8 1.31 1.29 45.6 44.9 44.2 43.5 1.4 1.4 5.7 5.6 19.08 18.78 79.00 77.74 2.19	0.28 3260.89 11.85 11.48 0.37 0.44 0.52
D	Sulfur dioxide, calc.		- v = -		0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			372	
F	K = 0.9781 F/A = 0.006116 Combustion efficiency = 9 Engine speed = 8415 rpm Engine exhaust temperatur			·	
G	EMISSION RATE (pounds of for a fuel flow rate of 7 Carbon monoxide Carbon dioxide 24 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	470 pounds per hou 2.12 358.85 88.55			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 19 M Engine S/N GG018 Test Cell 20, single poin JP-5 fuel.	RKFAC NORTH ISLAND AY 1977		e exhaust plane	

A	LM2500	8643 RPM		File L	.M2501L	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 in h = 0.01070 h _{sd} = 0.00607		m = 1 n = 2 η =		
	CONSTITUENT		T CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.52 sd 63.7 sd	1.8 1.51 64.4 62.4 2.0 8.8 18.94 79.54	1.8 1.50 64.0 62.0 2.0 8.8 18.83 79.06	1.8 1.47 62.9 60.9 2.0 8.6 18.50 77.67 2.35	0.25 3250.35 14.51 14.05 0.46 0.60 0.69
D	Sulfur dioxide, calc.			<u>-</u>		0.40
Ε	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				461	
F	<pre>K = 0.9765 F/A = 0.007008 Combustion efficiency = 99 Engine speed = 8643 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of conformation from formation for a fuel flow rate of 91) Carbon monoxide Carbon dioxide 296 Oxides of nitrogen 1: Hydrocarbons, CHy/R Hydrocarbons, Cl.4 Sulfur dioxide	30 pounds per hou 2.28 75.70 32.45				
н	Measurement by AIRCRAFT EMEASUREMENT at NAVAIREWORD Date of measurement 19 MAYENGINE S/N GG018 Test Cell 20, single point JP-5 fuel.	KFAC NORTH ISLAND Y 1977			st plane.	

Α	LM2500	8752 RPM		File LM2501N	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 66°F RH = 50% B = 29.98 in h = 0.010700 h = 0.00607		m = 13.0 n = 23.4 η = 0.95	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.58 sd n 73.0 sd n	1.57 73.8 7 71.5 7 2.3 7.1 18.86 1	0.9 0.9 1.56 1.53 3.4 72.1 1.1 69.8 2.3 2.3 7.0 6.9 8.75 18.41 9.08 77.65 2.40	0.13 3248.31 15.98 15.48 0.50 0.46 0.53
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			509	
F	K = 0.9760 F/A = 0.007287 Combustion efficiency = 9 Engine speed = 8752 rpm Engine exhaust temperatur				
G	EMISSION RATE (pounds of for a fuel flow rate of 1 Carbon monoxide Carbon dioxide 32 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	0080 pounds per ho 1.27 743.01 161.12			
H	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 19 M Engine S/N GG018 Test Cell 20, single poin JP-5 fuel.	RKFAC NORTH ISLAND AY 1977		exhaust plane	

А	T53-L-11D	GROUND IDLE		File	T53001I	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28	T = 78°F RH = 46% B = 29.83 in h = 0.01500 h _{sd} = 0.00607)5	m = n = η =		
	CONSTITUENT			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	3.14 sd 15.6 sd	518.7 3.12 15.8 15.3 0.5 .937.7 16.71 80.10	3.10 15.7 15.2 0.5	497.1 2.99 15.2 14.7 0.5 1856.9 16.01 76.77 4.17	31.51 2979.79 1.58 1.53 0.05 58.09 67.41
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				55	
F	<pre>K = 0.9583 F/A = 0.015705 Combustion efficiency = 93 Shaft horsepower = 35 Engine speed = 42 percent Engine exhaust temperature</pre>	rpm				
G	EMISSION RATE (pounds of of for a fuel flow rate of 14 Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide					
Н	Measurement by AIRCRAFT I Measurement at MCAS CAMP Date of measurement 26 AU Engine S/N L-E 12771 Test stand, single point p JP-5 fuel.	ENVIRONMENTAL SUPE PENDLETON IGUST 1975				

A	T53-L-11D	FLIGHT IDLE	File T53001B	· · · · · · · · · · · · · · · · · · ·
8	J = -0.07 $L = -0.0006$ $L' = 0.14$ $M = -0.00626$ $M' = 0.28$	T = 78°F RH = 46% B = 29.83 in. Hg h = 0.015005 h _{sd} = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONCI Measured dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
C	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.60 sd 2.58 19.8 sd 20.1 19.4 0.6	2.57 2.49 19.9 19.3 19.3 18.7 0.6 0.6 355.7 344.6	37.79 3119.75 2.53 2.45 0.08 13.57 15.75
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% o Oxides of nitrogen at 3% o		83	
F	<pre>K = 0.9628 F/A = 0.012443 Combustion efficiency = 97 Shaft horsepower = 110 Engine speed = 62 percent Engine exhaust temperature</pre>	rpm		
G				
н	Measurement by AIRCRAFT E. Measurement at MCAS CAMP Date of measurement 26 AU Engine S/N L-E 12771 Test stand, single point p JP-5 fuel.	PENDLETON GUST 1975		

А	T53-L-11D	N	IORMAL	RATED		File T	Γ53001N	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28	1	h = (05	m = 1 n = 2 η =		
	CONSTITUENT		Measure			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppmC % %	186.0 3.79 71.5 20.4	sd sd	126.5 3.77 72.5 70.3 2.3 21.4 15.86 80.35	2.3 21.3	120.6 3.59 69.2 67.0 2.2 20.4 15.12 76.59 4.67	6.83 3198.31 6.43 6.23 0.20 0.57 0.66
D	Sulfur dioxide, calc.			_				0.40
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3						213	
F	<pre>K = 0.9533 F/A = 0.017618 Combustion efficiency = Shaft horsepower = 410 Engine speed = 95 perce Engine exhaust temperate</pre>	ent rpm						
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		ounds po 40 91 15 37 43	-				
н	Measurement by AIRCRAI Measurement at MCAS CA Date of measurement 26 Engine S/N L-E 12771 Test stand, single poin JP-5 fuel.	AMP PEN 5 AUGUS'	DLETON T 1975					

A	T53-L-11D	MILITARY		File T53001M	
В	J = -0.07 $L = -0.0006$ $L' = 0.14$ $M = -0.00626$ $M' = 0.28$	T = 78°F RH = 46% B = 29.83 in. h = 0.015005 h = 0.00607	Нд	m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT	EXHAUST Measured	CONCENTRATI Calcul dry sem	ated i- wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 79.9 sd ppm ppm ppmC 10.6 w	78.6 78.	25 4.06 6 77.0 1 74.6 5 2.4 1 10.6	3.34 3201.57 6.34 6.14 0.20 0.26 0.30
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at :			211	
F	<pre>K = 0.9491 F/A = 0.019933 Combustion efficiency = 569 Shaft horsepower = 569 Engine speed = 98 perce Engine exhaust tempera</pre>	ent rpm			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		ar)		
н	Measurement by AIRCRA Measurement at MCAS Con Date of measurement 20 Engine S/N L-E 12771 Test stand, single point JP-5 fuel.	AMP PENDLETON 5 AUGUST 1975			

A	T53-L-11D	TAKEOFF		File 1	T53001T	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28	T = 78°F RH = 46% B = 29.83 in h = 0.01500 h _{sd} = 0.00607	5	m = n = η = η = η		
	CONSTITUENT		T CONCEN (dry	TTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	4.23 sd 96.1 sd	79.6 4.21 97.6 94.5 3.1 11.4 15.27 80.50	79.1 4.19 97.0 93.9 3.1 11.3	75.6 4.00 92.7 89.7 2.9 10.8 14.50 76.45 5.03	3.85 3201.13 7.75 7.51 0.24 0.27 0.32
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				258	
F	<pre>K = 0.9497 F/A = 0.019616 Combustion efficiency = 99 Shaft horsepower = 600 Engine speed = 100 percent Engine exhaust temperature</pre>	rpm				
	EMISSION RATE (pounds of of for a fuel flow rate of 69					<u> </u>
G	Carbon monoxide Carbon dioxide 22 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	2.66 208.78 5.35 0.19 0.22 0.28				
н	Measurement by AIRCRAFT E Measurement at MCAS CAMP Date of measurement 26 AU Engine S/N L-E 12771 Test stand, single point p JP-5 fuel.	PENDLETON IGUST 1975				

A	T56-A-16	LOW SP	EED GF	ROUND IDLE	File	T56001I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	RH = B =	97°F 15% 29.95 0.008 0.006	858	n =	13.0 23.4 0.95	
	CONSTITUENT	Measu		UST CONCEN' C. dry	TRATION alculated semi- dry	l wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	206.4 % 1.3 ppm 14.4 ppm ppm ppm 259.0 % 19.1 %	7 sd sd w	204.3 1.36 14.6 14.1 0.5 264.5	203.1 1.35 14.5 14.0 0.5 262.9 19.01 79.01	200.1 1.33 14.3 13.8 0.4 259.0 18.73 77.85 2.06	30.11 3149.25 3.53 3.41 0.11 19.24 22.32
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3					116 120	
F	K = 0.9794 F/A = 0.006523 Combustion efficiency = Shaft horsepower = 130 Engine speed = 9964 rpm Engine exhaust temperat						
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	18.04 1886.40 2.11 11.52					
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 23 Engine S/N 102138 Test Cell 11, single po JP-5 fuel.	WORKFAC ALAM JUNE 1976	EDA				

Α	T56-A-16	HIGH SPEED GROUND IE	DLE File T56001B	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.94 in. Hg h = 0.008860 h = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONC Measured dry	CENTRATION Calculated semi-wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.01 sd 1.00 18.4 sd 18.6 18.0 0.6	1.00 0.98 18.5 18.3 17.9 17.7 0.6 0.6 11.8 11.7 3 19.51 19 29	5.65 3275.53 6.35 6.15 0.20 1.22 1.42
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% o Oxides of nitrogen at 3% o		198 196	
F	K = 0.9827 F/A = 0.004629 Combustion efficiency = 99 Shaft horsepower = 245 Engine speed = 13485 rpm Engine exhaust temperature			
G	EMISSION RATE (pounds of conformation for a fuel flow rate of 75) Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide			
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 23 JU Engine S/N 102138 Test Cell 11, single point JP-5 fuel.	KFAC ALAMEDA NE 1976		

Α	T56-A-16	FLIGH	IT ID	LE		File T	56001C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	RH B h	- C		3	m = 1 n = 2 η =		
	CONSTITUENT	Mea	sure		T CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	% 1 ppm 20 ppm ppm ppmC 10	. 0	sd sd sd w	24.1 1.10 21.0 20.4 0.7 10.2 19.49 79.40	23.9 1.09 20.9 20.2 0.7 10.1 19.38 78.92	23.6 1.08 20.6 20.0 0.7 10.0 19.14 77.95 1.82	4.54 3268.50 6.52 6.32 0.21 0.95 1.10
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at Oxides of nitrogen at						205 207	
F	K = 0.9818 F/A = 0.005096 Combustion efficiency Shaft horsepower = 510 Engine speed = 13380 r Engine exhaust tempera	pm	°F	•				
	EMISSION RATE (pounds for a fuel flow rate o							
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	3.80 2732.46 5.45 0.79 0.92 0.33						
Н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N 102138 Test Cell 11, single po JP-5 fuel.	EWORKFAC AL 3 JUNE 1976	AMEI	A				

A	T56-A-16	75%	F	ile T56001D	
8	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.86 in. h = 0.008884 h = 0.00607	Hg n	= 13.0 = 23.4 = 0.95	
	CONSTITUENT	EXHAUST Measured	CONCENTRATIO Calcula dry semi dry	ted - wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %		4.2 4.2 2.06 2.0 60.4 60.1 58.5 58.2 1.9 1.9 3.4 3.4 18.20 18.0 79.74 79.2	4 2.00 58.8 57.0 1.9 3.3	0.42 3232.84 9.93 9.62 0.31 0.17 0.19
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or			327 318	
F	<pre>K = 0.9735 F/A = 0.009577 Combustion efficiency = 99 Shaft horsepower = 3550 Engine speed = 13820 rpm Engine exhaust temperature</pre>				
G		96 pounds per hour 0.84	•		
н	Measurement by AIRCRAFT EN Measurement at NAVAIREWORK Date of measurement 23 JUN Engine S/N 102138 Test Cell 11, single point JP-5 fuel.	KFAC ALAMEDA NE 1976		ck.	

A	T56-A-16	100%		File T56001E	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.85 in h = 0.00888 h _{sd} = 0.00607	7	$m = 13.0 n = 23.4 \eta = 0.95$	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x pp Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.14 sd m 64.0 sd m m mC 2.5 w	2.13 64.8 62.7 2.0 2.6 18.11 1	7.0 6.8 2.11 2.07 4.4 63.0 2.4 61.0 2.0 2.0 2.6 2.5 8.00 17.62 9.28 77.60 2.71	0.68 3230.89 10.29 9.97 0.32 0.12 0.14
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			340 330	
F	K = 0.9729 F/A = 0.009904 Combustion efficiency = 9 Shaft horsepower = 3890 Engine speed = 13820 rpm Engine exhaust temperatur				
G	EMISSION RATE (pounds of for a fuel flow rate of 2 Carbon monoxide Carbon dioxide 6 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	136 pounds per hou 1.45 901.18 21.99			
Н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 23 J Engine S/N 102138 Test Cell 11, single poin JP-5 fuel.	RKFAC ALAMEDA UNE 1976		stack.	

A	T56-A-16	MILITARY		File T56	001M
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 97°F RH = 15% B = 29.86 in h = 0.00888 h = 0.00607	4	$m = 13.$ $n = 23.$ $\eta = 0.$	4
	CONSTITUENT		T CONCENTR Cal dry	culated.	EMISSION INDEX wet
С	Carbon monoxide processing control of the control o	2.21 sd om 67.1 sd om om omC 2.9 w	65.8 2.1 3.0 18.01	65.4 2.1 3.0 17.90 1	6.8 2.13 3229.31 10.45 34.0 2.1 2.1 0.33 2.9 0.14 0.16 7.51 7.58 2.77
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			34 31	
F	K = 0.9723 F/A = 0.010231 Combustion efficiency = 9 Shaft horsepower = 4090 Engine speed = 13820 rpm Engine exhaust temperature				
	EMISSION RATE (pounds of for a fuel flow rate of 2				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CH _y /x Hydrocarbons, CH ₄ Sulfur dioxide	1.45 165.85 23.18 0.31 0.35 0.89			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 23 J Engine S/N 102138 Test Cell 11, single poir JP-5 fuel.	RKFAC ALAMEDA UNE 1976			

A	T58-GE-8F	IDLE			File T58A65	 51
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	I	56°F 29.81 in. 0.015195 0.00607	Нg	$ \begin{array}{r} m = 13.0 \\ n = 23.4 \\ \eta = 0.95 \end{array} $	
	CONSTITUENT	Measu			TION ulated emi- we dry	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water		2 sd w w 16	1.01 5.4 5.2 0.2 35.6 162	5.4 5. 5.2 5. 0.2 0. 5.7 1595. 9.39 19. 8.88 77.	99 2569.31 3 1.43 1 2 0.05 6 130.42 151.34
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at Oxides of nitrogen at				49	
F	<pre>K = 0.9755 F/A = 0.005961 Combustion efficiency Shaft horsepower = 15 Engine speed = 15016 r Engine exhaust tempera</pre>	рm				
	EMISSION RATE (pounds for a fuel flow rate o			r)		
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	23.55 339.15 0.19 17.21 19.98 0.05				
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 7 Engine S/N 271178 Test Cell 12, single p JP-5 fuel.	EWORKFAC NORT JUNE 1979	H ISLAND		exhaust pl	ane .

Α	T58-GE-8F	HIGH IDLE		File T58A55E	3
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	DEW = 56°F B = 29.81 : h = 0.015: h _{sd} = 0.0066	195	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		UST CONCE	NTRATION Calculated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.08 sd 5.8 w	929.6 1.07 6.0 5.8 0.2 1034.2 19.45 79.38	923.9 906.5 1.07 1.0 6.0 5.9 5.8 5.7 0.2 0.2 1027.9 1008.5 19.33 18.9 78.90 77.4 2.4	5 2760.33 1.62 1.57 0.05 83.67 97.09
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			53	
F	<pre>K = 0.9752 F/A = 0.005873 Combustion efficiency = 88 Shaft horsepower = 27 Engine speed = 16987 rpm Engine exhaust temperature</pre>				
G	Carbon dioxide 4 Oxides of nitrogen Hydrocarbons, $CH_{y/x}$ Hydrocarbons, CH_{4}	9 pounds per hou 22.70 11.29 0.24 12.47			-
н	Measurement by AIRCRAFT E. Measurement at NAVAIREWORD Date of measurement 7 JUN Engine S/N 271178 Test Cell 12, single point JP-5 fuel.	KFAC NORTH ISLA E 1979	ND		ne .

A	T58-GE-8F	APPROACH	File T58A56C	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	DEW = 56°F B = 29.81 in. Hg h = 0.015195 h _{sd} = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONCER Measured dry	NTRATION Calculated semi- wet dry	EMISSION INDEX
C	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 153.2 sd 150.3 % 1.79 sd 1.78 ppm 22.7 w 23.7 ppm 0.7 ppmC 19.1 w 19.7 % 18.57 % 79.64	149.4 145.8 1.77 1.72 23.6 23.0 22.8 22.3 0.7 0.7 19.6 19.1 18.45 18.01 79.16 77.23 3.02	17.28 3210.80 4.47 4.33 0.14 1.12 1.30
D	Sulfur dioxide, calc.			0.40
E		3% oxygen, calc.(ppm wet) 3% oxygen, meas.(ppm wet)	140	
F	<pre>K = 0.9698 F/A = 0.008346 Combustion efficiency Shaft horsepower = 918 Engine speed = 24578 r Engine exhaust tempera</pre>	pm		
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen	of constituent per hour) f 581 pounds per hour 10.04 1865.47 2.60		
	Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	0.65 0.75 0.23		
н	Measurement at NAVAIR Date of measurement 7 Engine S/N 271178			AFSO 09-20-1987

A	T58-GE-8F	CRUISE		File T58A31D	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	DEW = 56°F B = 29.80 in h = 0.01520 h = 0.00607	1	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.85 sd m 24.5 w m m m	1.84 25.6 24.8 0.8 14.5	26.1 123.0 1.83 1.78 25.4 24.8 24.6 24.0 0.8 0.8 14.5 14.1 18.38 17.92 79.18 77.21 3.07	14.13 3214.97 4.68 4.53 0.15 0.80 0.93
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			147	
F	K = 0.9693 F/A = 0.008613 Combustion efficiency = 9 Shaft horsepower = 1027 Engine speed = 24983 rpm Engine exhaust temperatur				
	EMISSION RATE (pounds of for a fuel flow rate of 6				
G	Carbon monoxide Carbon dioxide 2 Oxides of nitrogen Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	8.86 015.79 2.94 0.50 0.58 0.25			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 6 JU Engine S/N 271178 Test Cell 12, single poin JP-5 fuel.	RKFAC NORTH ISLAND NE 1979		e exhaust plane	

A	T58-GE-8F	MAXIMUM CONTIN	IUOUS	File 1	758A58N	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	DEW = 56°F B = 29.81 in h = 0.01519 h = 0.00607		m - η - η - η -		
	CONSTITUENT			NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.95 sd n 27.0 w n	122.7 1.94 28.2 27.4 0.9 14.0 18.35 79.70	122.0 1.93 28.1 27.2 0.9 14.0 18.24 79.21	118.9 1.88 27.4 26.5 0.9 13.6 17.77 77.18 3.15	12.96 3214.12 4.90 4.75 0.15 0.73 0.85
D	Sulfur dioxide, calc.					0.40
Ε	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				155	
F	<pre>K = 0.9685 F/A = 0.009078 Combustion efficiency = 99 Shaft horsepower = 1159 Engine speed = 25592 rpm Engine exhaust temperature</pre>					
	EMISSION RATE (pounds of of for a fuel flow rate of 68					
G	Carbon monoxide Carbon dioxide 22 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	8.88 201.67 3.36 0.50 0.58 0.27				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 7 JUN Engine S/N 271178 Test Cell 12, single point JP-5 fuel.	KFAC NORTH ISLAND IE 1979			st plane.	

A	T58-GE-8F	TAKE	OFF		File 1	Г58A76M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	B h	- 56°F - 29.81 : - 0.015: - 0.0060	195	m = n = η =		
	CONSTITUENT	Mea	EXHAU	JST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	2 ppm 32 ppm ppm	.4 sd .12 sd .7 w	92.9 2.11 34.3 33.2 1.1 8.3 18.13 79.76	1.1 8.2	89.8 2.04 33.1 32.1 1.0 8.0 17.53 77.13 3.30	9.03 3217.15 5.47 5.30 0.17 0.40 0.46
D	Sulfur dioxide, calc.						0.40
ε	Oxides of nitrogen at Oxides of nitrogen at					174	
F	K = 0.9670 F/A = 0.009854 Combustion efficiency Shaft horsepower = 130 Engine speed = 26689 to Engine exhaust temperate	50 cpm	°F				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CH _y /x Hydrocarbons, CH ₄ Sulfur dioxide						
н	Measurement by AIRCRA Measurement at NAVAII Date of measurement Engine S/N 271178 Test Cell 12, single JP-5 fuel.	REWORKFAC NO 7 JUNE 1979	RTH ISLAI	ΝD		st plane	AFSO 09-30-1987

Α	T64-GE-6B	IDLE	File T640011	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00185 M' = 0.28	T = 57°F RH = 64% B = 30.09 h = 0.000 h _{sd} = 0.000	9929	
	CONSTITUENT		AUST CONCENTRATION Calculated dr, semi- wet dry	EMISSION INDEX
C	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 417.2 sd % 1.39 sd ppm 11.5 sd ppm ppm ppm ppmC 182.0 w	397.5 395.1 388.7 1.38 1.37 1.35 11.6 11.6 11.4 11.3 11.2 11.0 0.4 0.4 0.4 186.1 185.0 182.0 19.08 18.97 18.66 79.50 79.02 77.75 2.20	57.27 3124.03 2.75 2.67 0.09 13.24 15.36
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at Oxides of nitrogen at			
ŕ	K = 0.9780 F/A = 0.006671 Combustion efficiency Shaft horsepower = 119 Engine speed = 13459 r Engine exhaust tempera	.bш		
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x	18.38 1002.81 0.88 4.25		
	Hydrocarbons, CH ₄ Sulfur dioxide	4.93 0.13		
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 1 Engine S/N 262265 Test Cell 9, single po JP-5 fuel.	EWORKFAC NORTH ISL 0 JANUARY 1974		

A	T64-GE-6B	75% hp		File 1	T64001B	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00185 M' = 0.28	T = 57°F RH = 64% B = 30.09 in h = 0.00992 h = 0.00607	9	m = n = η =		
	. CONSTITUENT		T CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
c	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 61.7 sd 1.78 sd ppm 40.3 sd ppm ppm ppm 7.0 w	36.7 1.77 40.8 39.5 1.3 7.2 13.59 79.63	36.5 1.76 40.5 39.3 1.3 7.1 18.48 79.15	35.8 1.72 39.8 38.5 1.3 7.0 18.12 77.64 2.50	4.27 3234.24 7.80 7.55 0.25 0.41 0.48
D	Sulfur dioxide, calc.					0.40
Ε		3% oxygen, calc.(ppm 3% oxygen, meas.(ppm			253	
F	K = 0.9750 F/A = 0.008240 Combustion efficiency Shaft horsepower = 20 Engine speed = 16650 Engine exhaust temper	52 rpm				
		of constituent per ho of 1063 pounds per hou				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	4.54 3437.99 8.29 0.44 0.51 0.43				
Н	Measurement at NAVAI Date of measurement Engine S/N 262265	AFT ENVIRONMENTAL SUPEREWORKFAC NORTH ISLAND 10 JANUARY 1974 oint probe 40 feet beh	•		t plane.	

А	T64-GE-6B	NORMAL RATED		File T64001N	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00185 M' = 0.28	T = 57°F RH = 64% B = 30.09 in h = 0.009929 h _{sd} = 0.00607	_	m = 13.0 n = 23.4 $\eta = 0.95$	_
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide ppr Carbon dioxide % Oxides of nitrogen ppr Nitric oxide ppr Nitrogen dioxide ppr Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.96 sd n 51.1 sd n	1.95 51.7 5 50.1 4 1.6 9.2 18.35 1	5.0 24.5 1.93 1.90 1.4 50.3 9.8 48.8 1.6 1.6 9.2 9.0 8.24 17.86 9.22 77.58 2.65	2.66 3231.12 8.97 8.69 0.28 0.48
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			293	
F	K = 0.9735 F/A = 0.009076 Combustion efficiency = 99 Shaft horsepower = 2679 Engine speed = 17096 rpm Engine exhaust temperature				
G	Oxides of nitrogen				
н	Measurement by AIRCRAFT I Measurement at NAVAIREWOR Date of measurement 10 JA Engine S/N 262265 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAND NUARY 1974		exhaust plane.	

Α	T64-GE-6B	MILITARY		File	Γ64001M	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00185 M' = 0.28	T = 57°F RH = 64% B = 30.09 i h = 0.0099 h = 0.0060	29	m = n = η =		
	CONSTITUENT		JST CONCEN C dry	TRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm 43.7 sd 2.05 sd ppm 58.4 sd ppm ppm ppm ppmC 10.0 w	18.5 2.04 59.1 57.2 1.9 10.3 18.23 79.73	18.4 2.02 58.8 56.9 1.9 10.2 18.12 79.25	18.0 1.98 57.5 55.7 1.8 10.0 17.73 77.55 2 73	1.87 3229.91 9.80 9.49 0.31 0.51
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at Oxides of nitrogen at				321	
F	K = 0.9727 F/A = 0.009493 Combustion efficiency Shaft horsepower = 300 Engine speed = 17544 Engine exhaust temper	04 rpm				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide					
	Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	13.43 0.70 0.81 0.55				
н	Measurement by AIRCR Measurement at NAVAI Date of measurement Engine S/N 262265 Test Cell 9, single po JP-5 fuel.	REWORKFAC NORTH ISLAN 10 JANUARY 1974	1D		t plane.	

A	T64-GE-6B	MAXIMUM CONTINUOUS	File T64001X	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00185 M' = 0.28	T = 57°F RH = 64% B = 30.09 in. Hg h = 0.009929 h _{sd} = 0.00607	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONC Measured dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
C	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	om 40.8 sd 15.2 2.10 sd 2.09 om 61.7 sd 62.5 om 2.0 om 2.0 om 11.3 4 18.16 79.75	2.07 2.03 62.1 60.7 60.1 58.8 2.0 1.9 11.2 11.0	1.50 3229.15 10.11 9.79 0.32 0.55 0.64
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%		331	
F	K = 0.9723 F/A = 0.009726 Combustion efficiency = Shaft horsepower = 3167 Engine speed = 17761 rpm Engine exhaust temperatu			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide			
Н	Measurement at NAVAIREW Date of measurement 10 Engine S/N 262265			

Α	T64-GE-413	IDLE	File T64031I	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00281 M' = 0.28		$n = 23.4$ 6 in. Hg $\eta = 0.95$	
	CONSTITUENT	EXF Measured	HAUST CONCENTRATION Calculated dry semi- wet dry	EMISSION INDEX
C	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen Nitrogen	pm 380.5 sd 1.37 sd pm 10.8 sd pm pm pm 234.7 w	1.36 1.35 1.33 10.9 10.9 10.7 10.6 10.5 10.4 0.3 0.3 0.3	51.83 3120.68 2.62 2.54 0.08 17.28 20.05
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			
F	K = 0.9790 F/A = 0.006582 Combustion efficiency = Shaft horsepower = 64 Engine speed = 11985 rpm Engine exhaust temperatu			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide			
н	Engine S/N 264274	ORKFAC NORTH ISL JANUARY 1974		

A	T64-GE-413	759	% HP	·		File 1	T64031B	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00281 M' = 0.28	T RH B h h	= 5 = 3	7°F 9% 0.16 ir 0.00912 0.00607	4	m = η = η =		
	CONSTITUENT		easur		T CONCENT Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
C	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	%	47.8 1.90 47.1 6.3	sd sd	17.8 1.89 47.7 46.2 1.5 6.5	17.7 1.88 47.4 45.9 1.5 6.4 18.32 79.20	17.4 1.84 46.5 45.0 1.5 6.3 17.96 77.66 2.53	1.94 3234.40 8.54 8.27 0.27 0.35 0.40
D	Sulfur dioxide, calc.					·		0.40
E	Oxides of nitrogen at Oxides of nitrogen at						279	
F	<pre>K = 0.9747 F/A = 0.008791 Combustion efficiency Shaft horsepower = 269 Engine speed = 16875 r Engine exhaust tempera</pre>	19 :pm	19°F					
	EMISSION RATE (pounds for a fuel flow rate of							
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	2.50 4162.67 10.99 0.45 0.52						
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N 264274 Test Cell 9, single po JP-5 fuel.	EWORKFAC 8 JANUARY	NORTH	I ISLANI)		t plane.	

A	T64-GE-413	NORMAL RATED		File T64031N	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00281 M' = 0.28	T = 57°F RH = 59% B = 30.16 in. h = 0.009124 h = 0.00607	Нg	m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT	EXHAUST Measured	dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.09 sd 58.6 sd 5 C 6.6 w	2.08 5 59.3 5 7.4 5 1.9 6.8	2.0 11.8 2.06 2.02 9.0 57.7 7.1 55.9 1.9 1.8 6.7 6.6 8.06 17.68 9.26 77.60 2.69	1.20 3230.58 9.65 9.34 0.30 0.33
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% o Oxides of nitrogen at 3% o			317	
F	<pre>K = 0.9731 F/A = 0.009675 Combustion efficiency = 99 Shaft horsepower = 3345 Engine speed = 17274 rpm Engine exhaust temperature</pre>				
G			-)		
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 28 JA Engine S/N 264274 Test Cell 9, single point JP-5 fuel.	KFAC NORTH ISLAND NUARY 1974		exhaust plane.	

A	T64-GE-413	INTERMEDIATE	F	File T64031M	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00281 M' = 0.28	T = 57°F RH = 59% B = 30.16 in. 1 h = 0.009124 h = 0.00607	n	= 13.0 = 23.4 = 0.95	
	CONSTITUENT	EXHAUST (Measured	CONCENTRATIO Calcula dry semi dry	ted - wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	2.24 sd pm 71.1 sd 7 pm 6 pm pm pm 7.3 w	7.3 7.3 2.23 2.2 2.0 71.6 9.7 69.3 2.3 2.3 7.5 7.5 7.97 17.8 9.80 79.3	1 2.16 70.0 67.8 2.2 7.3	0.67 3227.98 10.92 10.57 0.34 0.34
D	Sulfur dioxide, calc.				0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			360	
F	K = 0.9719 F/A = 0.010373 Combustion efficiency = Shaft horsepower = 3779 Engine speed = 17472 rpm Engine exhaust temperatu				
G)		
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 28 Ergine S/N 264274 Test Cell 9, single poin JP-5 fuel.	ORKFAC NORTH ISLAND JANUARY 1974		aust plane.	

А	T64-GE-413	MAXIMUM		File T64031X	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00281 M' = 0.28	T = 57°F RH = 59% B = 30.16 in. h = 0.009124 h _{sd} = 0.00607		m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT	EXHAUST Measured	dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH4 Oxygen Nitrogen	pm 38.4 sd 2.31 sd pm 76.7 sd pm pm pm 5.9 w	2.30 77.7 75.2 2.4 6.1 17.88	5.5 5.4 2.28 2.23 7.2 75.4 4.8 73.1 2.4 2.4 6.0 5.9 7.77 17.36 9.34 77.53 2.87	0.49 3227.08 11.42 11.06 0.36 0.27 0.31
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			378	
F	K = 0.9713 F/A = 0.010697 Combustion efficiency = Shaft horsepower = 3937 Engine speed = 17589 rpm Engine exhause temperatu				
G					
Н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 28 Engine S/N 264274 Test Cell 9, single poin JP-5 fuel.	ORKFAC NORTH ISLAND JANUARY 1974		exhaust plane.	

Α	T64-GE-415	IDLE		File	Г64051І	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00578 M' = 0.28	T = 64°F RH = 56% B = 29.87 i h = 0.0112 h = 0.0060	16	m = n = η =		
	CONSTITUENT		dry	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.40 sd m 9.1 sd m	530.5 1.39 9.2 8.9 0.3 352.0 19.06 79.50	18.94	518.1 1.36 9.0 8.7 0.3 343.8 18.61 77.64 2.34	74.33 3059.84 2.12 2.05 0.07 24.35 28.25
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				69	
F	K = 0.9766 F/A = 0.006860 Combustion efficiency = 9 Shaft horsepower = 41 Engine speed = 11755 rpm Engine exhaust temperatur					
G	EMISSION RATE (pounds of for a fuel flow rate of 2 Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	69 pounds per hou 20.00 823.10 0.57				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 23 O Engine S/N 264453 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAN CTOBER 1975	ID		t plane.	

Α	T64-GE-415	75%	File	T64051B	
В	J0.07 L0.0006 L' - 0.14 M0.00578 M' - 0.28	T = 64°F RH = 56% B = 29.87 ir h = 0.01121 h = 0.00607	n = η =	13.0 23.4 0.95	
	CONSTITUENT		T CONCENTRATION Calculated dry semi- dry	1 -	MISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen	om 75.2 sd 2.51 sd om 59.2 sd om om om om om 3.2 w	25.6 25.4 2.49 2.48 60.0 59.6 58.1 57.7 1.9 1.9 3.3 3.3 17.60 17.50 79.89 79.41	24.8 2.41 58.0 56.2 1.8 3.2 17.03 77.30 3.24	2.10 3221.31 8.09 7.84 0.26 0.13 0.16
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			266	
F	K = 0.9676 F/A = 0.011636 Combustion efficiency = 9 Shaft horsepower = 3066 Engine speed = 17170 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of for a fuel flow rate of flow				
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 23 (Engine S/N 264453 Test Cell 9, single point JP-5 fuel.	ORKFAC NORTH ISLAND OCTOBER 1975		t plane.	

А	T64-GE-415	NORMAL RATED		File T64051N	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00578 M' = 0.28	T = 64°F RH = 56% B = 29.87 in. h = 0.011216 h = 0.00607		m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT			ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.72 sd n 73.7 sd n	2.70 74.7 72.3 2.4 2.1	19.7 19.1 2.69 2.61 74.2 72.1 71.9 69.8 2.3 2.3 2.1 2.0 17.22 16.73 79.48 77.23 3.42	1.50 3219.21 9.29 9.00 0.29 0.08 0.09
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			307	
F	K = 0.9658 F/A = 0.012609 Combustion efficiency = 99 Shaft horsepower = 3660 Engine speed = 17536 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of of for a fuel flow rate of 17) Carbon monoxide Carbon dioxide 55 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	730 pounds per hour 2.60 569.23			
н	Measurement by AIRCRAFT E Measurement at NAVAIREWOR Date of measurement 23 OC Engine S/N 264453 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAND CTOBER 1975			

A	T64-GE-415	MILITARY	F	ile T64051M	
8	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00578 M' = 0.28	T = 64°F RH = 56% B = 29.87 in h = 0.01121 h _{sd} = 0.00607	. Hg η	= 13.0 = 23.4 = 0.95	
	CONSTITUENT		T CONCENTRATION Calcula dry semi dry	ted - wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 69.2 sd 2.82 sd ppm 82.2 sd ppm ppm ppm ppm 7.5 v	17.7 17.6 2.80 2.7 83.3 82.8 80.7 80.2 2.6 2.6 7.8 7.7 17.19 17.0 80.00 79.5	9 2.70 80.4 77.8 2.5 7.5	1.29 3217.52 9.99 9.68 0.32 0.28 0.33
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 33 Oxides of nitrogen at 33			331	
F	K = 0.9650 F/A = 0.013075 Combustion efficiency = Shaft horsepower = 4100 Engine speed = 17750 rps Engine exhaust temperate	n			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide	1916 pounds per hou 2.48			
	Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	6164.77 19.15 0.54 0.62 0.77			
Н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 23 Engine S/N 264453 Test Cell 9. single poin JP-5 fuel.	JORKFAC NORTH ISLAND OCTOBER 1975		aust plane.	

A	T64-GE-415	MAXIMUM RATED F	OWER	File To	64051X	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00578 M' = 0.28	T = 64°F RH = 56% B = 29.87 in. h = 0.011216 h _{sd} = 0.00607		$ \begin{array}{r} m = 1 \\ n = 2 \\ \eta = \end{array} $	3.4	
	CONSTITUENT	EXHAUST Measured		TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.87 sd 90.7 sd	20.4 2.85 91.9 89.0 2.9 5.5 17.12 80.02	20.3 2.84 91.4 88.5 2.9 5.5 17.01 79.54	19.7 2.75 88.7 85.9 2.8 5.3 16.51 77.18 3.55	1.47 3216.87 10.83 10.49 0.34 0.19
D	Sulfur dioxide, calc.		-			0.40
Ε	Oxides of nitrogen at 3% ox Oxides of nitrogen at 3% ox				359	
F	<pre>K = 0.9645 F/A = 0.013307 Combustion efficiency = 99. Shaft horsepower = 4372 Engine speed = 17910 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of co for a fuel rlow rate of 200 Carbon monoxide Carbon dioxide 644 Oxides of nitrogen 2	05 pounds per hour 2.94				
		0.39 0.45 0.80				
н	Measurement by AIRCRAFT EN Measurement at NAVAIREWORK Date of measurement 23 OCT Engine S/N 264453 Test Cell 9, single point p JP-5 fuel.	CFAC NORTH ISLAND COBER 1975			plane.	

А	T64-GE-7	IDLE		File 1	T64002I	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00082 M' = 0.28	T = 41°F RH = 64% B = 30.06 i h = 0.0054 h _{sd} = 0.0060	£67	m = η = η = η = η = η		
	CONSTITUENT		JST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen % Nitrogen % Water %	1.36 sd m 10.6 sd m m mC 194.3 w	358.2 1.35 10.7 10.4 0.3 197.7 19.13 79.49	356.0 1.34 10.7 10.3 0.3 196.5 19.01 79.01	352.0 1.33 10.5 10.2 0.3 194.3 18.79 78.10 1.74	52.84 3129.02 2.60 2.52 0.08 14.40 16.71
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				88	
F	K - 0.9826 F/A = 0.006517 Combustion efficiency = 9 Shaft horsepower = 81 Engine speed = 12196 rpm Engine exhaust temperatur					
	EMISSION RATE (pounds of for a fuel flow rate of 2					
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	13.84 819.80 0.68 3.77 4.38 0.10				
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 J Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAN ANUARY 1974	ND		t plane.	

Α	T64-GE-7	75% HORSEPOWER	File T64002B	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00082 M' = 0.28	T = 41°F RH = 64% B = 30.06 in. Hg h = 0.005467 h _{sd} = 0.00607	$m = 13.0 n = 23.4 \eta = 0.95$	
	CONSTITUENT	EXHAUST CO Measured	ONCENTRATION Calculated ry semi- wet dry	EMISSION INDEX
C	Carbon monoxide process of nitrogen dioxide process of nitrogen dioxide process of nitrogen process of nit	2.00 sd 1. m 51.1 sd 51. m 50 m 1 mC 5.6 w 5	.4 21.2 20.9 .99 1.97 1.94 .7 51.4 50.6 .1 49.8 49.0 .6 1.6 1.6 .7 5.7 5.6 .29 18.18 17.88 .71 79.23 77.91 2.26	2.21 3231.36 8.79 8.52 0.28 0.29 0.34
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			
F	<pre>K = 0.9774 F/A = 0.009259 Combustion efficiency = 9 Shaft horsepower = 2697 Engine speed = 16761 rpm Engine exhaust temperature</pre>			
G	Hydrocarbons, CHy/x	300 pounds per hour 2.88 200.77 11.43 0.38		
	Hydrocarbons, CH₄ Sulfur dioxide	0.44 0.52		
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAND ANUARY 1974		

A	T64-GE-7	NO	ORMAL RATED		File T	64002N	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00082 M' = 0.28	T RI B h	= 0.00546		$m = 1$ $n = 2$ $\eta = 2$	23.4	
	CONSTITUENT			T CONCEN' Ca dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC % % % %	35.7 sd 2.20 sd 63.5 sd	15.6 2.19 64.3 62.3 2.0 7.1 18.02 79.78	15.5 2.17 63.9 61.9 2.3 7.6 17.92 79.30	15.3 2.13 62.7 60.7 2.0 6.9 17.59 77.84 2.43	1.47 3227.62 9.92 9.61 0.31 0.33 0.38
D	Sulfur dioxide, calc.						0.40
Ε	Oxides of nitrogen at Oxides of nitrogen at					335	
F	K = 0.9757 F/A = 0.010190 Combustion efficiency Shaft horsepower = 372 Engine speed = 17365 r Engine exhaust tempera	9 pm	275°F				
	EMISSION RATE (pounds for a fuel flow rate o	f 1676 p	ounds per hou				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	2.4 5409.4 16.6 0.5 0.6 0.6	9 3 5 4				
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N 261033 Test Cell 9, single po JP-5 fuel.	EWORKFAC 9 JANUAR	NORTH ISLAND Y 1974			t plane.	

Δ,	T64-GE-7		INTERMEDIATE		File	T64002M	
æ	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00082 M' = 0.28		T = 41°F RH = 64% B = 30.06 h = 0.005 h _{sd} = 0.006	467		13.0 23.4 0.95	
	CONSTITUENT		EXHA Measured	UST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC %	35.7 sd 2.37 sd 75.0 sd	14.5 2.35 75.9 73.6 2.4 7.1 17.79 79.84	14.4 2.34 75.5 73.1 2.4 7.0 17.69 79.36	14.1 2.29 74.0 71.7 2.3 6.9 17.34 77.79 2.58	1.26 3224.58 10.87 10.53 0.34 0.30
D	Sulfur dioxide, calc.						0.40
Ē	Oxides of nitrogen at Oxides of nitrogen at					368	· -
F	<pre>K = 0.9742 F/A = 0.010981 Combustion efficiency Shaft horsepower = 372 Engine speed = 17365 n Engine exhaust tempera</pre>	29 cpm					
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocartors, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	2 5404 18 0 0	pounds per h .11 .40				
н	Measurement by AIRCRA Measurement at NAVAII Date of measurement 2 Engine S/N 261033 Test Cell 9, single po JP-5 fuel.	REWORKF 29 JANU	AC NORTH ISLA ARY 1974	MD		t plane.	

А	T64-GE-7	MAXIMUM		File T64002X	
8	J0.07 L0.0007 L' - 0.14 M0.00082 M' - 0.28	T = 41°F RH = 64% B = 30.06 in h = 0.00546 h _{sd} = 0.00607	7	m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT		,		EMISSION INDEX
С	Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp	om om omC 6.1 w	2.40 2 81.2 80 78.7 78 2.6 2 6.3 6	.4 15.1 .39 2.34 .7 79.1 .2 76.6 .5 2.5 .2 6.1 .62 17.26 .38 77.77 2.62	1.32 3223.70 11.38 11.02 0.36 0.26 0.31
D	Sulfur dioxide, calc.		· · · · · ·		0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			385	
F	K = 0.9738 F/A = 0.011214 Combustion efficiency = 9 Shaft horsepower = 3870 Engine speed = 17471 rpm Engine exhaust temperature				
G	EMISSION RATE (pounds of for a fuel flow rate of for a fuel flow flow rate of for a fuel flow flow rate of for a fuel flow flow flow rate of fuel flow flow flow flow flow flow flow flo	2.29 5580.22 19.70 0.46 0.53			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 S Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAND ANUARY 1974		xhaust plane.	

A	T64-GE-7	IDLE		File	T64003I	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00082 M' = 0.28	h = 0.0	6 in. Hg	n =	13.0 23.4 0.95	
į	CONSTITUENT		HAUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	2.09 sd m 19.1 sd m m nC 274.1 w	2.08	18.01	547.3 2.03 18.9 18.3 0.6 274.1 17.69 77.84 2.38	53.38 3105.69 3.02 2.93 0.10 13.19 15.31
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				104	
F	K = 0.9762 F/A = 0.010065 Combustion efficiency = 9 Shaft horsepower = 81 Engine speed = 12196 rpm Engine exhaust temperatur					
G	EMISSION RATE (pounds of for a fuel flow rate of 2 Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	62 pounds per 13.99				
Н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 J Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH IS ANUARY 1974	LAND		st plane	,

A	T64-GE-7	75% HORSEPOWER	₹	File To	64003B	
8	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00082 M' = 0.28	T = 41°F RH = 64% B = 30.06 in. h = 0.005467 h _{sd} = 0.00607		m = 1 n = 2 η =	3.4	
	CONSTITUENT			TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	3.06 sd 84.7 sd	30.9 3.04 85.9 83.1 2.7 6.8 16.86 80.09	30.7 3.02 85.3 82.6 2.7 6.8	29.9 2.95 83.1 80.5 2.6 6.6 16.33 77.55 3.16	2.08 3213.53 9.48 9.18 0.30 0.23 0.26
0	Sulfur dioxide, calc.					0.40
Ε	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of				323	
F	<pre>K = 0.9684 F/A = 0.014193 Combustion efficiency = 99 Shaft horsepower = 2697 Engine speed = 16761 rpm Engine exhaust temperature</pre>					
G	Hydrocarbons, CHy/x	00 pounds per hour 2.70				
н	Measurement by AIRCRAFT E Measurement at NAVAIREWORD Date of measurement 29 JAI Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	KFAC NORTH ISLAND NUARY 1974			t plane	

А	T64-GE-7	NORMAL RATED		File T64003N	
8	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00082 M' = 0.28	T = 41°F RH = 64% B = 30.06 in. h = 0.005467 h _{sd} = 0.00607		m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide procarbon dioxide carbon dioxide carbon dioxide procarbons, CHy/x procarbons, CH ₄ carbon carbons, CH ₄ carb	3.37 sd m 105.5 sd 1 m 1 m mC 8.2 w	3.35 .07.0 10 .03.6 10 3.4 8.5	9.5 18.9 3.33 3.24 6.3 103.3 3.0 100.1 3.4 3.3 8.4 8.2 6.34 15.88 9.71 77.45 3.42	1.19 3211.69 10.72 10.38 0.34 0.26 0.30
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			366	
F	K = 0.9658 F/A = 0.015623 Combustion efficiency = 9 Shaft horsepower = 3279 Engine speed = 17111 rpm Engine exhaust temperature				
	EMISSION RATE (pounds of for a fuel flow rate of 1				
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, Cdy/x Hydrocarbons, CH ₄ Sulfur dioxide	1.80 830.38 16.12 0.38 0.45 0.60			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 Engine S/N 261033 Test Cell 9, single point JP-5 fuel.	RKFAC NORTH ISLAND ANUARY 1974		exhaust plane	

A	T64-GE-7	INTER	MEDIATE		File	T64003M	<u>-</u>
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00082 M' = 0.28	RH B h	= 41°F = 64% = 30.06 : = 0.0054 = 0.0060	¥67	n =	13.0 23.4 0.95	
	CONSTITUENT		EXHAI sured	JST CONCEN C dry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen Nitrogen Water	% 3 ppm 126 ppm ppm	.9 sd .64 sd .9 sd	19.5 3.62 128.7 124.7 4.1 8.5		18.8 3.49 124.0 120.1 3.9 8.2 15.49 77.36 3.65	1.10 3209.59 11.93 11.55 0.38 0.24 0.27
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at 3					408	
F	K = 0.9635 F/A = 0.016870 Combustion efficiency = Shaft horsepower = 3729 Engine speed = 17365 rp Engine exhaust temperat	om	°F				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	1.84 5379.28 19.99					
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 29 Engine S/N 261033 Test Cell 9, single poi JP-5 fuel.	WORKFAC NO JANUARY 1	RTH ISLAN 974	ND		ıst plane.	

A	T64-GE-7	MAXIMUM		File T64003X	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00082 M' = 0.28	T = 41°F RH = 64% B = 30.06 i h = 0.0054 h = 0.0060	n. Hg	m = 13.0 m = 23.4 m = 0.95	
	CONSTITUENT		ST CONCENTRATIO Calculates dry sem	ated i- wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄ Oxygen	pm 48.8 sd % 3.75 sd pm 137.2 sd pm pm pmC 8.0 w	21.7 3.73 3.3 139.2 134.8 4.4 8.3 15.92 80.33 21.1 3.7 138.4 4.4 8.7 8.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9	71 3.59 4 134.0 0 129.8 4 4.2 3 8.0	1.19 3208.65 12.51 12.12 0.39 0.22 0.26
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			428	
F	<pre>K = 0.9626 F/A = 0.017378 Combustion efficiency = Shaft horsepower = 3870 Engine speed = 17471 rpm Engine exhaust temperatu</pre>				
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide				
н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 29 Engine S/N 261033 Test Cell 9, single poin JP-5 fuel.	ORKFAC NORTH ISLAN JANUARY 1974	D.	xhaust plane	

A	T76-G-12A	GROUND START	File T76001I	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00593 M' = 0.28	T = 63°F RH = 79% B = 29.84 in. Hg h = 0.015352 h _{sd} = 0.00607	$m = 13.0 n = 23.4 \eta = 0.95$	
	CONSTITUENT	Measured	ONCENTRATION Calculated ry semi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.84 sd 1. 23.5 sd 23. 23. 0 0 1.82.0 w 187.	.83 1.82 1.77 .8 23.6 23.0 .0 22.9 22.3 .7 0.7 0.7	28.29 3162.13 4.30 4.17 0.14 10.21 11.85
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			
F	K = 0.9691 F/A = 0.008710 Combustion efficiency = 98 Engine speed = 40500 rpm Engine exhaust temperature			
G	EMISSION RATE (pounds of of for a fuel flow rate of 18 Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	5.09 5.09 69.18 0.77		
Н	Measurement by AIRCRAFT I Measurement at MCAS CAMP Date of measurement 26 AU Engine S/N 000427 Test stand, single point p JP-5 fuel.	PENDLETON IGUST 1975		

Α	T76-G-12A	HIGH IDLE		File T76001B	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00593 M' = 0.28	T = 63°F RH = 79% B = 29.84 h = 0.01 h = 0.00	5352	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		AUST CONCENT Ca dry	TRATION Alculated semi- wet dry	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 323.4 sd 2.26 sd ppm 30.1 sd ppm ppm ppm ppmC 133.5 w	273.6 2.25 30.5 29.5 1.0 138.3 17.92 79.80	272.0 264.2 2.23 2.17 30.3 29.4 29.3 28.5 1.0 0.9 137.4 133.5 17.81 17.30 79.32 77.06 3.44	24.59 3170.73 4.50 4.36 0.14 6.13 7.12
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3			145	
F	K = 0.9656 F/A = 0.010654 Combustion efficiency = Engine speed = 40100 rp Engine exhaust temperate	m			
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	5.21 5.21 672.19 0.95			
н	Measurement by AIRCRAI Measurement at MCAS CA Date of measurement 26 Engine S/N 000427 Test stand, single poin JP-5 fuel.	MP PENDLETON AUGUST 1975			

Α	T76-G-12A	MILITAI	RY		File	Г76001M	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00593 M' = 0.28	RH -	63°F 79% 29.84 in 0.01539 0.00607	52	m = n = η =		
	CONSTITUENT	Measu		Concent Concent Concent	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	% 4.2 ppm 88.9 ppm ppm	sd 23 sd 9 sd	34.9 4.21 90.3 87.4 2.8 2.0 15.28 80.50	34.7 4.19 89.7 86.9 2.8 2.0 15.18 80.02	33.2 4.00 85.7 83.0 2.7 1.9	1.69 3205.27 7.18 6.96 0.23 0.05 0.06
D	Sulfur dioxide, calc.						0.40
E	Oxides of nitrogen at Oxides of nitrogen at					239	
F	K = 0.9494 F/A = 0.019591 Combustion efficiency Engine speed = 41700 r Engine exhaust tempera	pm	7				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	0.65 1224.41 2.74					
н	Measurement by AIRCRA Measurement at MCAS of Date of measurement 2 Engine S/N 000427 Test stand, single poi	AMP PENDLETON 6 AUGUST 1975	5 7				

A	T400-CP-400	GROUND IDLE	File T400011	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28	T = 75°F RH = 47% B = 29.83 in. Hg h = 0.013930 h = 0.00607	$m = 13.0 n = 23.4 \eta = 0.95$	
	CONSTITUENT		ONCENTRATION Calculated Ty semi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x pp Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	3.09 sd 3. m 28.2 sd 28. m 27. m 0. mC 268.3 w 279.	07 3.05 2.95 6 28.4 27.4 7 27.5 26.6 9 0.9 0.9 5 277.9 268.3 78 16.68 16.11	29.78 3141.05 3.05 2.96 0.10 8.98 10.42
D	Sulfur dioxide, calc.			0.40
Е	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			
F	<pre>K = 0.9598 F/A = 0.014662 Combustion efficiency = 9 Torque = 3 foot pounds Engine speed = 3366 rpm Engine exhaust temperatur</pre>			
G		38 pounds per hour 4.11		
н	Measurement by AIRCRAFT Measurement at MCAS CAMP Date of measurement 25 A Engine S/N 64100 Test stand, single point JP-5 fuel.	PENDLETON UGUST 1975		

A	T400-CP-400	FLIGHT IDLE	File T40001B	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28	T = 75°F RH = 47% B = 29.83 in. Hg h = 0.013930 h = 0.00607	m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT	EXHAUST CONCI Measured dry	ENTRATION Calculated semi- wet dry	EMISSION INDEX
C	Carbon monoxide ppr Carbon dioxide % Oxides of nitrogen ppr Nitric oxide ppr Nitrogen dioxide ppr Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	3.06 sd 3.04 a 28.1 sd 28.5 a 27.6 a 0.9	3.02 2.92 28.3 27.3 27.4 26.5 0.9 0.9 228.3 220.5	30.71 3144.78 3.08 2.98 0.10 7.46 8.65
D	Sulfur dioxide, calc.			0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of		102	
F	<pre>K = 0.9600 F/A = 0.014504 Combustion efficiency = 98 Torque = 5.9 foot pounds Engine speed = 4105 rpm Engine exhaust temperature</pre>			
G	EMISSION RATE (pounds of of for a fuel flow rate of land carbon monoxide Carbon dioxide Oxides of nitrogen	3 pounds per hour		
		1.07 1.24 0.06		_
н	Measurement by AIRCRAFT Measurement at MCAS CAMP Date of measurement 25 Al Engine S/N 64100 Test stand, single point JP-5 fuel.	PENDLETON JGUST 1975		

Α	T400-CP-400		CRUISE		File	T40001C	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28		T = 75°F RH = 47% B = 29.83 h = 0.00 h _{sd} = 0.00	3 in. Hg L3930	1	13.0 23.4 0.95	
	CONSTITUENT			AUST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC	108.0 sd 3.75 sd 53.8 sd 5.4 w	3.73	48.0 3.71 54.3 52.5 1.7 5.6 15.83 79.85	46.1 3.56 52.1 50.5 1.6 5.4 15.20 76.69 4.53	2.64 3206.59 4.90 4.75 0.15 0.15
D	Sulfur dioxide, calc.			****			0.40
E	Oxides of nitrogen at Oxides of nitrogen at					163	
F	K = 0.9547 F/A = 0.017389 Combustion efficiency Torque = 20.1 foot po Engine speed = 5735 r Engine exhaust temper	unds pm					
G	EMISSION RATE (pounds for a fuel flow rate Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide	of 283 (907 ((pounds per 1 0.75 7.46 39				
н	Measurement by AIRCR Measurement at MCAS Date of measurement Engine S/N 64100 Test stand, single po	CAMP PE 25 AUGU	ENDLETON IST 1975				

Α	T400-CP-400	N	MILITARY			File T	40001M	
В	J = -0.07 L = -0.0006 L' = 0.14 M = -0.00626 M' = 0.28		h – 0		Нg	m = 1 n = 2 η =	23.4	
	CONSTITUENT		Measure		CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm % ppm ppm ppm ppmC	79.0 4.31 84.2 4.5	sd sd w	15.7 4.29 85.5 32.8 2.7 4.7	15.6 4.26 85.0 82.3 2.7 4.7 15.08 80.04	15.0 4.08 81.2 78.7 2.6 4.5 14.41 76.51 4.99	0.75 3206.10 6.68 6.47 0.21 0.11
D	Sulfur dioxide, calc.							0.40
E	Oxides of nitrogen at Oxides of nitrogen at						223	
F	<pre>K = 0.9501 F/A = 0.019951 Combustion efficiency Torque = 36.7 foot pout Engine speed = 6310 rp Engine exhaust temperate</pre>	inds om						
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide		ounds pe 31 91 75 05		r)			
н	Measurement by AIRCRA Measurement at MCAS Control Date of measurement 2 Engine S/N 64100 Test stand, single point JP-5 fuel.	CAMP PEN	DLETON T 1975					

A	GTC85-72	NO LOAD	File GT8501I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 68°F RH = 61% B = 29.93 in. I h = 0.014080 h _{sd} = 0.00607	$\begin{array}{c} m = 13.0 \\ n = 23.4 \\ \eta = 0.95 \end{array}$	
	CONSTITUENT	EXHAUST (Measured	CONCENTRATION Calculated dry semi- wet dry	EMISSION INDEX
С	Carbon dioxide 2 Oxides of nitrogen properties oxide properties properties oxide properties	0.96 sd (0.96 sd (0.9	4.2 173.2 170.4 0.95 0.95 0.93 9.3 9.2 9.1 9.0 9.0 8.8 0.3 0.3 0.3 0.5 50.2 49.4 9.68 19.56 19.25 9.35 78.87 77.59 2.21	37.43 3215.88 3.28 3.18 0.10 5.36 6.22
D	Sulfur dioxide, calc.	· · · · · · · · · · · · · · · · · · ·		0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			
F	K = 0.9779 F/A = 0.004482 Combustion efficiency = 9 Engine speed = 42400 rpm Engine exhaust temperature			
G	EMISSION RATE (pounds of for a fuel flow rate of 1) Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide)	
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 29 SEngine S/N 126P2245 Test Cell 103, single points of JP-5 fuel.	ORKFAC ALAMEDA UULY 1976		

A	GTC85-72	LOAD		File GT8501M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 68°F RH = 61% B = 29.93 i h = 0.0140 h _{sd} = 0.0060	80	m = 13.0 n = 23.4 $\eta = 0.95$	
	CONSTITUENT	EXHAU Measured	dry se	CION lated emi- wet dry	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide	ppm 157.6 sd 2.14 sd ppm 24.3 sd ppm ppm ppm 2.7 w	2.13 2 24.6 24 23.8 23 0.8 0 2.8 2	3.5 149.5 2.11 2.06 3.5 23.8 3.7 23.1 0.8 0.8 2.8 2.7 7.98 17.51 7.28 77.20 3.21	14.83 3208.28 3.88 3.76 0.12 0.13 0.15
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3 Oxides of nitrogen at 3			124	
F	K = 0.9679 F/A = 0.009974 Combustion efficiency = Engine speed = 42050 rp Engine exhaust temperat	m			
	EMISSION RATE (pounds o for a fuel flow rate of	-			
G	Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CH _y /x Hydrocarbons, CH ₄ Sulfur dioxide	3.11 673.74 0.81 0.03 0.03 0.08			
н	Measurement by AIRCRAF Measurement at NAVAIRE Date of measurement 29 Engine S/N 126P2245 Test Cell 103, single p JP-5 fuel.	WORKFAC ALAMEDA JULY 1976		stack.	

A	GTPC95-2	IDLE		File GT9501I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 94°F RH = 18% B = 29.90 in h = 0.00968 h = 0.00607		$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT		dry s	TION ulated emi- wet dry	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	0.94 sd 11.9 sd	0.93 12.0 1 11.6 1 0.4 19.6 1	3.8 82.8 0.93 0.92 2.0 11.8 1.6 11.4 0.4 0.4 9.5 19.3 9.60 19.37 8.86 77.94 1.76	18.75 3259.21 4.39 4.25 0.14 2.16 2.50
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% of Oxides of nitrogen at 3% of			135	
F	<pre>K = 0.9824 F/A = 0.004331 Combustion efficiency = 99 Engine exhaust temperature</pre>				
G	EMISSION RATE (pounds of of for a fuel flow rate of 13) Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide				
н	Measurement by AIRCRAFT I Measurement at NAVAIREWOR Date of measurement 15 JU Engine S/N P-28735 Test Cell 115, single poin JP-5 fuel.	RKFAC ALAMEDA INE 1976		stack.	AE SO 19-30-1987

Α	GTPC95-2	100%	File	GT9501M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 94°F RH = 18% B = 29.90 in h = 0.00968 h = 0.00607	n = η = 7	13.0 23.4 0.95	
	CONSTITUENT		T CONCENTRATION Calculate dry semi- dry	ed wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 35.5 sd 2.05 sd ppm 33.7 sd ppm ppm ppm ppm 7.0 w	31.7 31.5 2.04 2.02 34.1 33.9 33.0 32.8 1.1 1.1 7.2 7.2 18.23 18.12 79.73 79.25	30.8 1.98 33.2 32.1 1.0 7.0	3.20 3228.29 5.65 5.47 0.18 0.36 0.42
D	Sulfur dioxide, calc.				0.40
E		3% oxygen, calc.(ppm 3% oxygen, meas.(ppm		185	
F	K = 0.9729 F/A = 0.009498 Combustion efficiency Engine exhaust temper			,	
G		of constituent per ho of 293 pounds per hour 0.94 945.89 1.66 0.10 0.12 0.12		-	
H	Measurement at NAVAI Date of measurement Engine S/N P-28735			ek.	

A	GTCP100-54	IDLE		File C	T1001I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 77°F RH = 36% B = 29.82 in h = 0.01133 h _{sd} = 0.00607	8	m = 1 n = 2 η =		
	CONSTITUENT		T CONCENT Ca dry	RATION lculated semi- dry	wet	EMISSION INDEX
С	Carbon dioxide Oxides of nitrogen p Nitric oxide p Nitrogen dioxide p Hydrocarbons, CHy/x p Hydrocarbons, CH ₄	pm 56.0 sd % 0.90 sd pm 16.3 sd pm pm pm % 13.7 w	53.4 0.89 16.5 16.0 0.5 14.0	53.1 0.89 16.4 15.9 0.5 13.9	52.4 0.88 16.2 15.7 0.5 13.7 19.40 77.83 1.88	12.48 3276.38 6.32 6.12 0.20 1.61 1.87
D	Sulfur dioxide, calc.					0.40
Ε	Oxides of nitrogen at 3% Oxides of nitrogen at 3%				188	
F	K = 0.9812 F/A = 0.004125 Combustion efficiency = Engine speed = 35730 rpm Engine exhaust temperatu					
G	EMISSION RATE (pounds of for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide					
Н	Measurement by AIRCRAFT Measurement at NAVAIREW Date of measurement 28 Engine S/N P9907 Test Cell 114, single po JP-5 fuel.	ORKFAC ALAMEDA JUNE 1976				

A	GTCP100-54	100%		File	GT1001M	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 77°F RH = 36% B = 29.82 in h = 0.01133 h _{sd} = 0.00603	38	m = n = η =		
	CONSTITUENT		ST CONCEN Codry	TRATION alculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide Carbon dioxide Oxides of nitrogen Nitric oxide Nitrogen dioxide Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen Nitrogen Water	ppm 52.3 sd 1.72 sd ppm 29.7 sd ppm ppm ppm ppmC 2.7 w	48.9 1.71 30.0 29.1 0.9 2.8 18.67 79.61	48.6 1.70 29.9 28.9 0.9 2.8 18.56 79.13	47.6 1.66 29.3 28.3 0.9 2.7 18.19 77.56 2.59	5.89 3234.53 5.95 5.76 0.19 0.16 0.19
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at Oxides of nitrogen at				190	
F	K = 0.9741 F/A = 0.007963 Combustion efficiency Engine speed = 35190 r Engine exhaust tempera	pm				
G	EMISSION RATE (pounds for a fuel flow rate of Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	f 413 pounds per hour 2.43 1335.86 2.46				
н	Measurement by AIRCRA Measurement at NAVAIR Date of measurement 2 Engine S/N P9907 Test Cell 114, single JP-5 fuel.	EWORKFAC ALAMEDA 8 JUNE 1976				

A	T-62T-27	IDLE		File	T6201I	
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 83°F RH = 30% B = 29.80 h = 0.0114 h _{sd} = 0.0066	442	n =	13.0 23.4 0.95	
	CONSTITUENT		JST CONCE	NTRATION Calculated semi- dry	wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	1.03 sd 15.9 sd	146.9 1.02 16.1 15.6 0.5 29.8 19.59 79.37	146.0 1.02 16.0 15.5 0.5 29.6	143.9 1.00 15.7 15.3 0.5 29.2 19.20 77.77 2.01	29.53 3228.98 5.31 5.14 0.17 2.96 3.43
D	Sulfur dioxide, calc.		<u></u>			0.40
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or				161	
F	<pre>K = 0.9799 F/A = 0.004788 Combustion efficiency = 99 Engine speed = 4330 rpm Engine exhaust temperature</pre>					
G	EMISSION RATE (pounds of conformate flow rate of 50) Carbon monoxide Carbon dioxide Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH4 Sulfur dioxide	pounds per hour 1.48				
н	Measurement by AIRCRAFT EMBELS Measurement at NAVAIREWORD Date of measurement 28 JUNE Engine S/N S-424421 Test Cell 116, single point JP-5 fuel.	KFAC ALAMEDA NE 1976				

A	T-62T-27	100%		File T6201M	-
В	J = -0.07 L = -0.0001 L' = 0.14 M = -0.00033 M' = 0.28	T = 83°F RH = 30% B = 29.80 in h = 0.01144 h = 0.00607	+2	$m = 13.0$ $n = 23.4$ $\eta = 0.95$	
	CONSTITUENT	EXHAUS Measured		ATION culated semi- wet dry	EMISSION INDEX
С	Carbon monoxide pp Carbon dioxide % Oxides of nitrogen pp Nitric oxide pp Nitrogen dioxide pp Hydrocarbons, CHy/x pp Hydrocarbons, CH4 Oxygen % Nitrogen % Nitrogen %	1.62 sd m 19.0 sd m m mC 123.2 w	1.61 19.2 18.6 0.6 126.4 1	40.6 334.0 1.60 1.57 19.1 18.7 18.5 18.1 0.6 0.6 25.6 123.2 18.66 18.30 79.10 77.56 2.54	42.77 3154.46 3.94 3.82 0.12 7.79 9.04
٥	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% Oxides of nitrogen at 3%			127	
F	<pre>K = 0.9746 F/A = 0.007693 Combustion efficiency = 9 Shaft horsepower = 100 Engine speed = 4240 rpm Engine exhaust temperatur</pre>				
G	EMISSION RATE (pounds of for a fuel flow rate of l Carbon monoxide Carbon dioxide Oxides of nitrogen	02 pounds per hour 4.36 321.76 0.40			
	Hydrocarbons, CH _{y/x} Hydrocarbons, CH ₄ Sulfur dioxide	0.79 0.92 0.04			
н	Measurement by AIRCRAFT Measurement at NAVAIREWO Date of measurement 28 J Engine S/N S-424421 Test Cell 116, single poi JP-5 fuel.	RKFAC ALAMEDA UNE 1976			

Α	WR27-1	LOW FLOW 38 CAN	1	File WR2701B	
В	J = -0.07 L = -0.0008 L' = 0.14 M = -0.00658 M' = 0.28	h = 0.010000 h _{sd} = 0.00607		m = 9.5 n = 19.0 $\eta = 0.95$	
	CONSTITUENT	EXHAUST Measured	dry se	CION ulated emi- wet	EMISSION INDEX
С	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Oxygen % Nitrogen % Water %	1.49 sd 9.3 sd 8.5 w	1.48 9.4 9.1 0.3 8.7	5.1 24.7 1.47 1.44 9.3 9.2 9.1 8.9 0.3 0.3 3.7 8.5 3.81 18.47 9.11 77.68 2.40	3.48 3199.86 2.13 2.06 0.07 0.60 0.69
D	Sulfur dioxide, calc.				0.40
E	Oxides of nitrogen at 3% ox Oxides of nitrogen at 3% ox			67	
F	<pre>K = 0.9760 F/A = 0.006974 Combustion efficiency = 99. Shaft horsepower = 85 Engine speed = 102.7 percer Engine exhaust temperature</pre>	nt rpm			
G	Oxides of nitrogen Hydrocarbons, CH _Y /x Hydrocarbons, CH ₄		:)		
н	Measurement by AIRCRAFT EN Measurement at NAVAL AIR S Date of measurement 10 DEC Engine S/N 121 APU Test Stand, probe at en	TATION, NORTH ISLA EMBER 1975	AND		

А	WR27-1	HIGH FLOW 90 C	AM	File V	VR2701C	
В	J = -0.07 L = -0.0007 L' = 0.14 M = -0.00658 M' = 0.28	h = 0.01000 h _{sd} = 0.00607		n = 3	9.5 19.0 0.95	
	CONSTITUENT		T CONCEN C dry	TRATION Calculated semi- dry	wet	EMISSION INDEX
O	Carbon monoxide ppm Carbon dioxide % Oxides of nitrogen ppm Nitric oxide ppm Nitrogen dioxide ppm Hydrocarbons, CHy/x ppm(Hydrocarbons, CH4 Oxygen % Nitrogen % Water %	121.7 sd 2.37 sd 32.5 sd	66.0 2.36 32.9 31.9 1.0 5.0	65.6 2.34 32.7 31.7 1.0 4.9 17.59 79.45	63.9 2.28 31.8 30.8 1.0 4.8 17.13 77.35 3.23	5.66 3171.54 4.63 4.49 0.15 0.21
D	Sulfur dioxide, calc.					0.40
E	Oxides of nitrogen at 3% or Oxides of nitrogen at 3% or				150	
F	<pre>K = 0.9677 F/A = 0.011153 Combustion efficiency = 99 Shaft horsepower = 85 Engine speed = 101.9 percer Engine exhaust temperature</pre>	nt rpm				
G	EMISSION RATE (pounds of co for a fuel flow rate of 140 Carbon monoxide Carbon dioxide 40 Oxides of nitrogen Hydrocarbons, CHy/x Hydrocarbons, CH ₄ Sulfur dioxide) pounds per hour 0.79				
Ħ	Measurement by AIRCRAFT EN Measurement at NAVAL AIR S Date of measurement 10 DEC Engine S/N 121 APU Test Stand, probe at en	IVIRONMENTAL SUPF STATION, NORTH IS SEMBER 1975	LAND	CE		